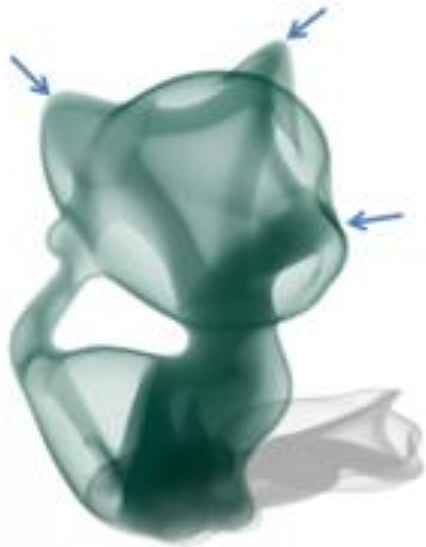


Topology Optimization for Computational Fabrication



Jun Wu

Depart. of Design Engineering, TU Delft

www.jun-wu.net





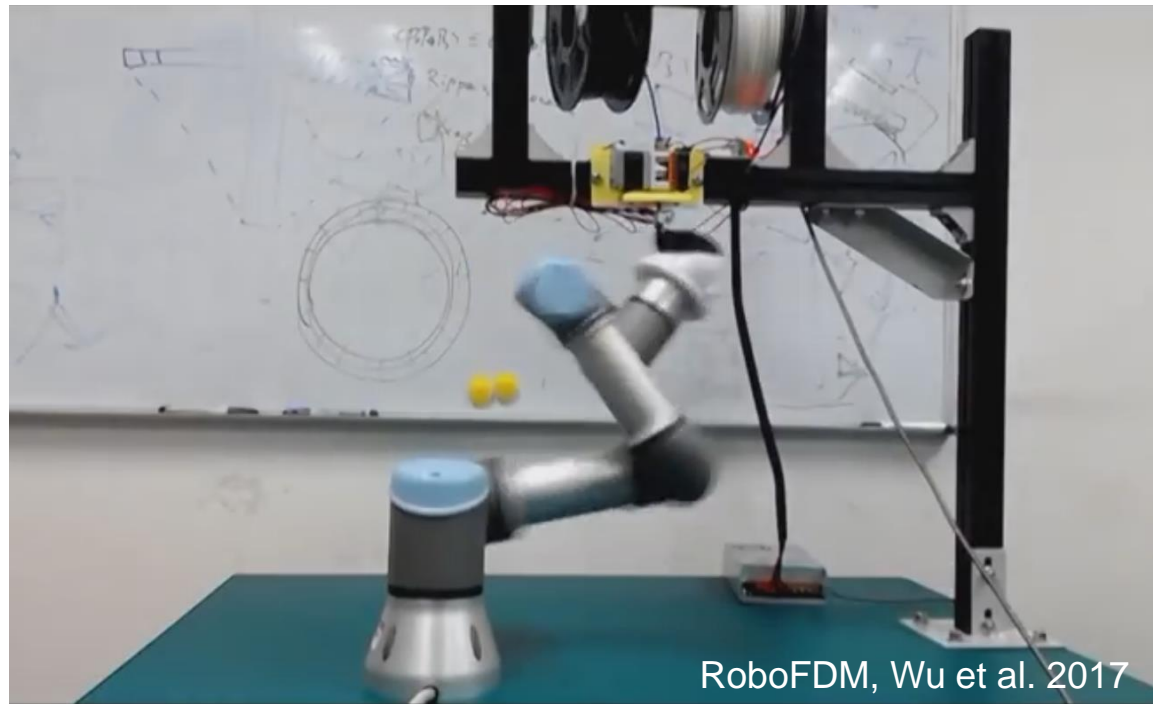


Computational Design and Fabrication Group

- Charlie Wang (CUHK->TU Delft), Jun Wu (TU Munich->Denmark->Delft)
- Generative design | Soft robots | 3D printing and robot manufacturing



Rob Scharff



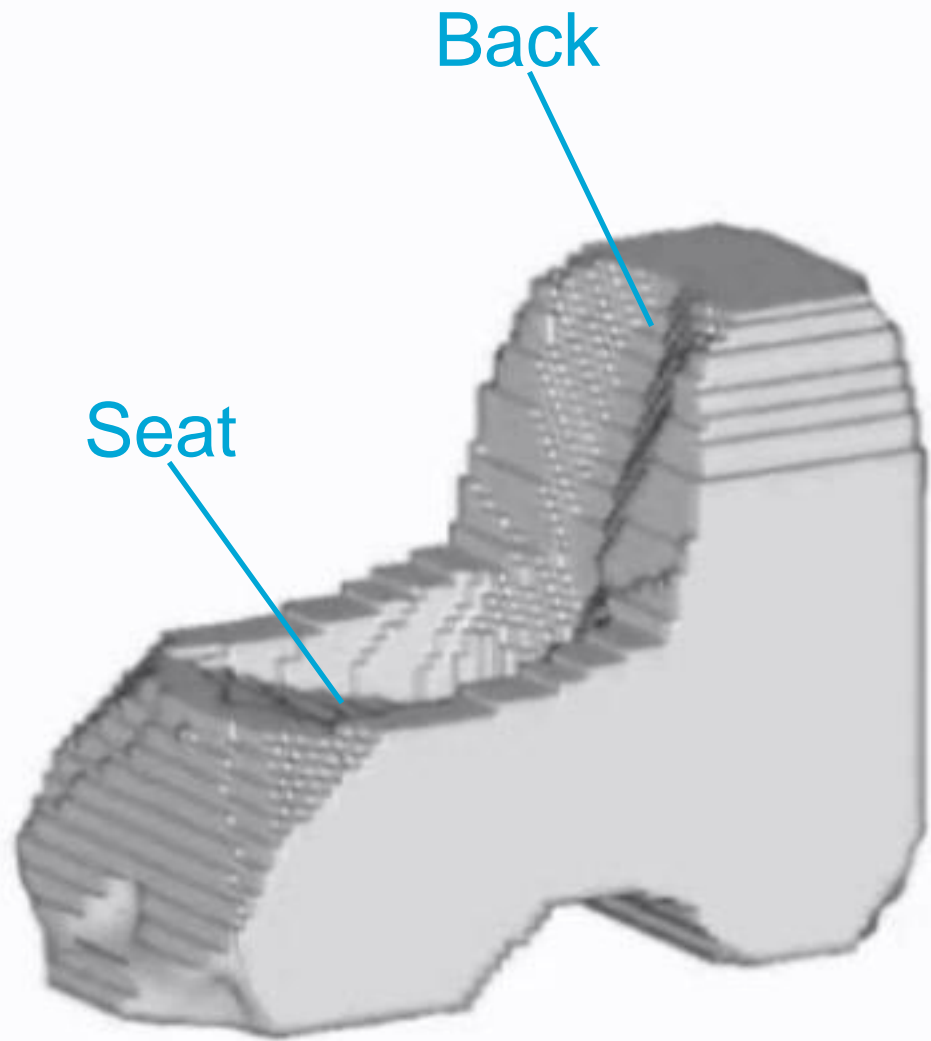
RoboFDM, Wu et al. 2017

Outline

- Basics of Topology Optimization
- Topology Optimization for Additive Manufacturing



Bone Chair by Joris Laarman



Optimization of Bone Chair
by Lothar Harzheim & Opel GmbH



Topology Optimization Examples



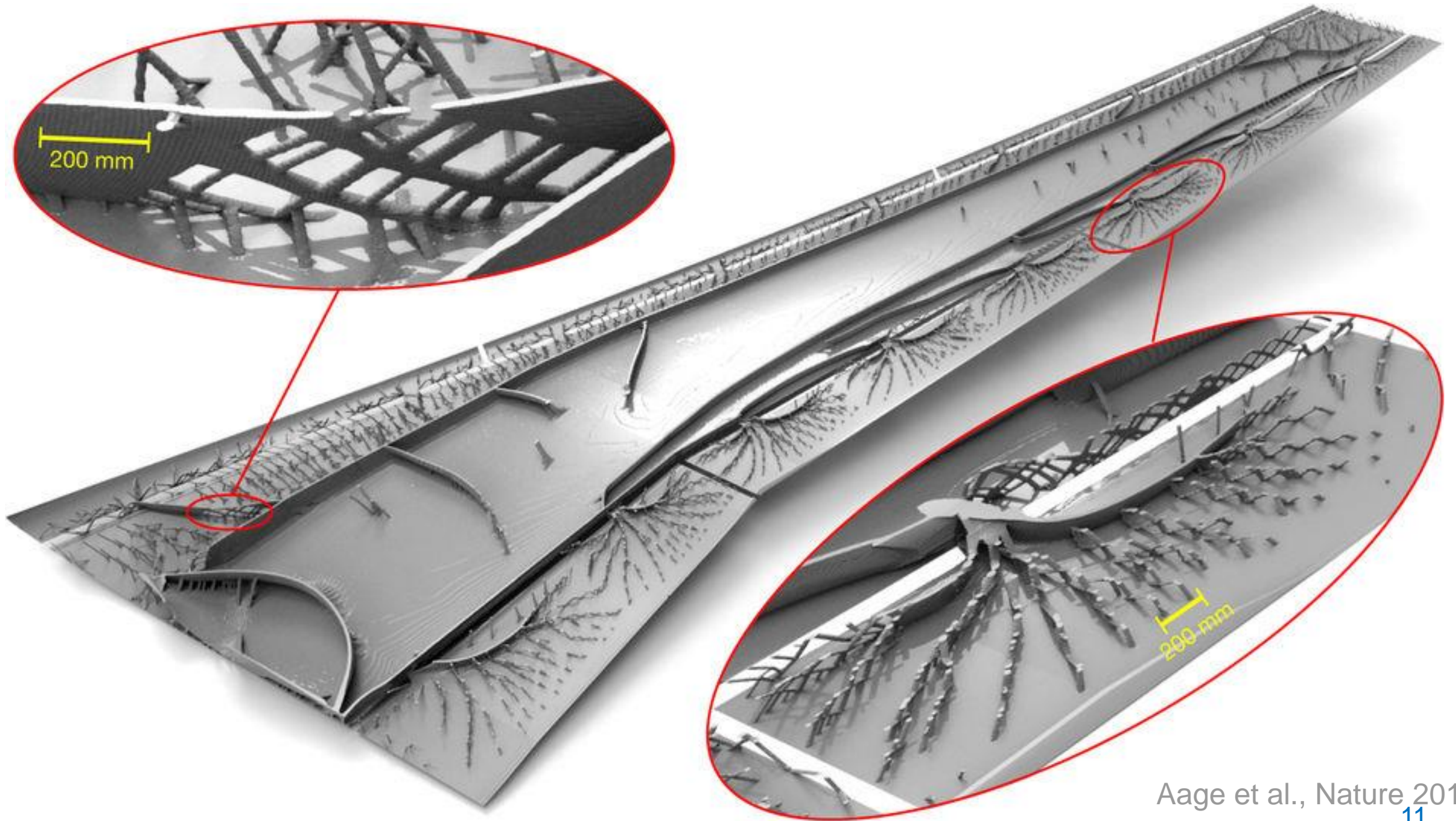
Frustum Inc.



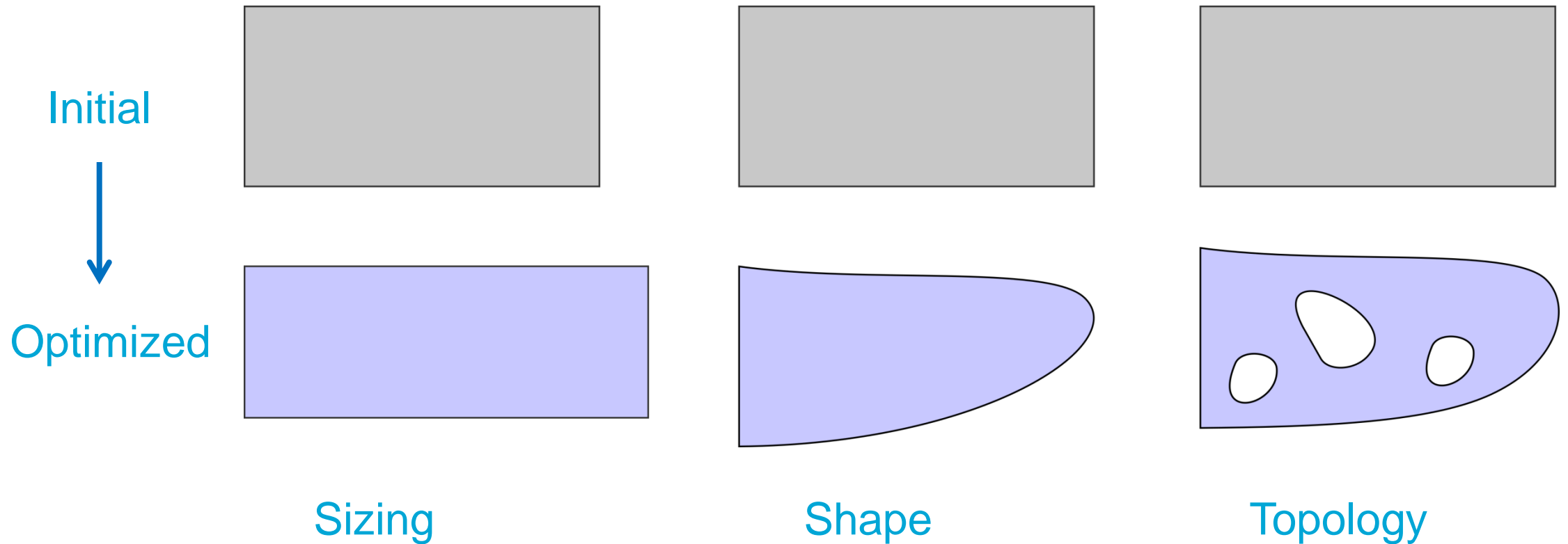
Airbus APWorks, 2016



Qatar national convention

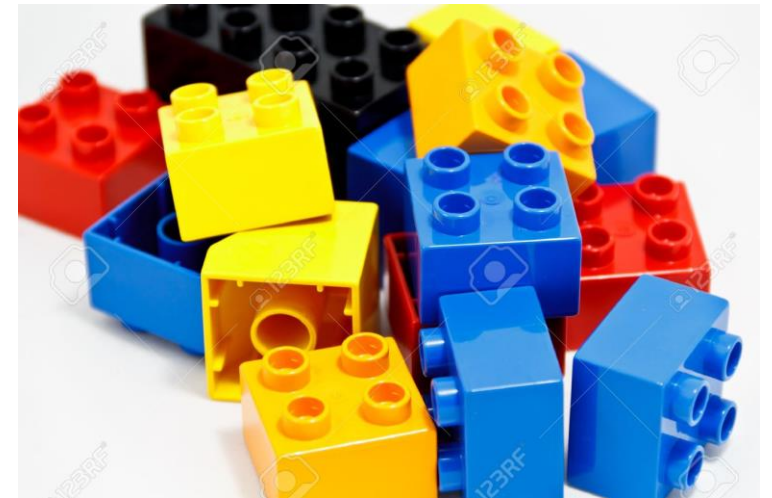
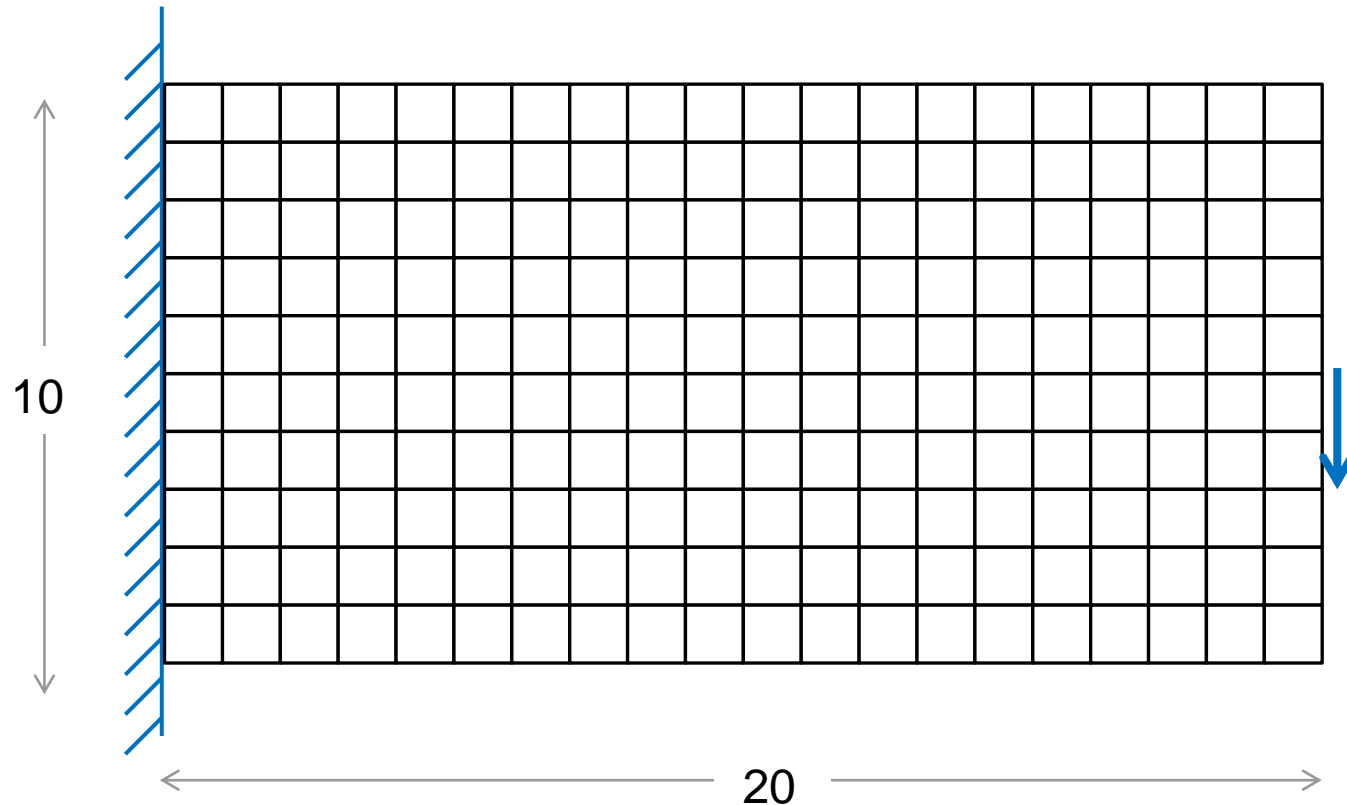


Classes of Structural optimization: Sizing, Shape, Topology



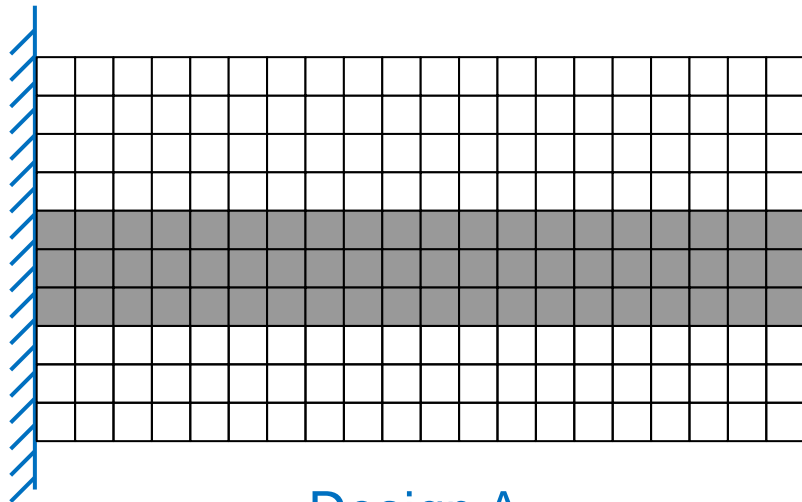
A Toy Problem

- Design the **stiffest** shape, by placing **60** Lego blocks into a grid of **20 × 10**

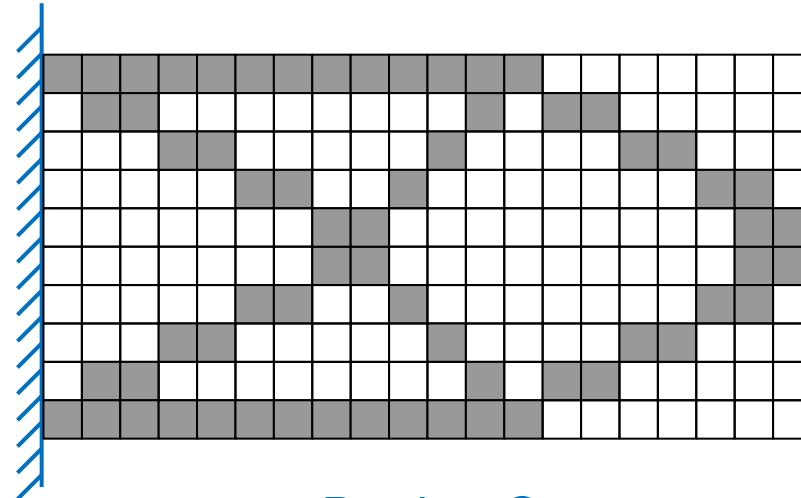


A Toy Problem: Possible Solutions

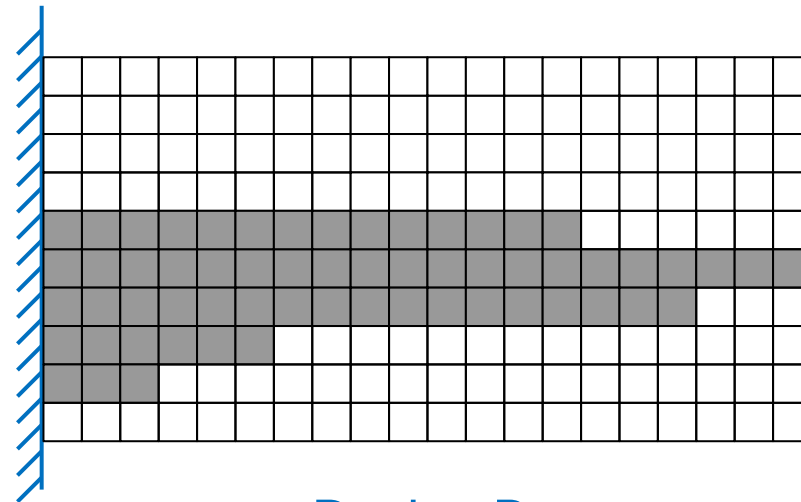
- Number of possible designs
 - $C(200,60) = \frac{200!}{60!(200-60)!} = 7.04 \times 10^{51}$
- Which one is the stiffest?



Design A



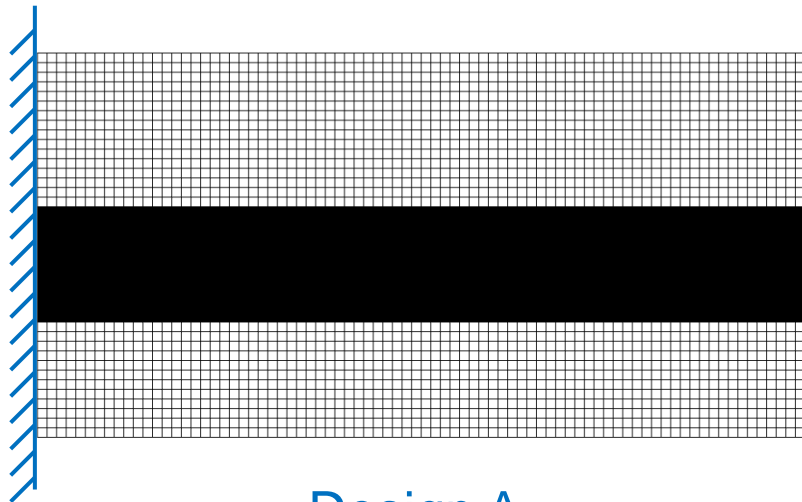
Design C



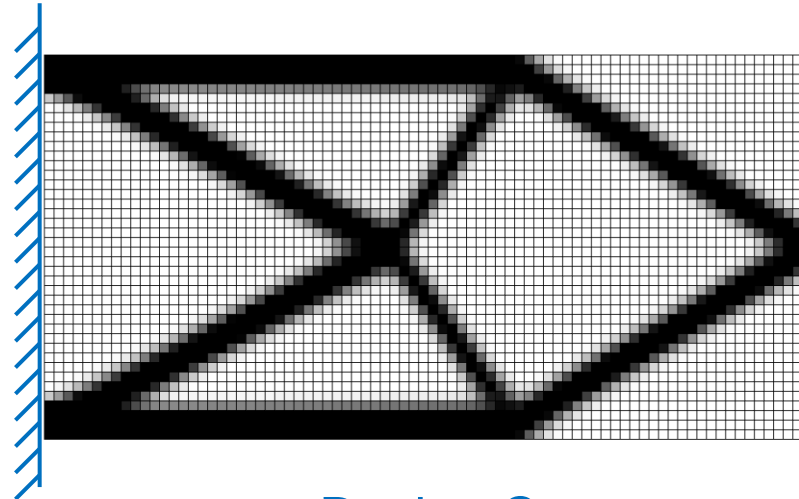
Design B

A Toy Problem: Possible Solutions

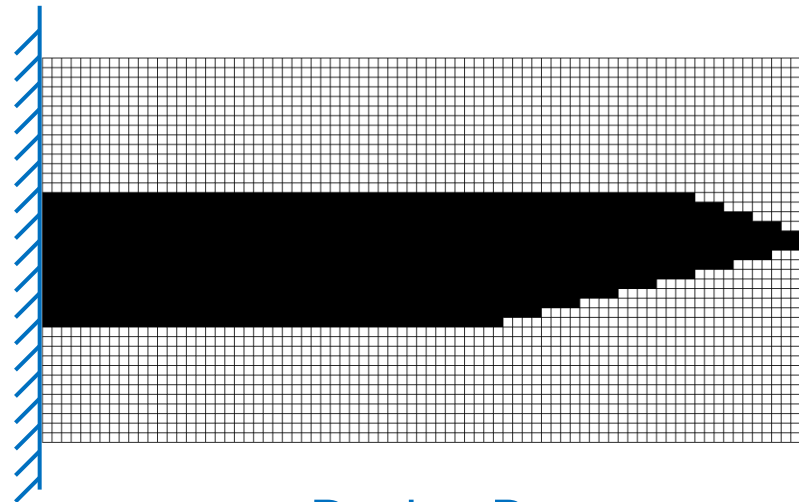
- Which one is the stiffest?



Design A



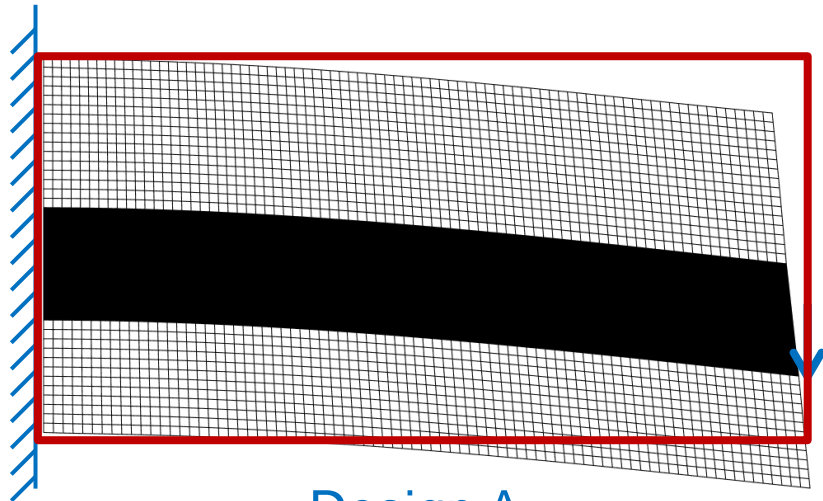
Design C



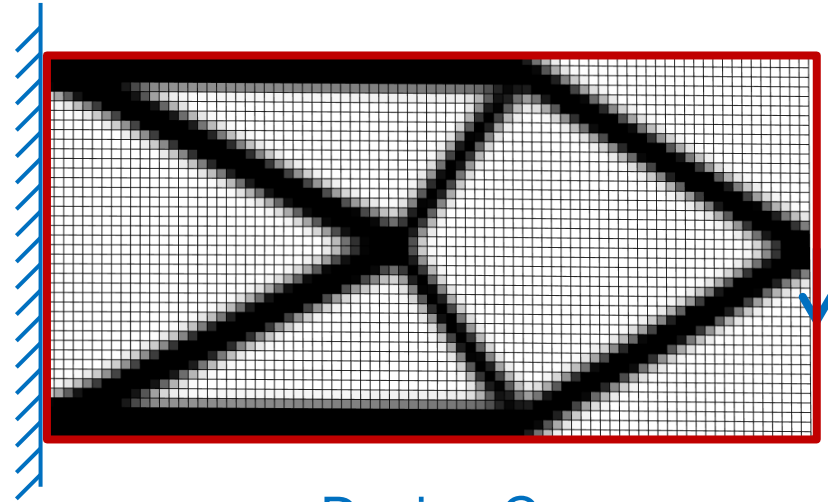
Design B

A Toy Problem: Possible Solutions

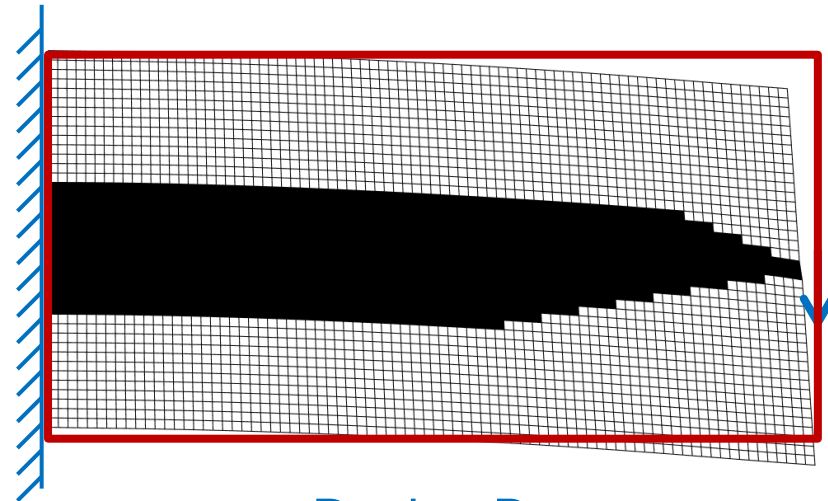
- Which one is the stiffest?



Design A

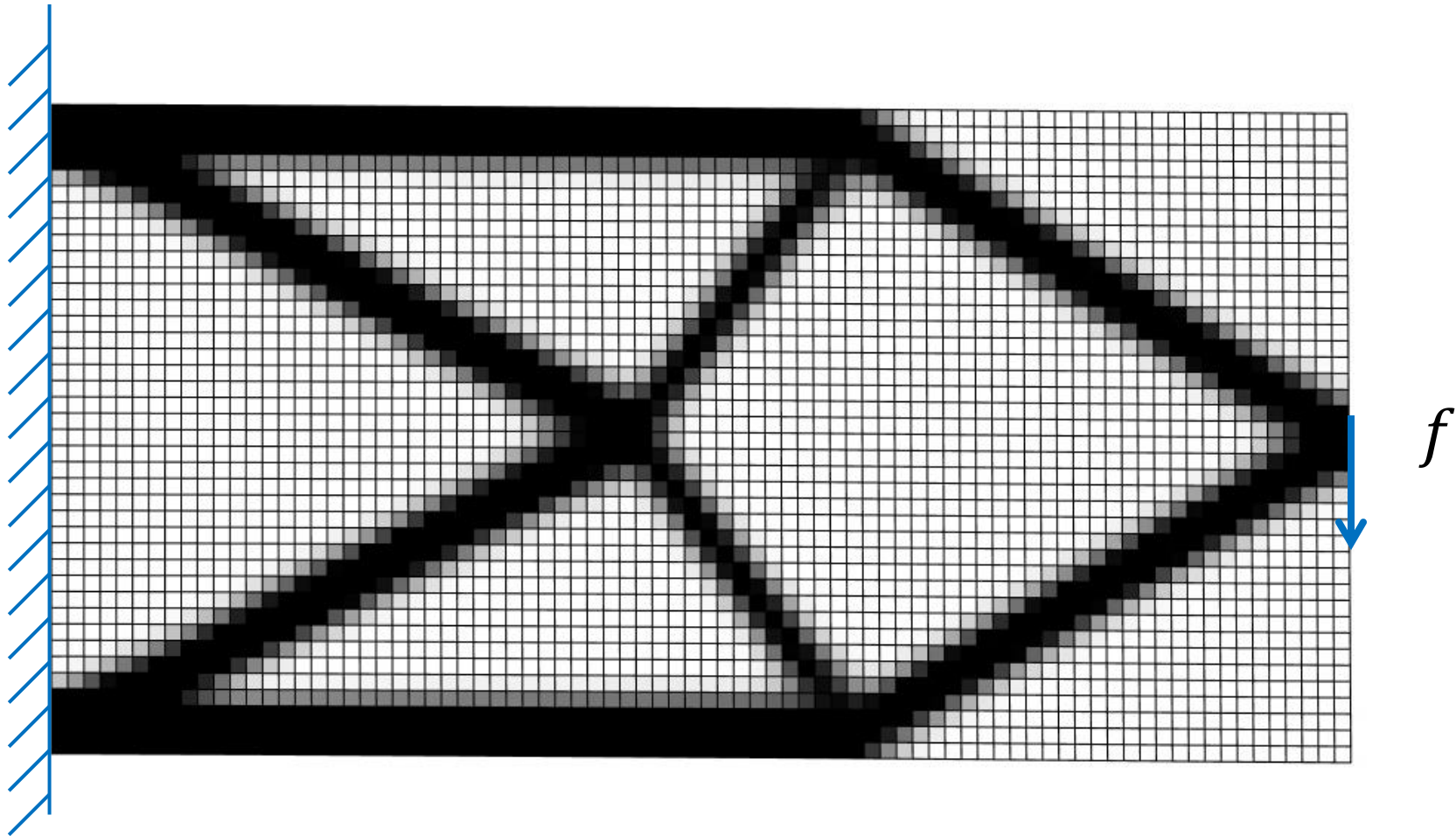


Design C



Design B

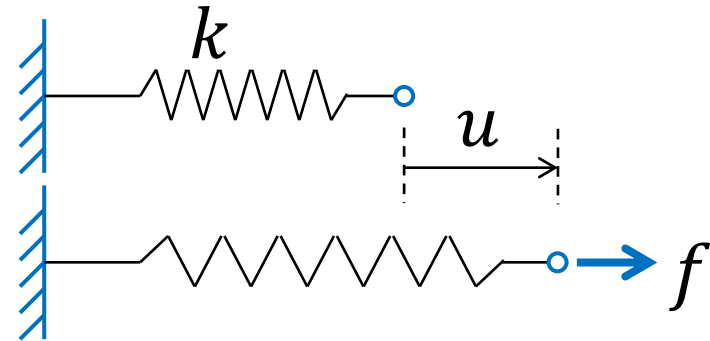
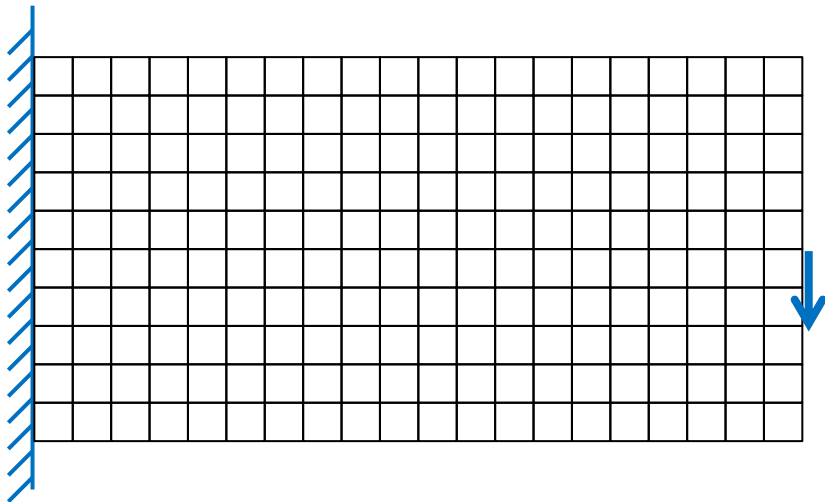
Topology Optimization Animation



Topology Optimization

Minimize: $c = \frac{1}{2} U^T K U$ ← Elastic energy $c = \frac{1}{2} f u = \frac{1}{2} k u^2$

Subject to: $K U = F$ ← Static equation $k u = f$



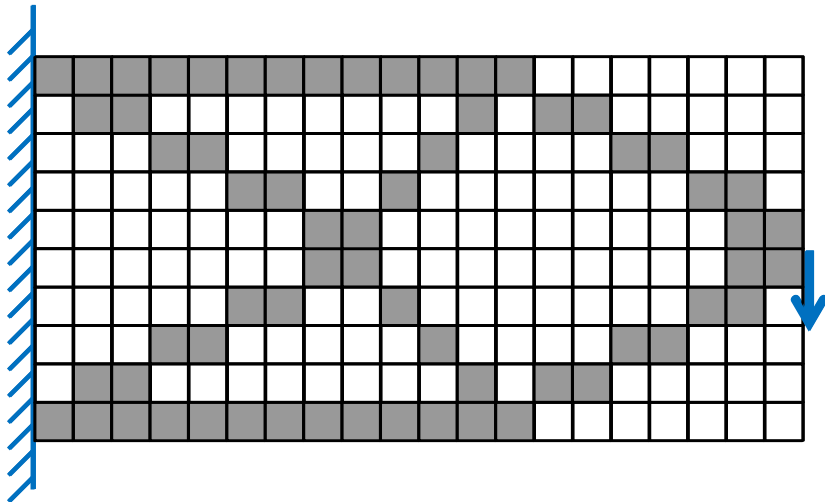
Topology Optimization

Minimize: $c = \frac{1}{2} U^T K U$ Elastic energy

Subject to: $KU = F$ Static equation

$\rho_i \in [0, 1]$ Design variables
(1 (solid)
(0 (void), $\forall i$

$g = \sum_i \rho_i - V_0 \leq 0$ Volume constraint



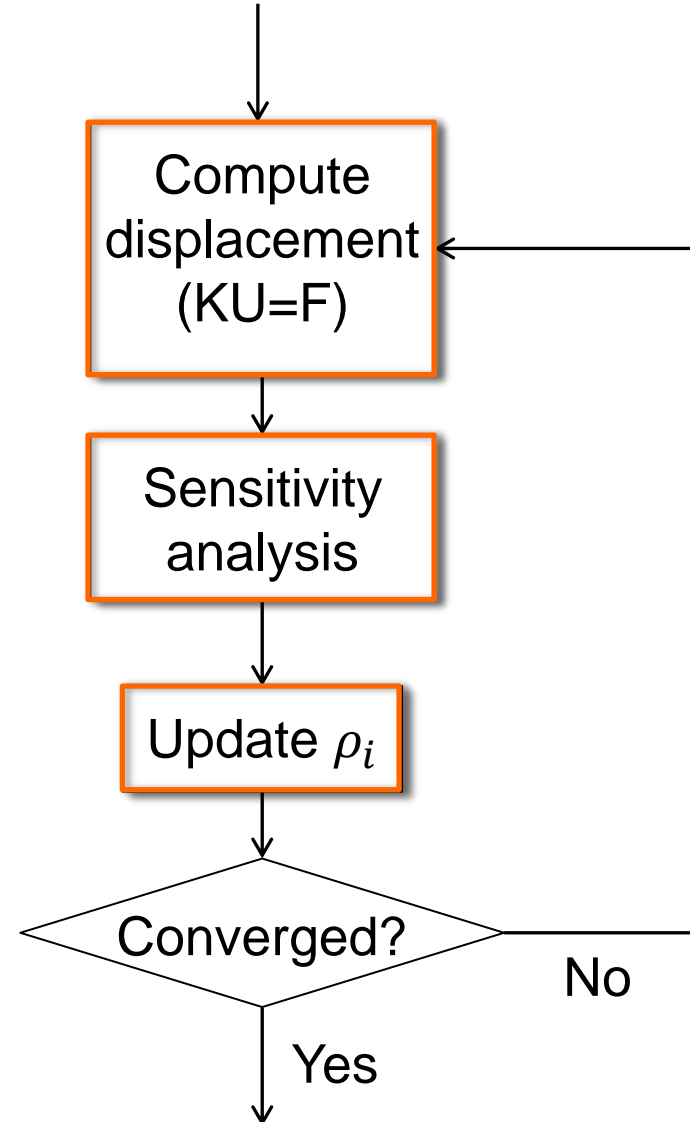
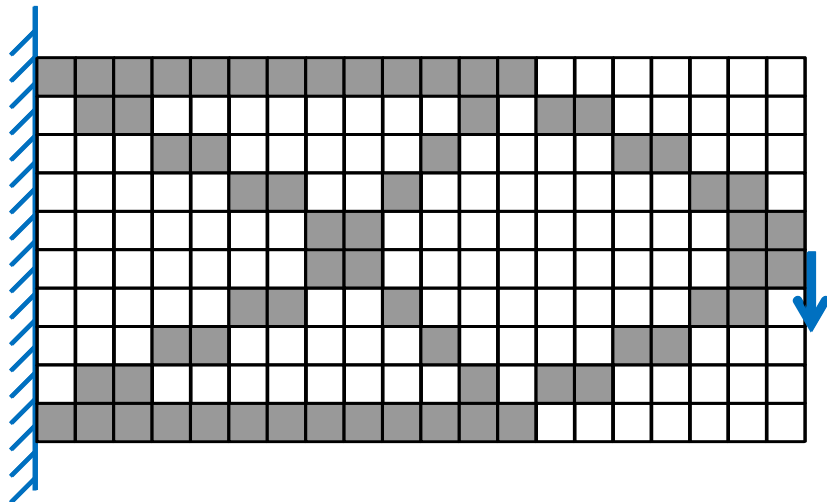
Topology Optimization

Minimize: $c = \frac{1}{2} U^T K U$

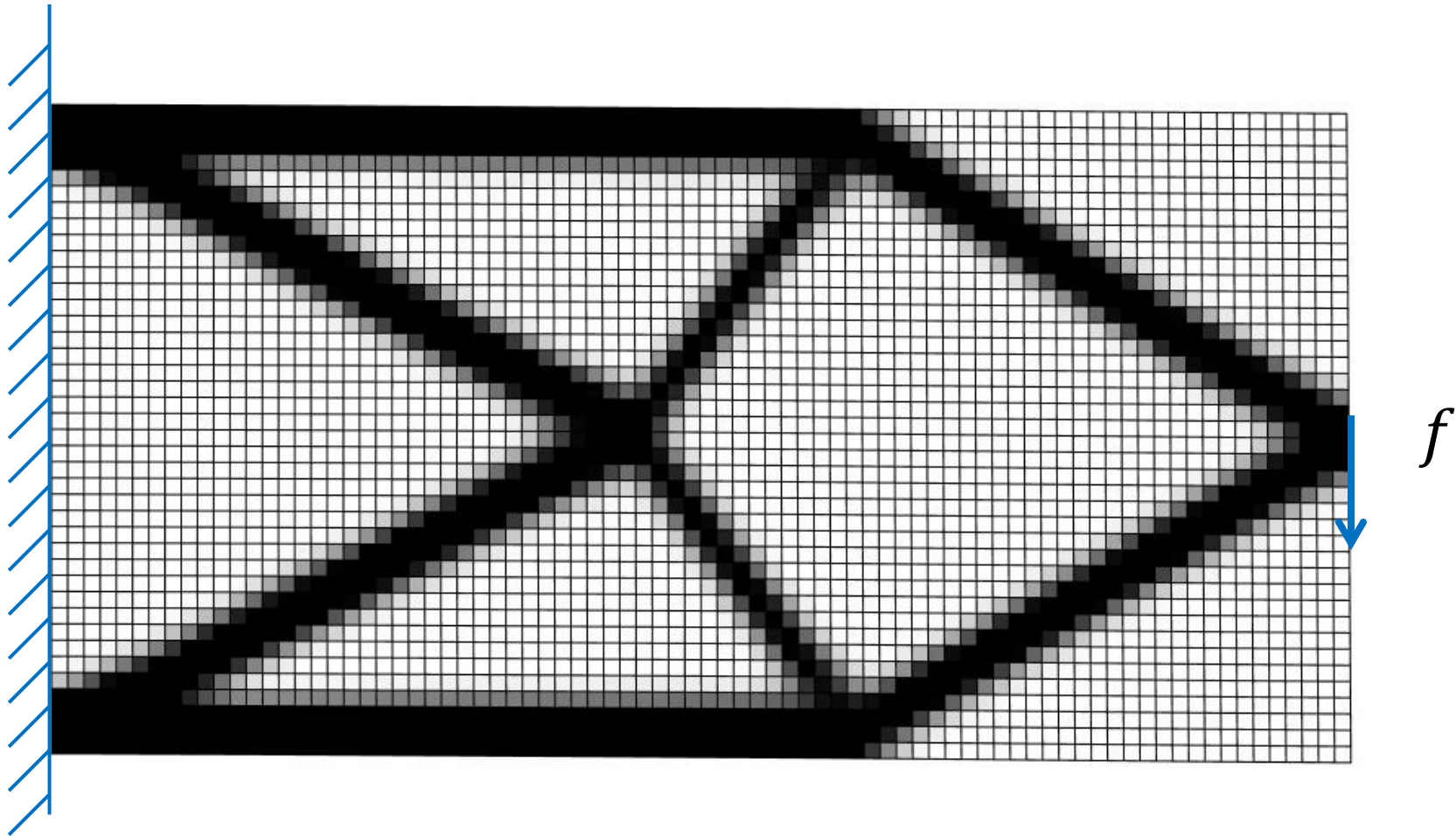
Subject to: $KU = F$

$$\rho_i \in [0,1], \forall i$$

$$g = \sum_i \rho_i - V_0 \leq 0$$

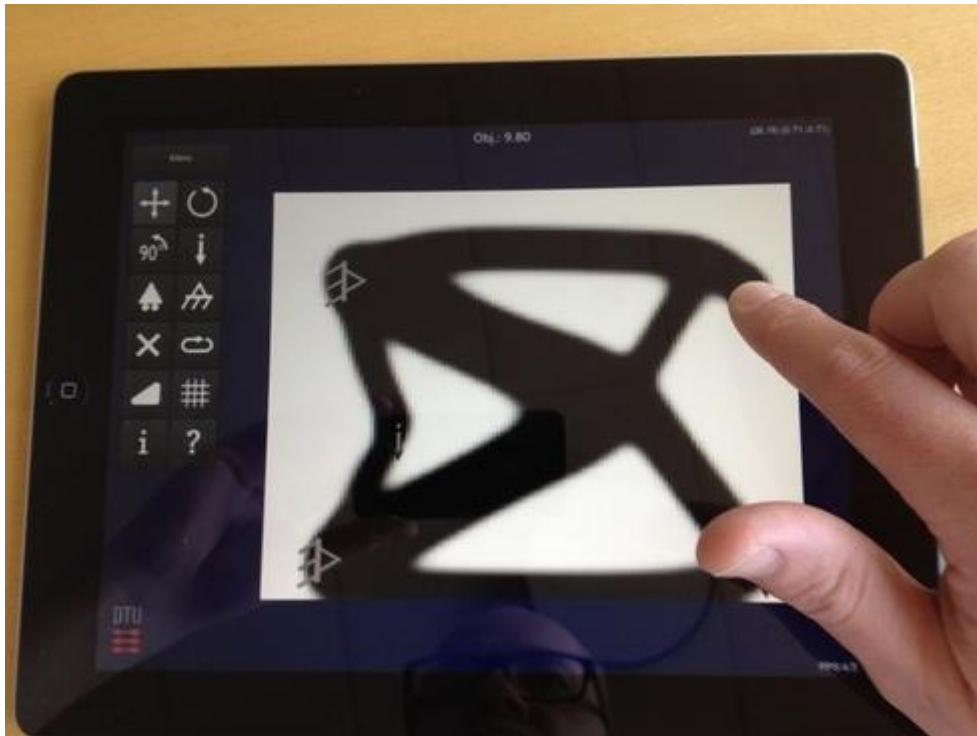


Topology Optimization Animation



Demo

- www.topopt.dtu.dk



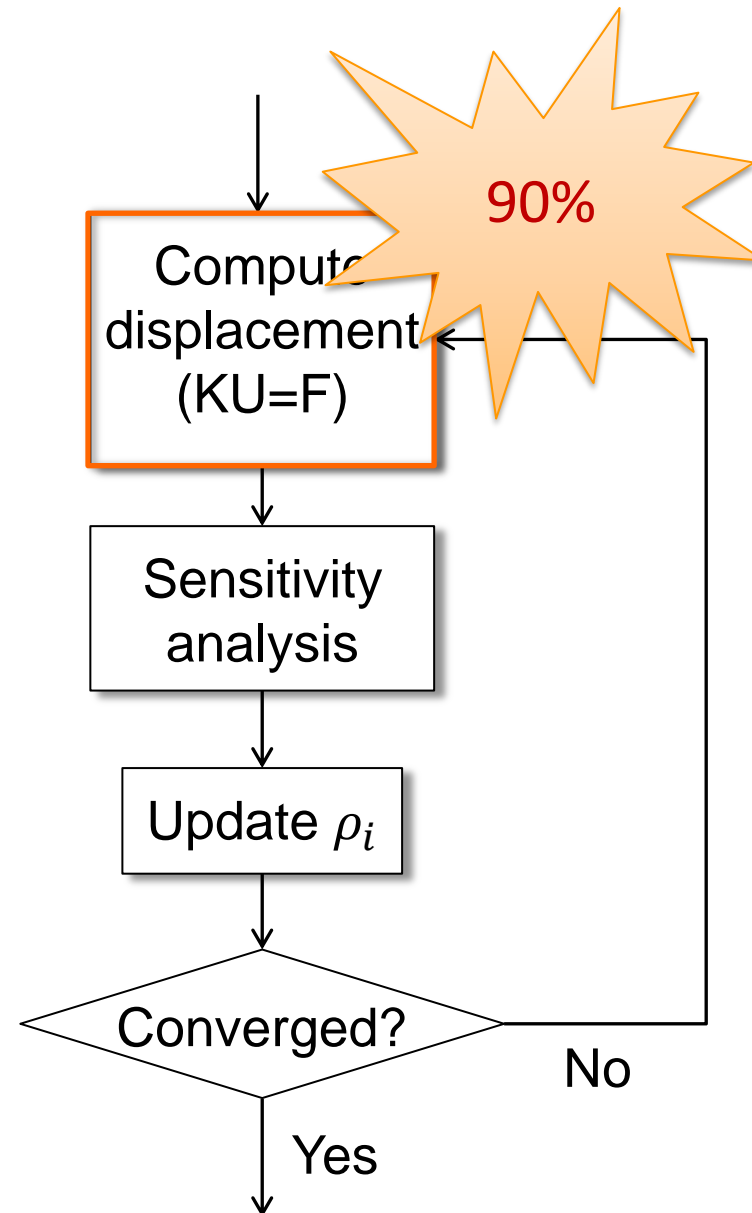
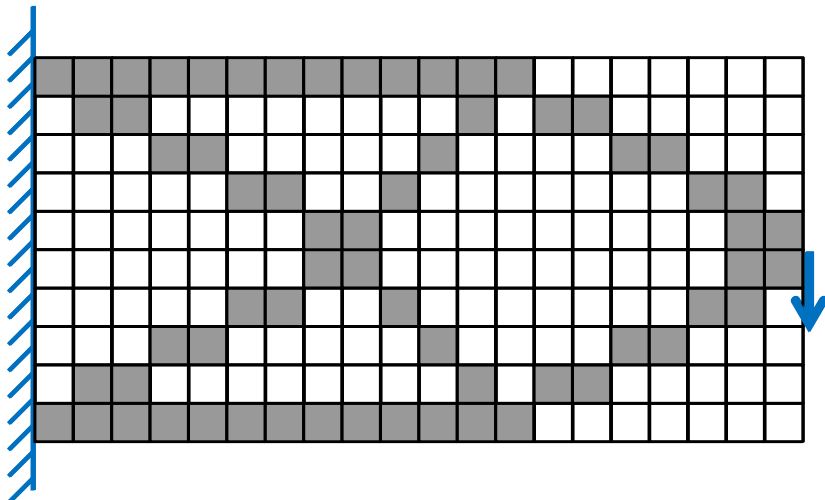
Topology Optimization

Minimize: $c = \frac{1}{2} U^T K U$

Subject to: $KU = F$

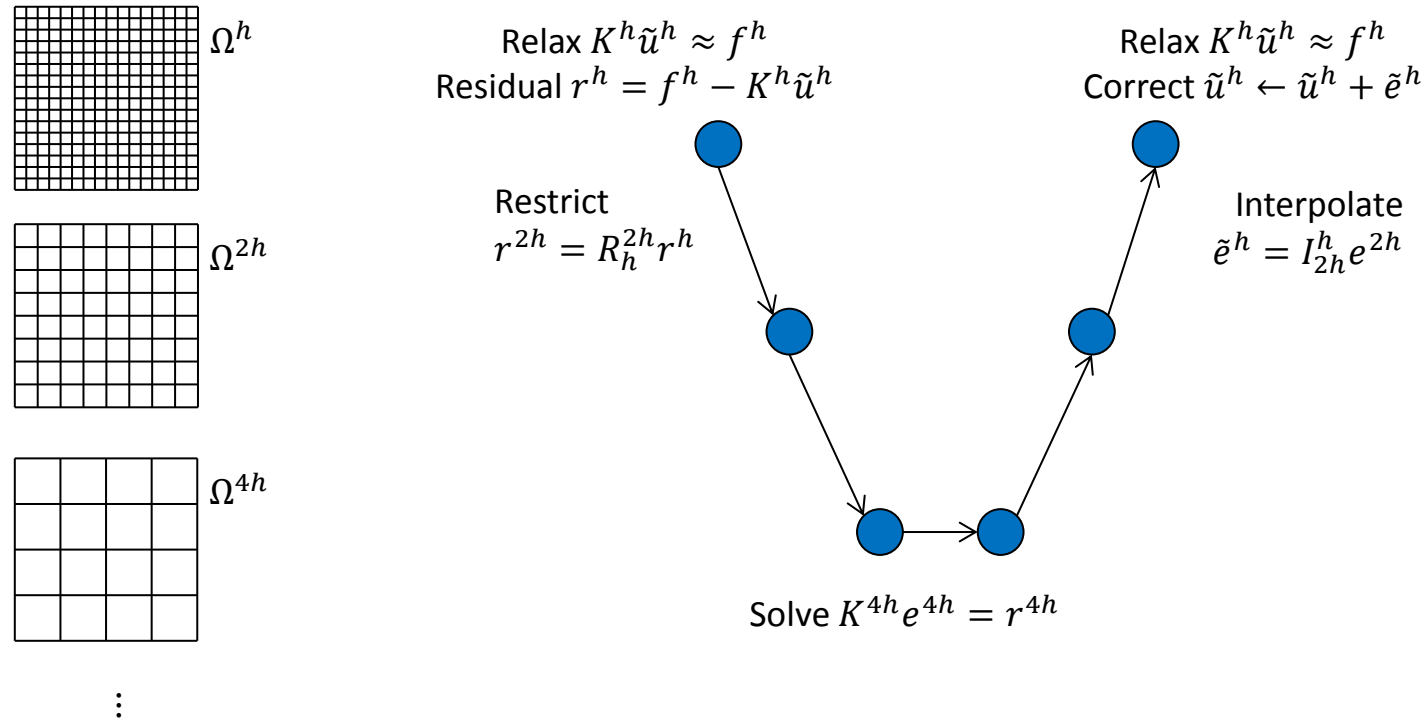
$$\rho_i \in [0,1], \forall i$$

$$g = \sum_i \rho_i - V_0 \leq 0$$



Geometric Multigrid: Solving $Ku = f$

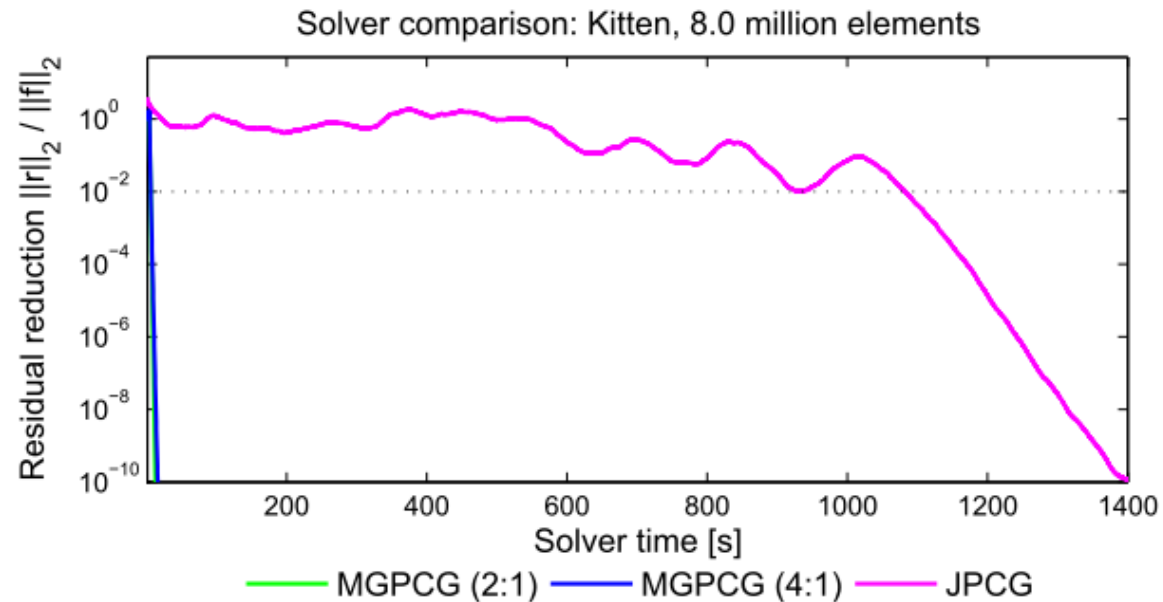
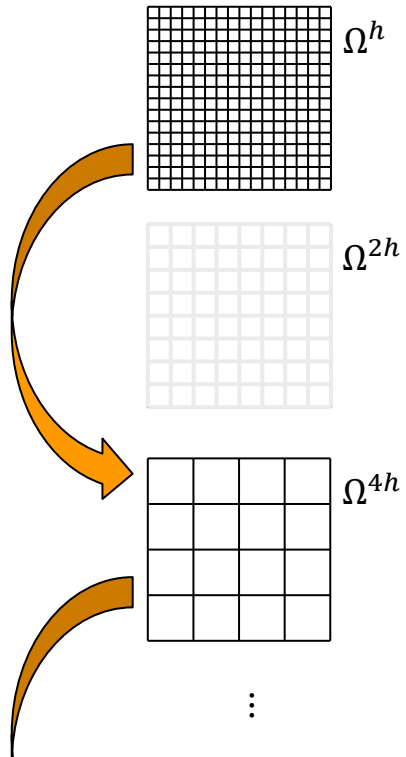
- Successively compute approximations u_m to the solution $u = \lim_{m \rightarrow \infty} u_m$
- Consider the problem on a hierarchy of successively coarser grids to accelerate convergence



W. Briggs, A multigrid tutorial, 2000

Memory-Efficient Implementation on GPU

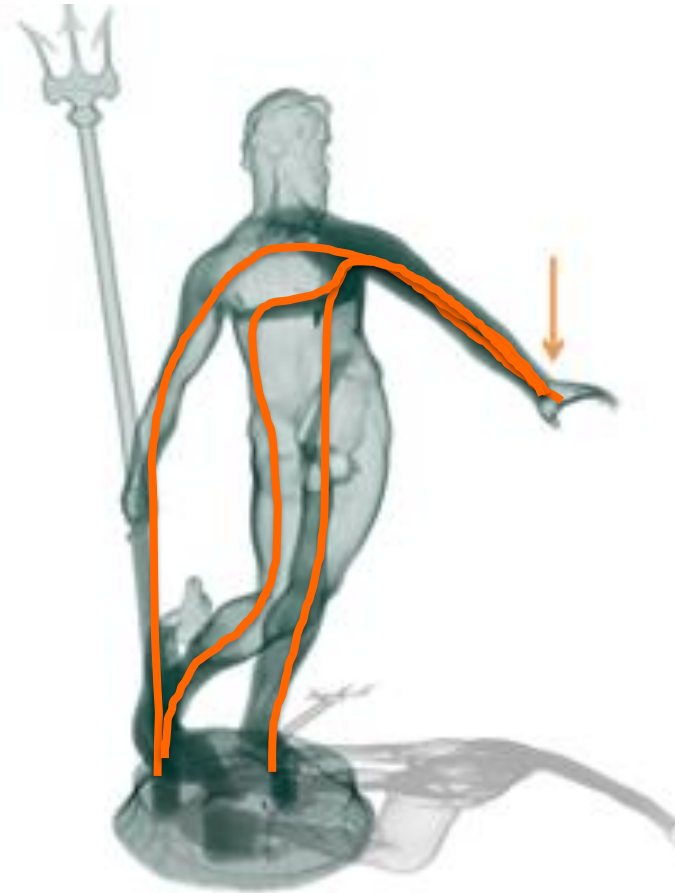
- On-the-fly assembly
 - Avoid storing matrices on the finest level
- Non-dyadic coarsening (i.e., 4:1 as opposed to 2:1)
 - Avoid storing matrices on the second finest level



Wu et al., TVCG'2016
Dick et al., SMPT'2011

High-Resolution Design

Resolution: $621 \times 400 \times 1000$
#Element 14.2m
Time: 12 minutes



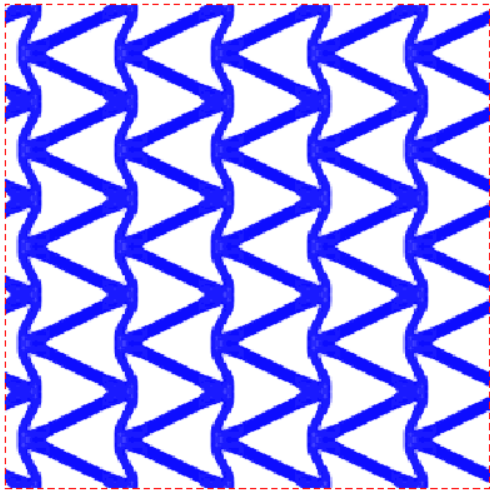
Kitten

Resolution: **262 × 238 × 400**

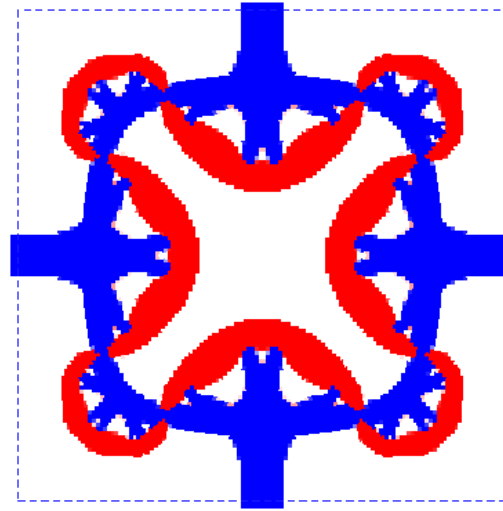
Elements: **8 million**

Target volume reduction: **60%**

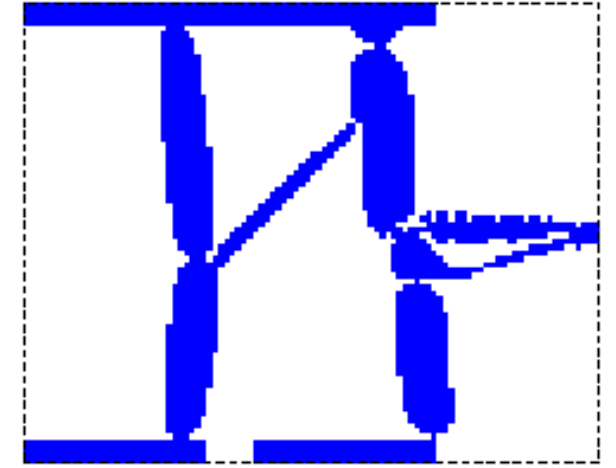




Negative Poisson's ratio
Larsen et al. 1997



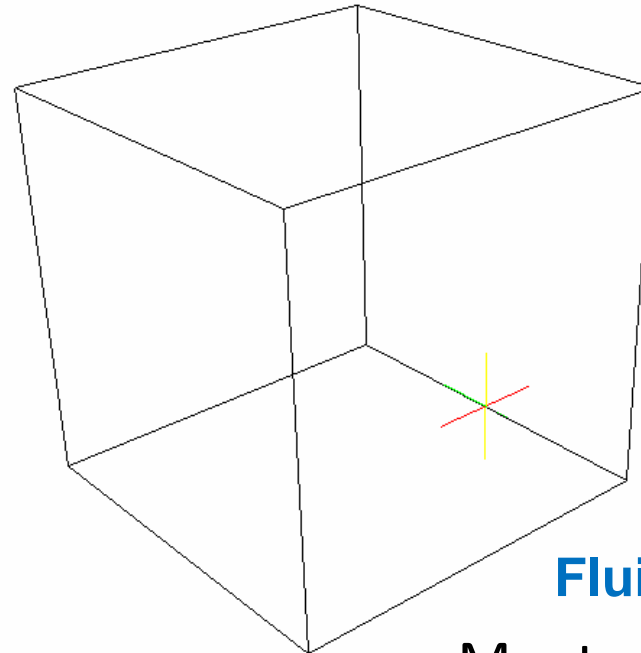
Negative thermal expansion
Sigmund & Torquato 1996



Electric actuator
Sigmund 2000



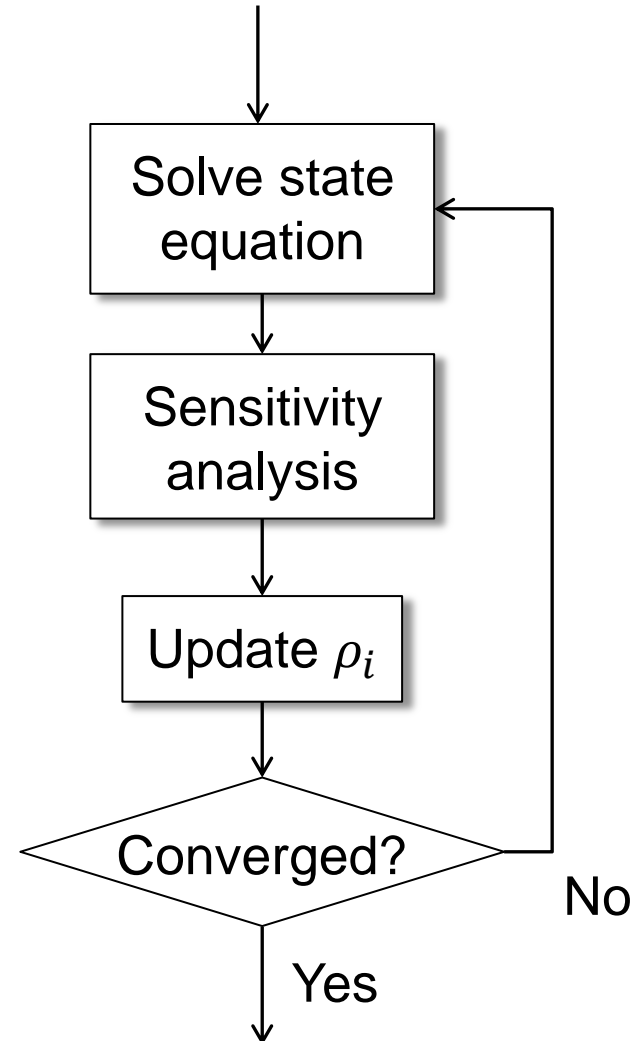
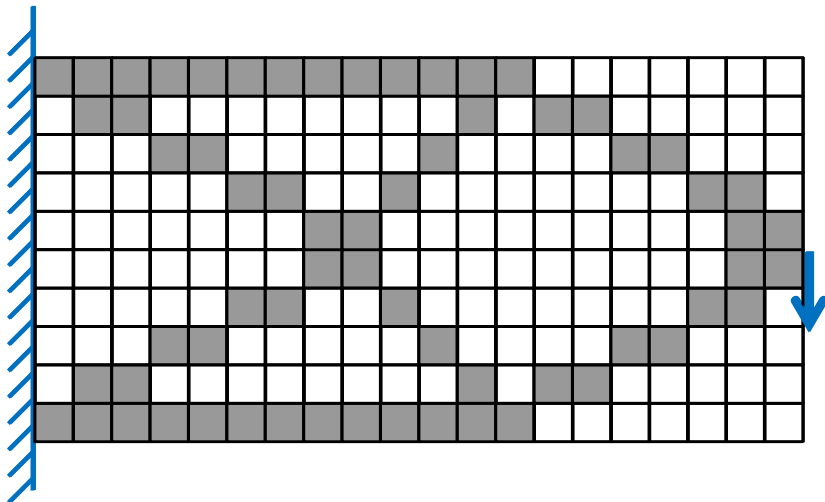
Natural convection
Alexandersen et al. 2016



Fluid flow
Maute & Pingen

A General Formulation

Minimize: $c(\rho)$
Subject to: $\rho_i \in [0,1], \forall i$
 $g_i(\rho) \leq 0$



Outline

- Basics of Topology Optimization
- Topology Optimization for Additive Manufacturing

Additive Manufacturing: Complexity is free



TU Delft & MX3D, 2015



Joshua Harker

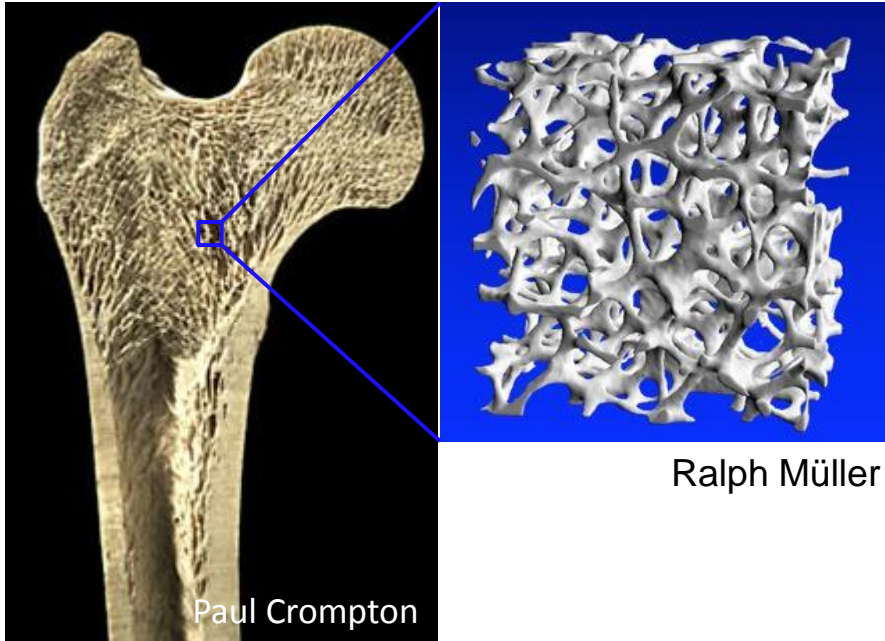


Scott Summit

Complexity is free? ... Not really!

- Printer resolution: Minimum geometric feature size
- Layer-upon-layer: Supports for overhang region
- Shell-infill composite

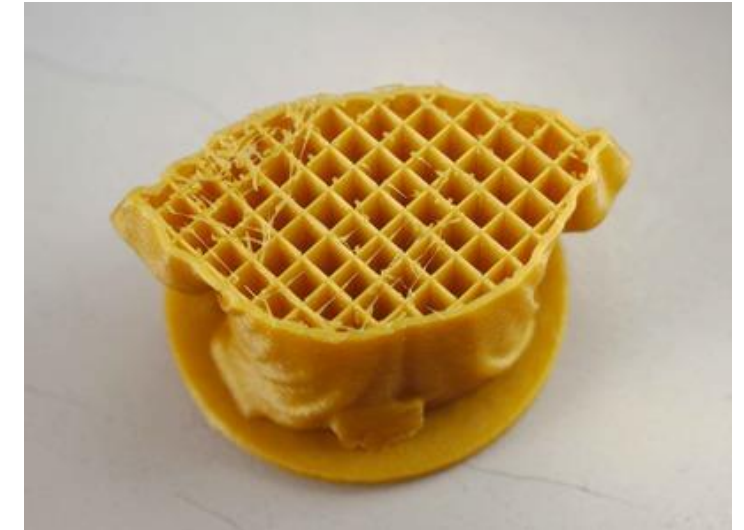
Tiny details



Supports



Infill

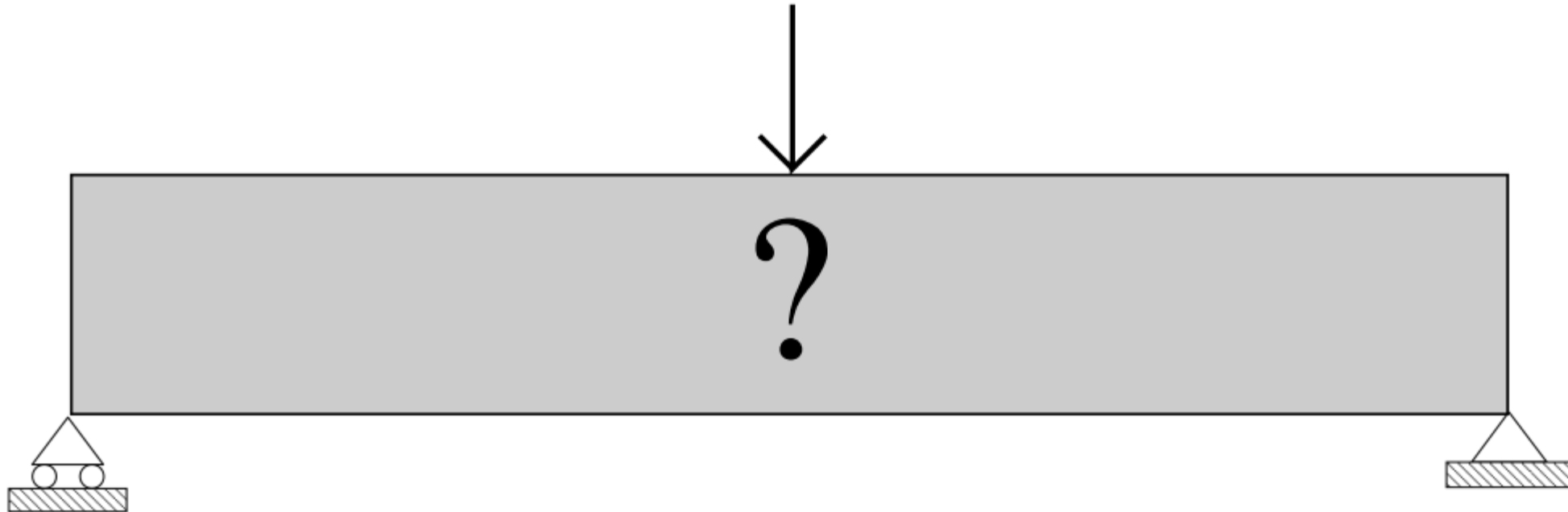


Outline

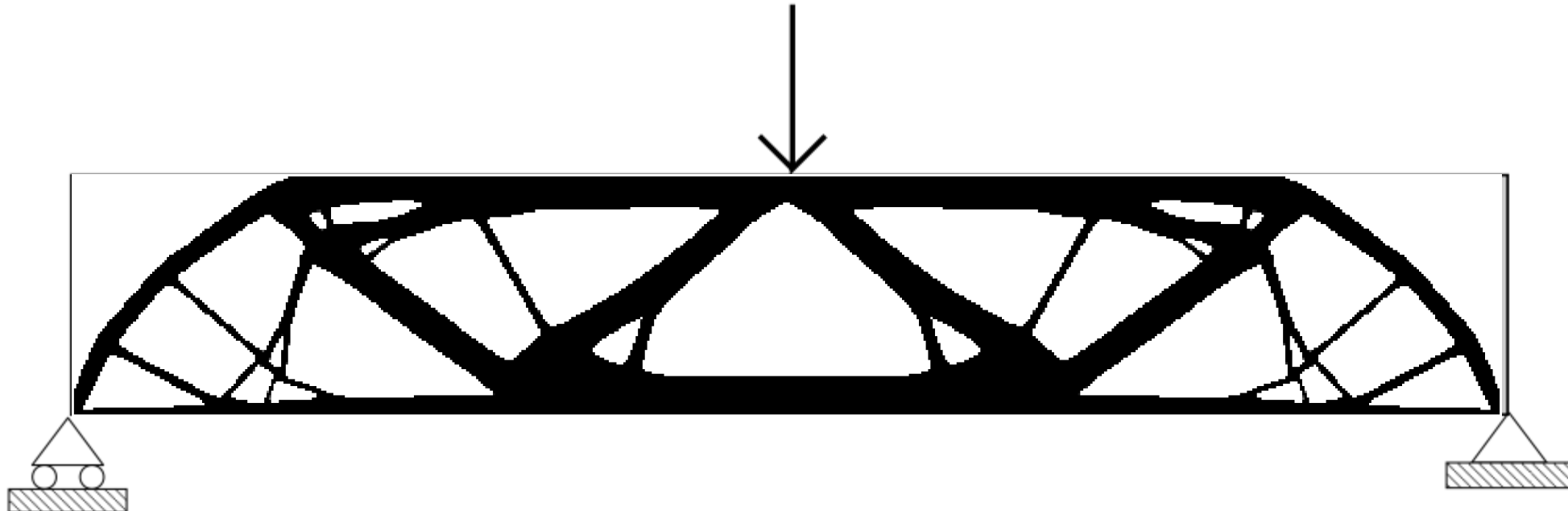
- Basics of Topology Optimization
- Topology Optimization for Additive Manufacturing
 - Geometric feature control by **density filters**
 - Geometric feature control by **alternative parameterizations**

Test case

- Messerschmidt-Bölkow-Blohm (MBB) beam



Test case

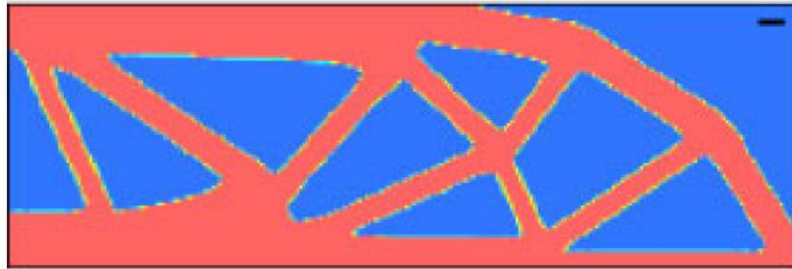


Geometric feature control by density filters (An incomplete list)

Reference



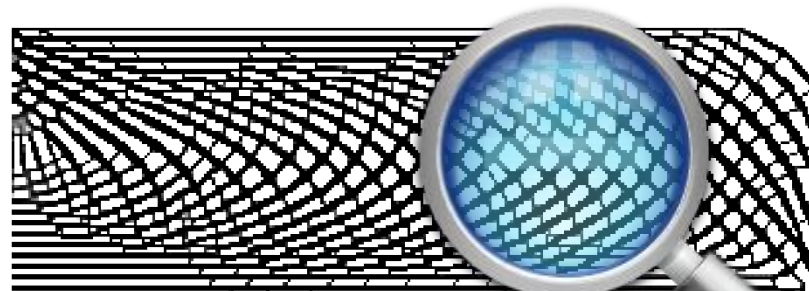
Minimum feature size, Guest'04



Coating structure, Clausen'15

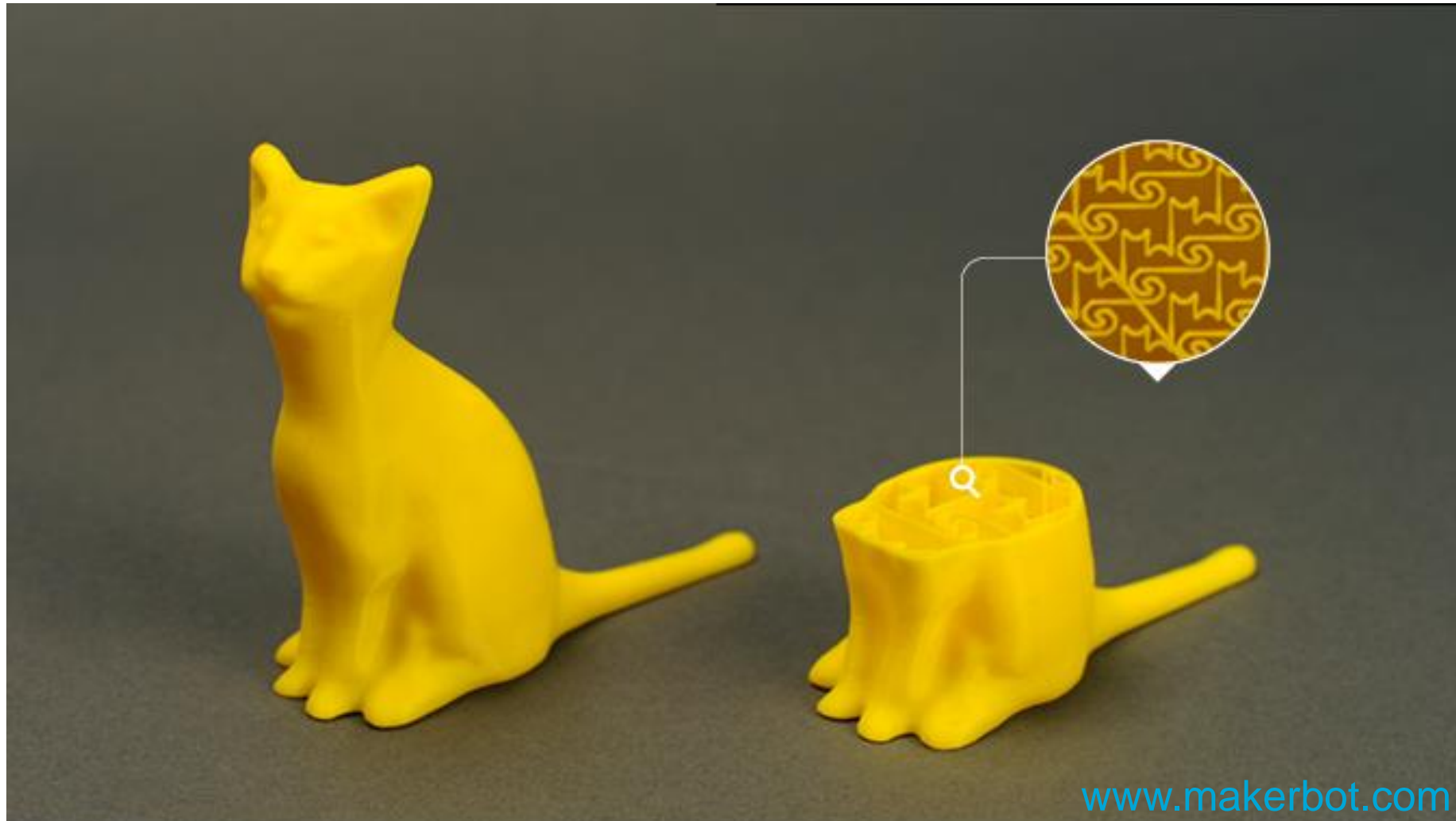


Self-supporting design, Langelaar'16



Porous infill, Wu'16

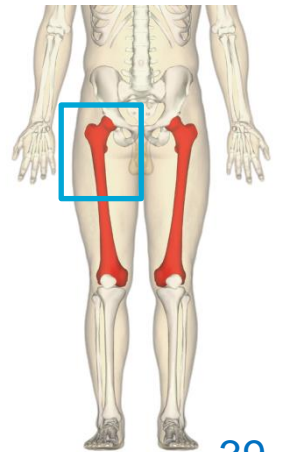
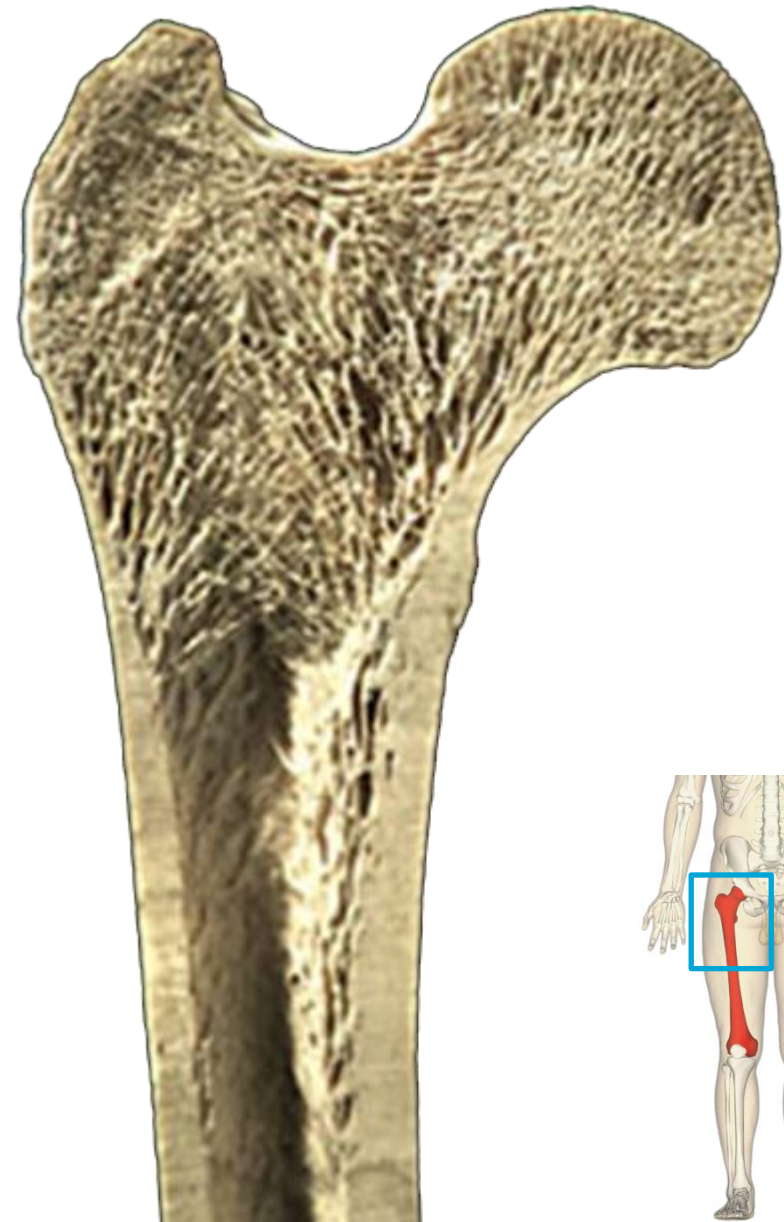
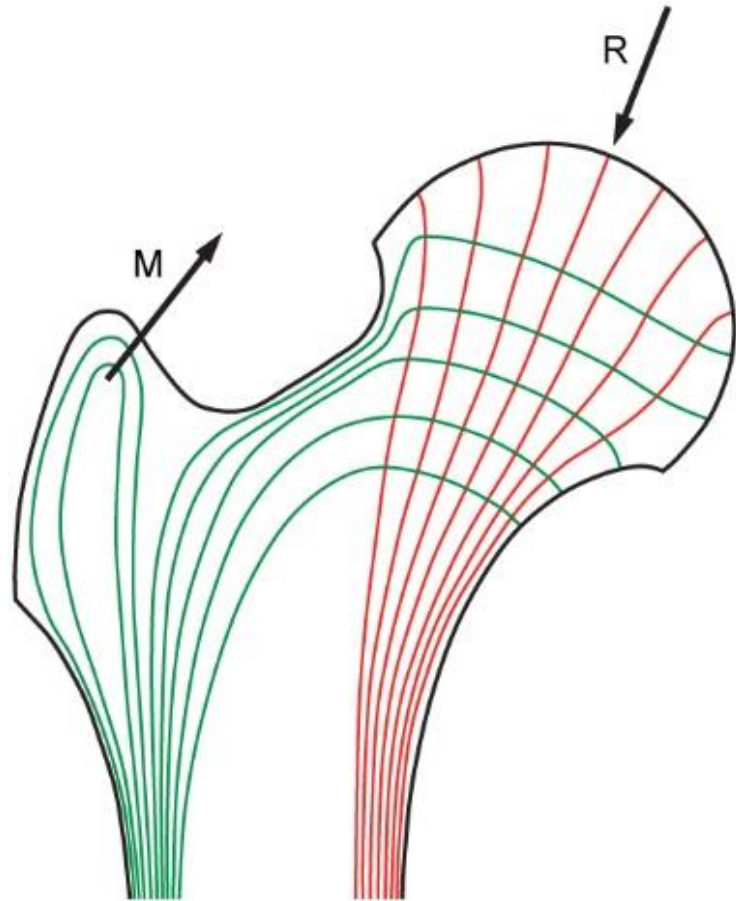
Infill in 3D Printing: Regular Structures



3dplatform.com

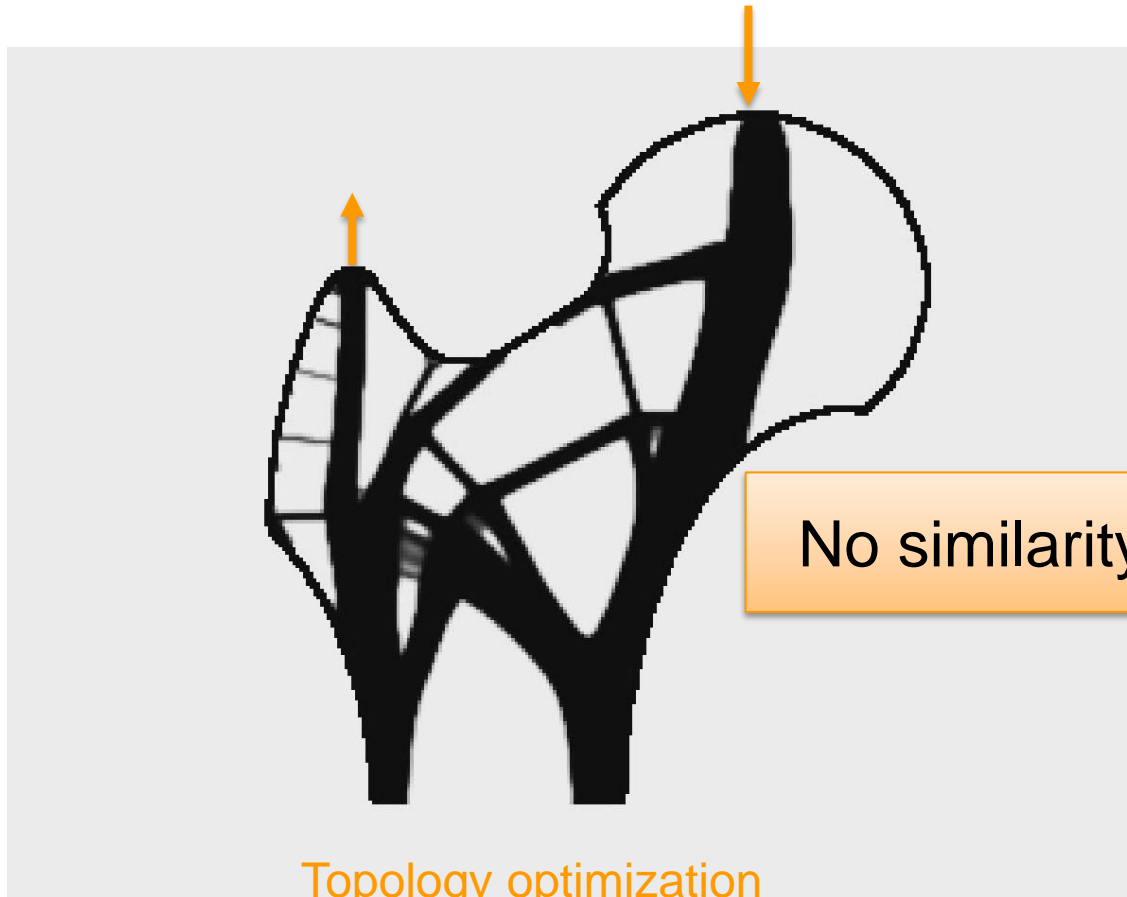


Infill in Bone: Porous Structures

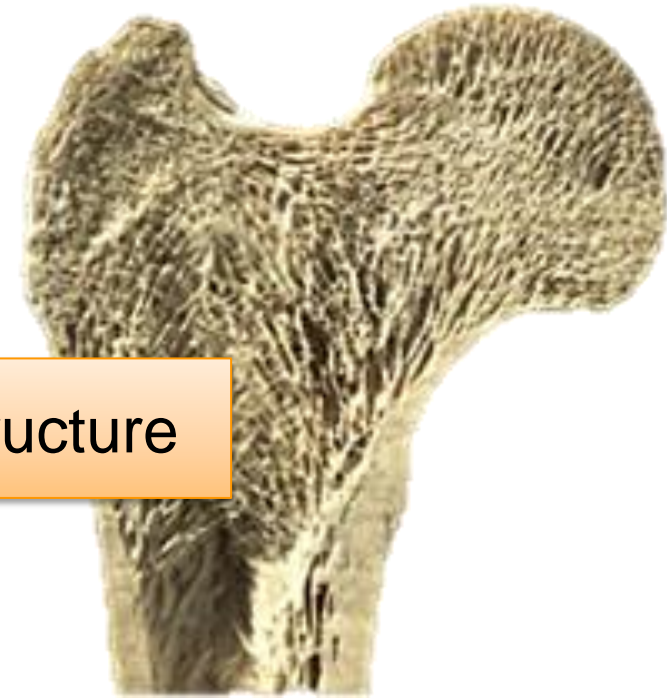


Can we apply the principle of bone to 3D printing?

Topology Optimization Applied to Design Infill



No similarity in structure



Topology Optimization Applied to Design Infill

- Materials accumulate to “important” regions
- The **total** volume $\sum_i \rho_i v_i \leq V_0$ does not restrict local material distribution



Infill by standard
topology optimization

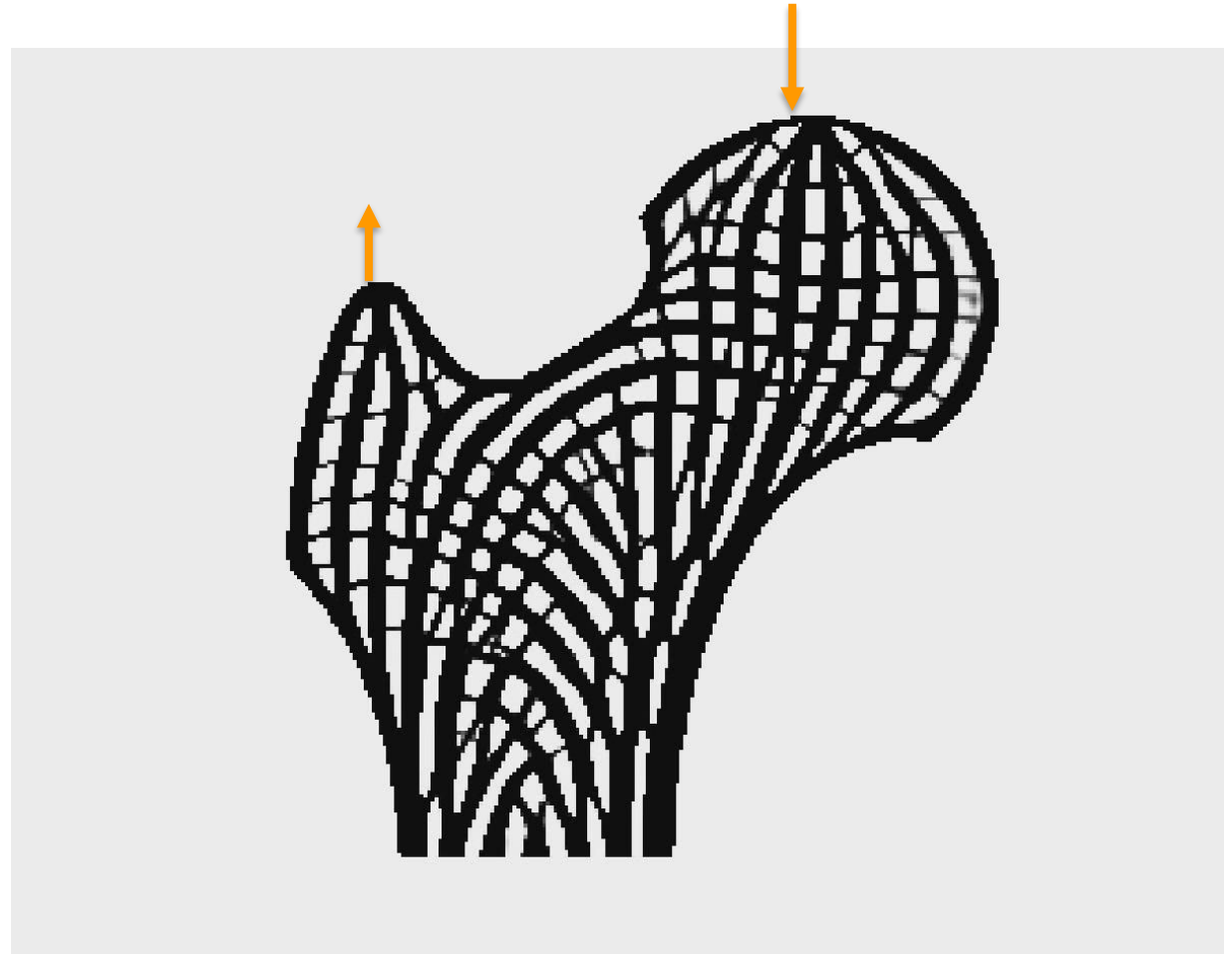


Infill in the bone

Bone-like Infill in 2D



Cross-section of a human femur



Approaching Bone-like Structures: The Idea

- Impose **local constraints** to avoid fully solid regions

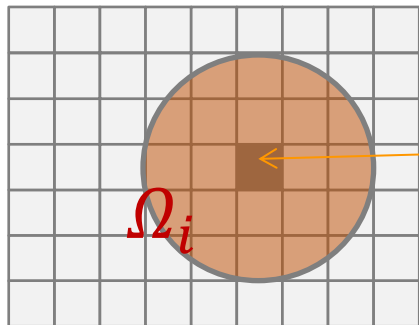
Min: $c = \frac{1}{2} U^T K U$

s.t. : $K U = F$

$\rho_i \in [0,1], \forall i$

~~$\sum_i \rho_i \leq V_0$~~

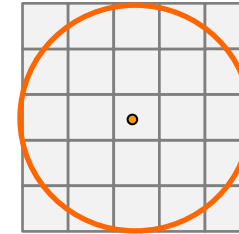
$\hat{\rho}_i \leq \alpha, \forall i$



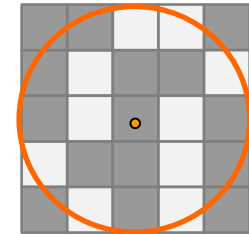
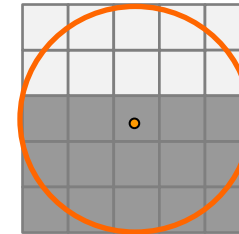
$$\hat{\rho}_i = \frac{\sum_{j \in \Omega_i} \rho_j}{\sum_{j \in \Omega_i} 1}$$

Local-volume measure

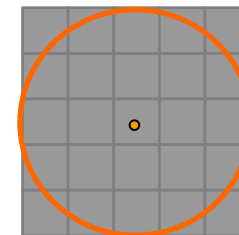
$\hat{\rho}_i = 0.0$



$\hat{\rho}_i = 0.6$

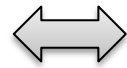


$\hat{\rho}_i = 1.0$

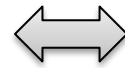


Constraints Aggregation (Reduce the Number of Constraints)

$$\hat{\rho}_i \leq \alpha, \forall i$$



$$\max_{i=1, \dots, n} |\hat{\rho}_i| \leq \alpha$$



$$\lim_{p \rightarrow \infty} \|\rho\|_p = (\sum_i (\hat{\rho}_i)^p)^{\frac{1}{p}} \leq \alpha$$

Too many constraints!

A single constraint
But non-differentiable

A single constraint
and differentiable
Approximated with $p = 16$

Optimization Process: The same as in the standard toptopt

- Impose **local constraints** to avoid fully solid regions

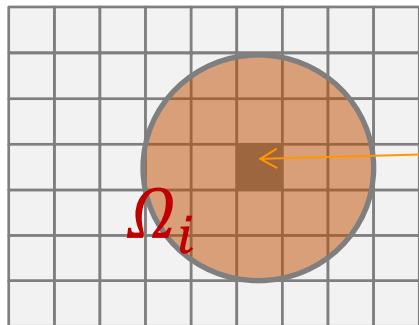
$$\text{Min: } c = \frac{1}{2} U^T K U$$

$$\text{s.t. : } K U = F$$

$$\rho_i \in [0,1], \forall i$$

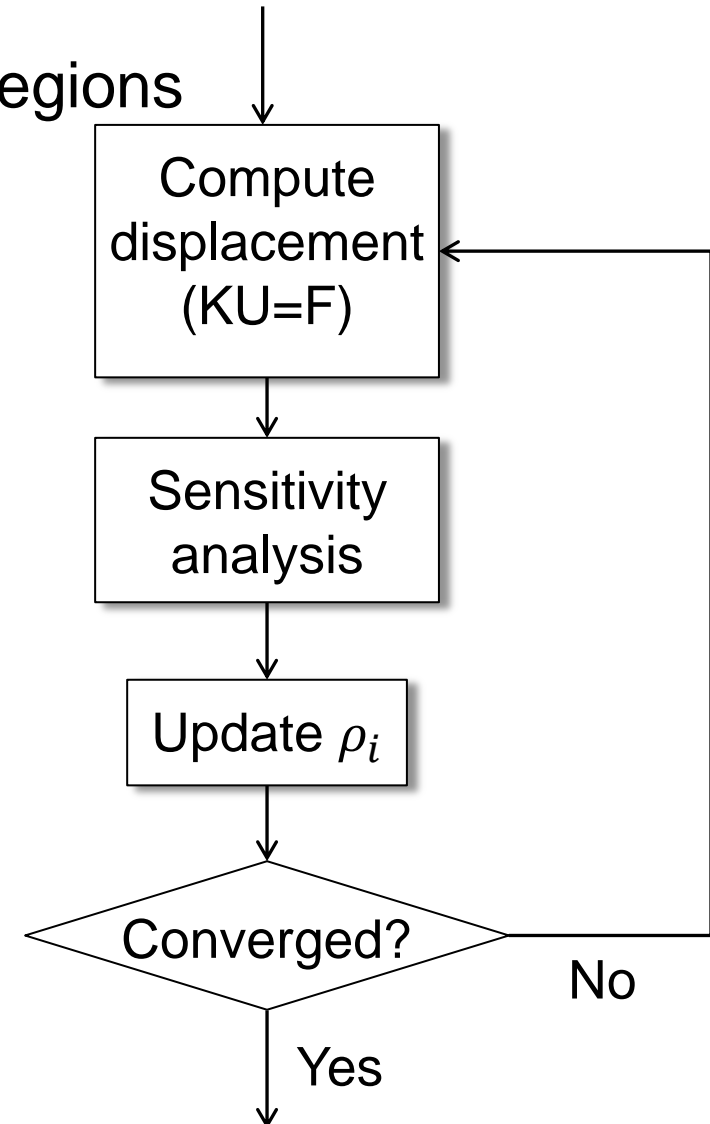
~~$$\sum_i \rho_i \leq V_0$$~~

$$\hat{\rho}_i \leq \alpha, \forall i$$

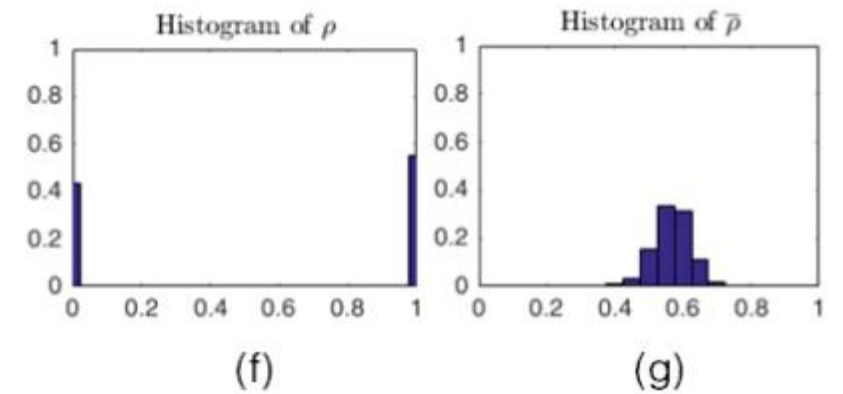
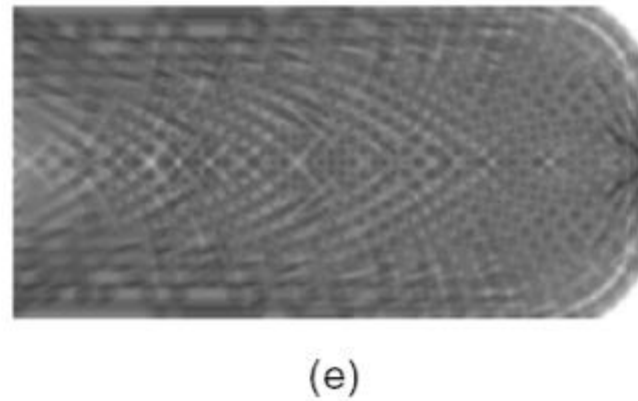
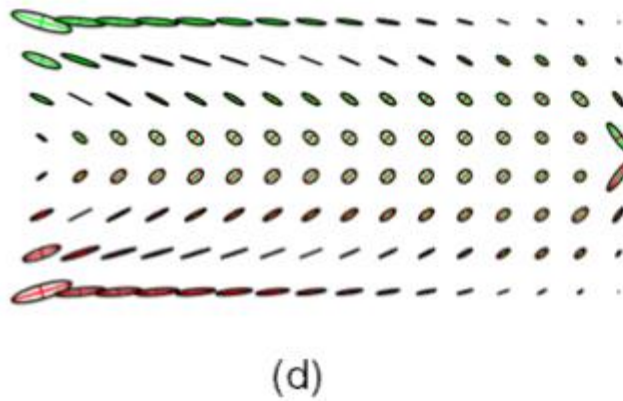
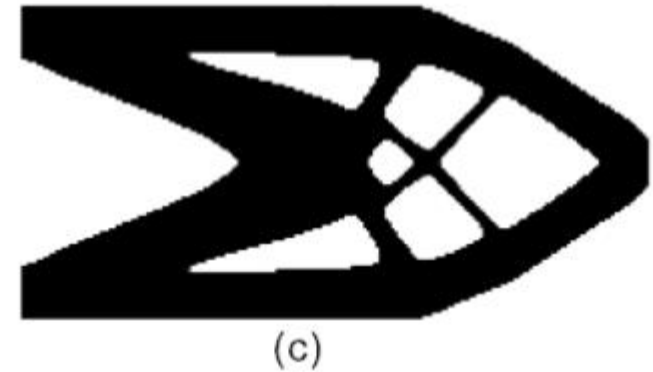
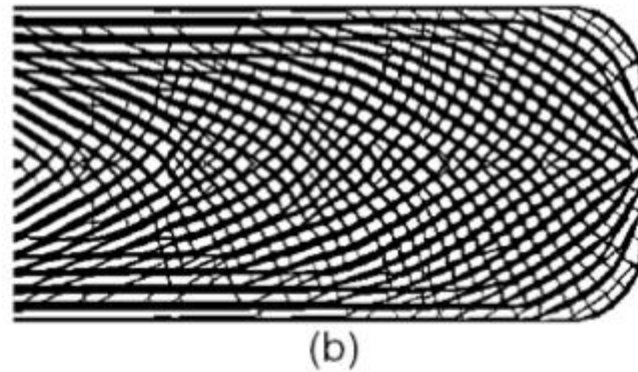
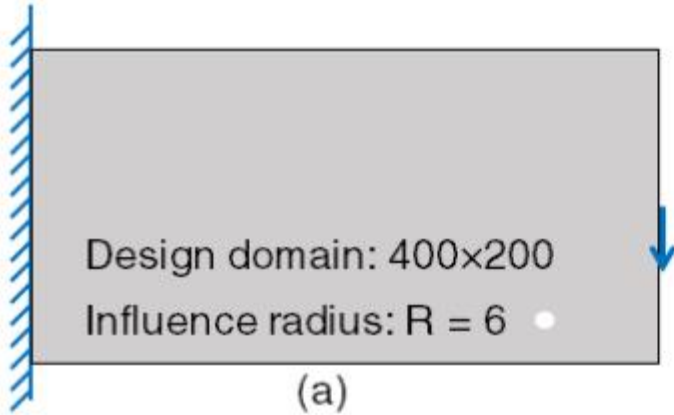


$$\hat{\rho}_i = \frac{\sum_{j \in \Omega_i} \rho_j}{\sum_{j \in \Omega_i} 1}$$

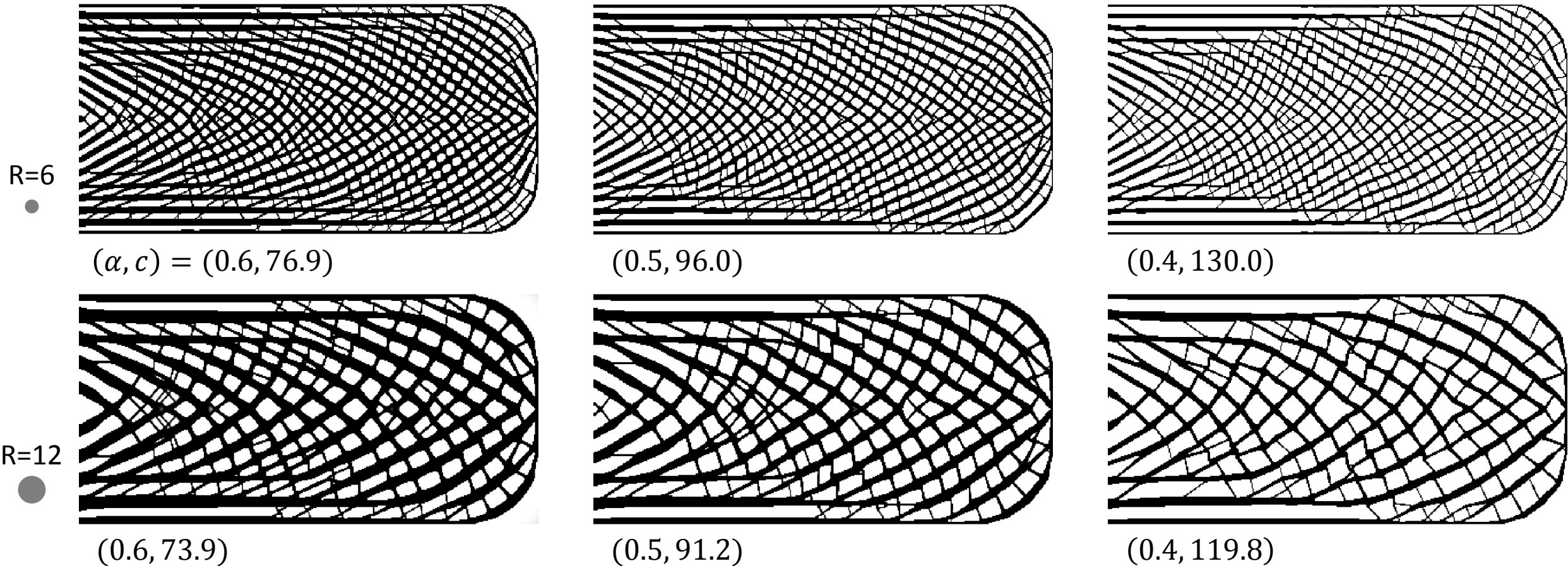
Local-volume measure



A Test Example

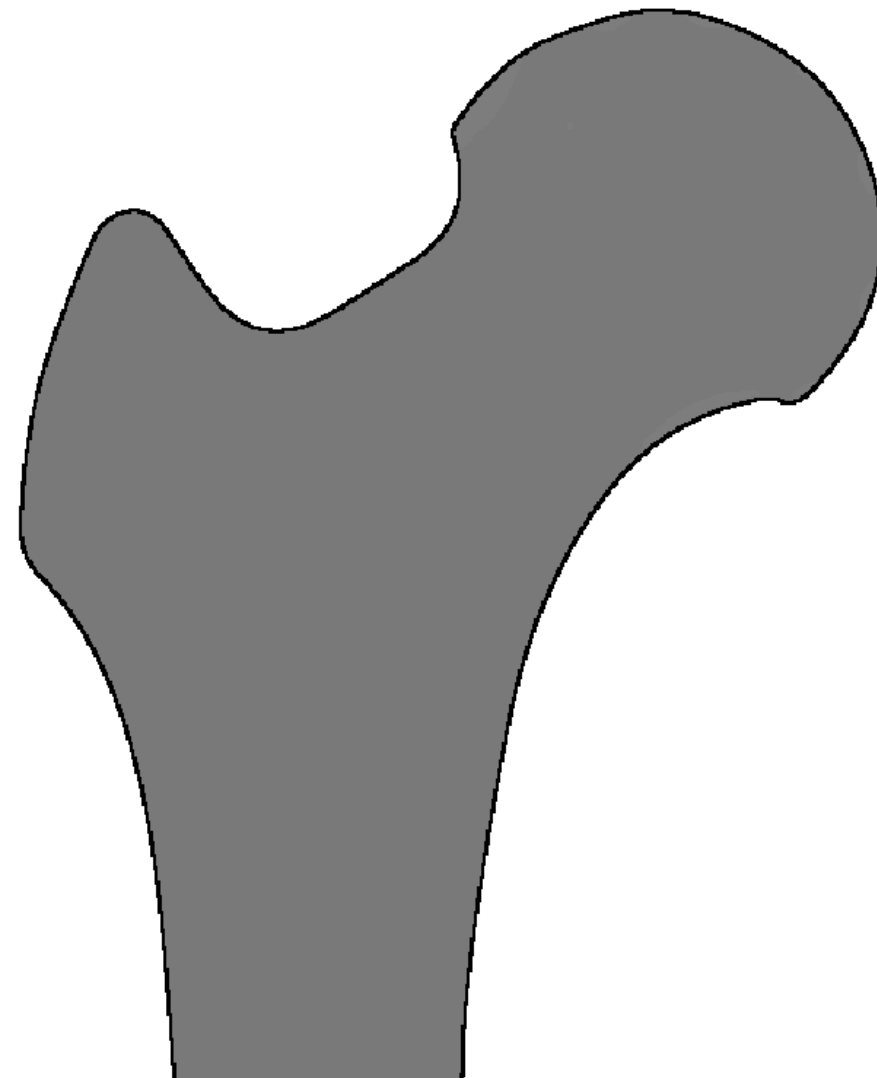
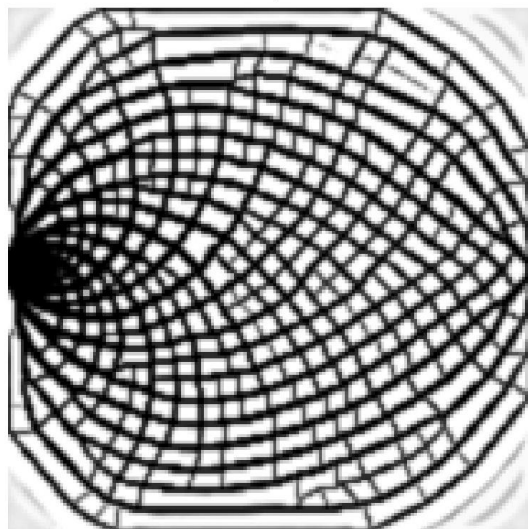
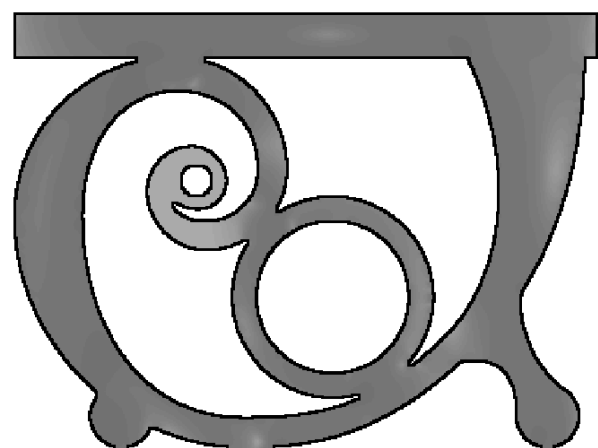
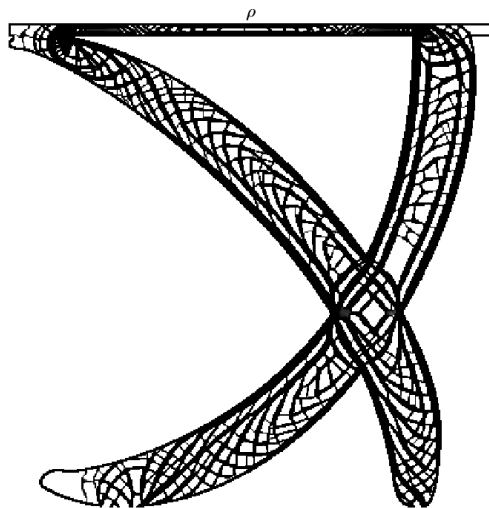
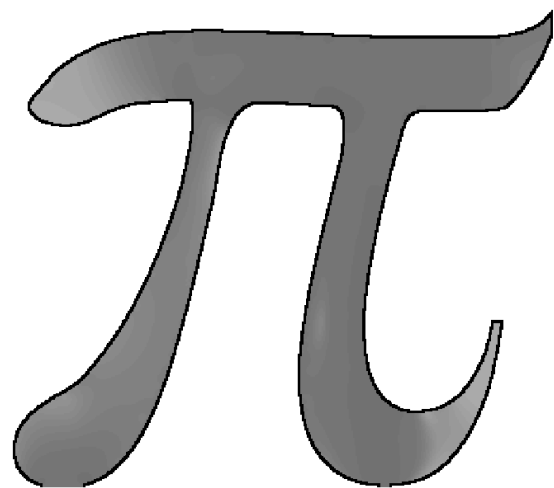


Effects of Filter Radius and Local Volume Upper Bound



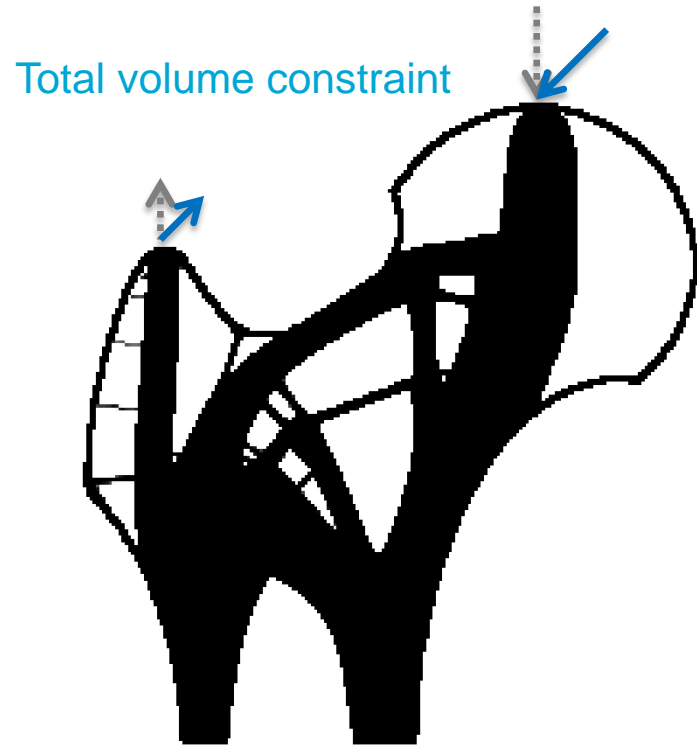
2D Animations

ρ

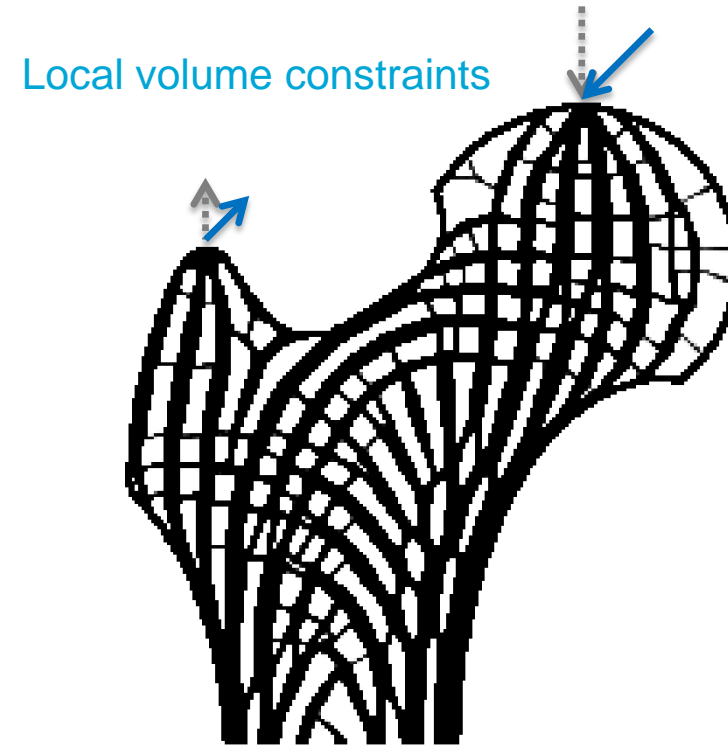


Robustness wrt. Force Variations

- Porous structures are significantly stiffer (126%) in case of **force variations**



$c = 30.54$
 $c' = 45.83$

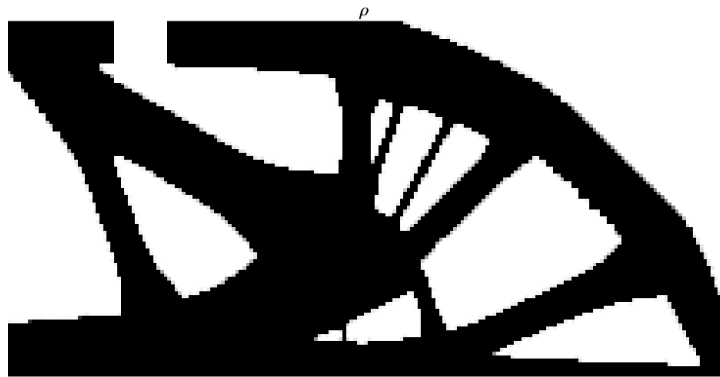


$c = 36.72$
 $c' = 36.23$

Robustness wrt. Material Deficiency

- Porous structures are significantly stiffer (180%) in case of **material deficiency**

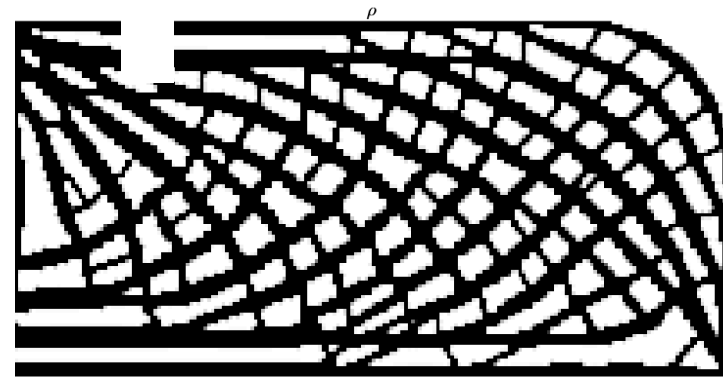
Total volume constraint



$$c = 76.83$$

$$c' = 242.77$$

Local volume constraints



$$c = 93.48$$

$$c' = 134.84$$

Bone-like Infill in 3D



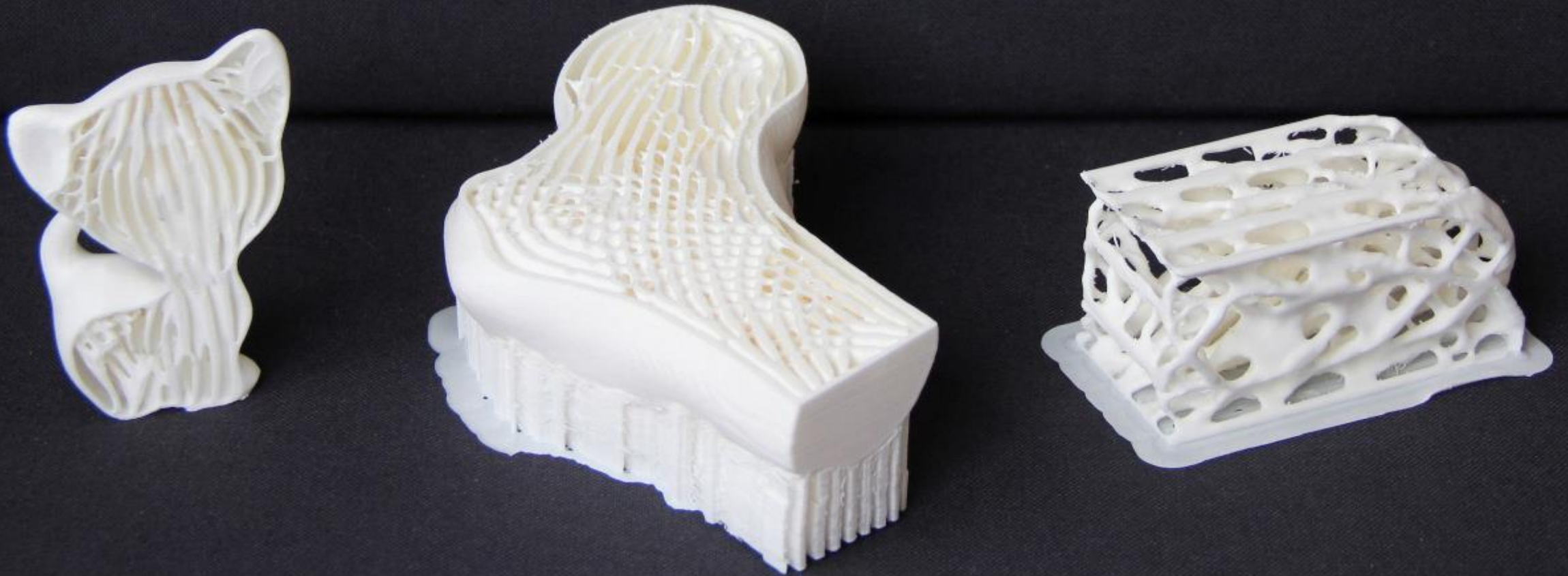
Infill in the bone



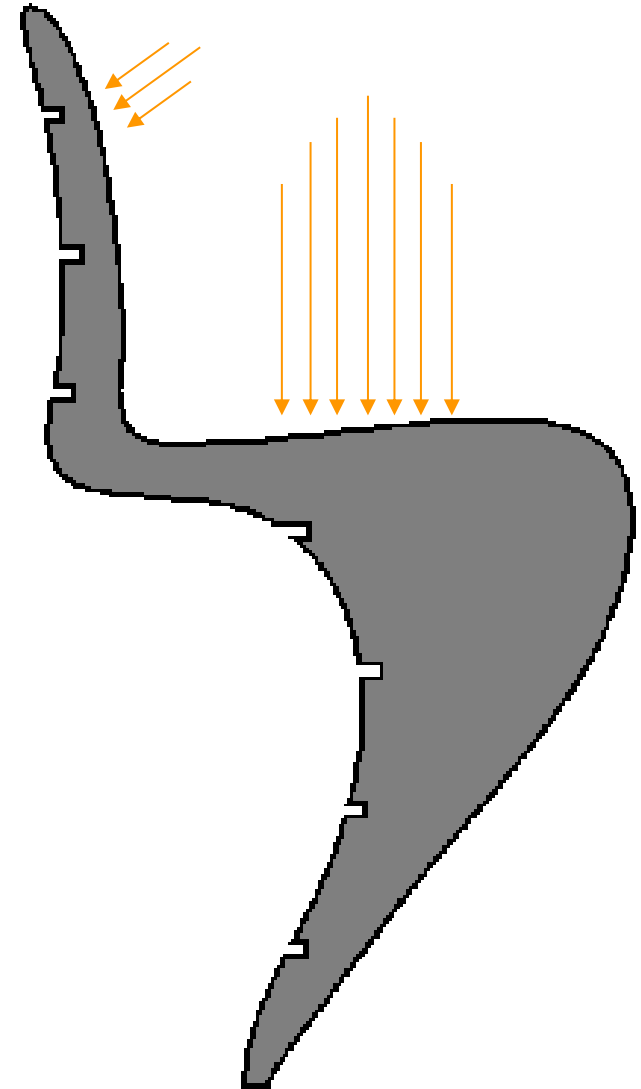
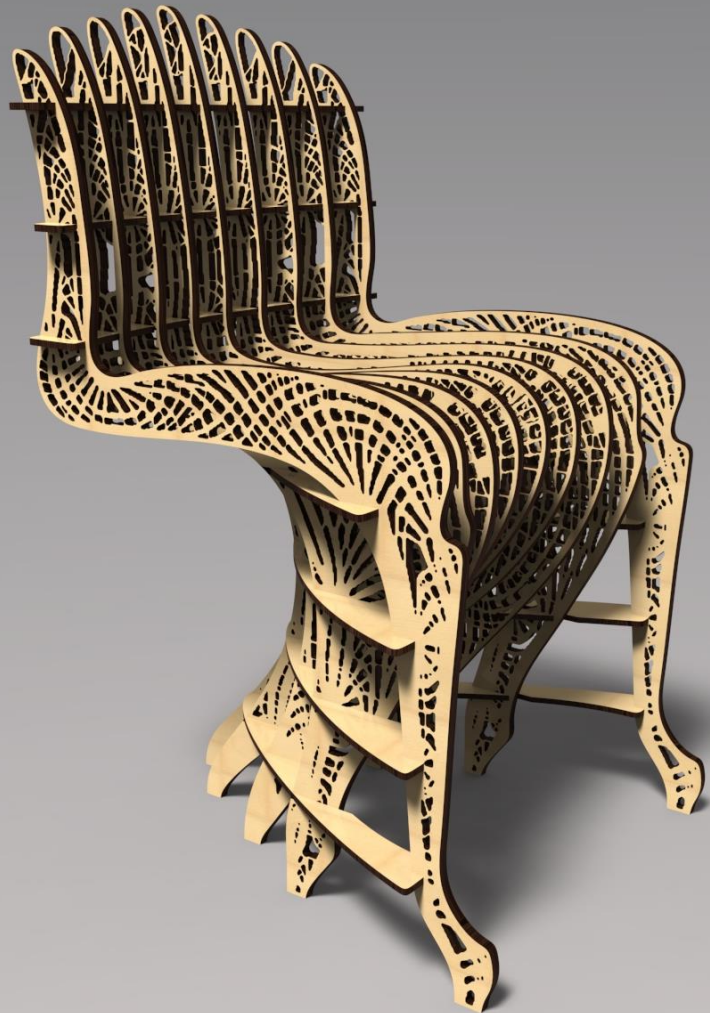
Optimized bone-like infill




FDM Prints



Chair





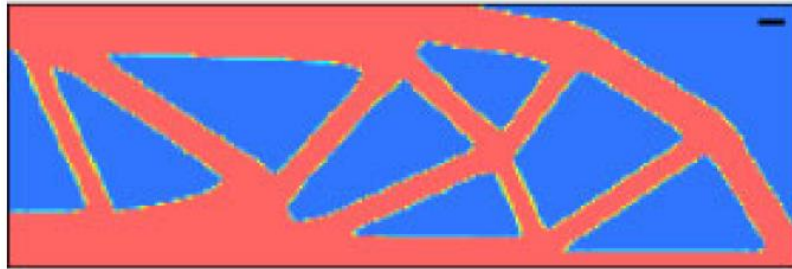
**It's what's on the inside
that matters**

Geometric feature control by density filters (An incomplete list)

Reference

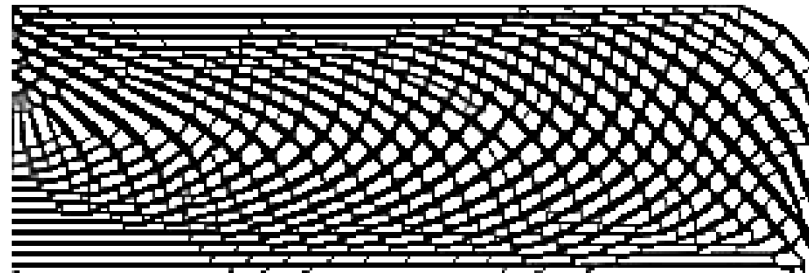


Minimum feature size, Guest'04



Self-supporting design, Langelaar'16

Coating structure, Clausen'15



Porous infill, Wu'16

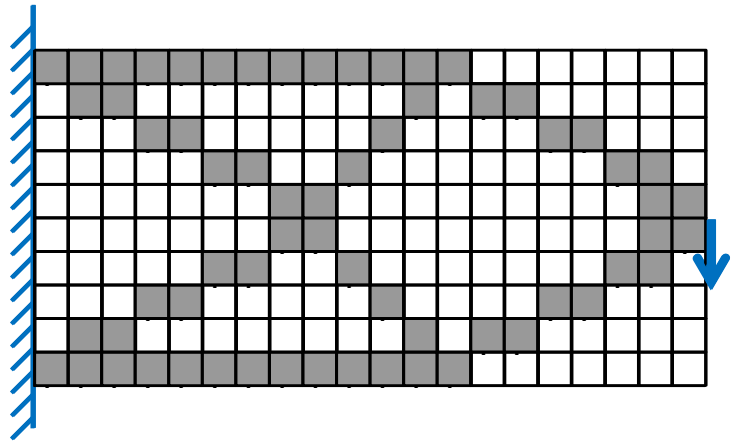
Concurrent Shell-Infill Optimization



Outline

- Basics of Topology Optimization
- Topology Optimization for Additive Manufacturing
 - Geometric feature control by **density filters**
 - Geometric feature control by **alternative parameterizations**

Geometric feature control by alternative parameterizations (An incomplete list)



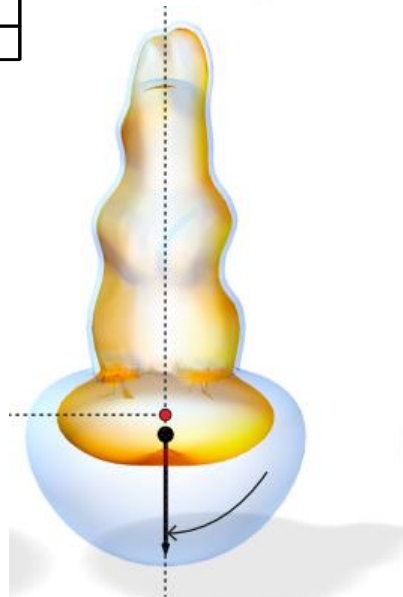
Reference: Voxel discretization



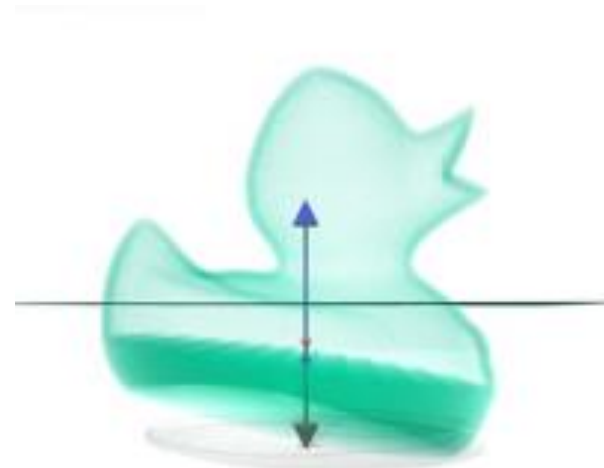
Skin-frame, Wang'13



Voronoi cells, Lu'14



Offset surfaces, Musialski'15



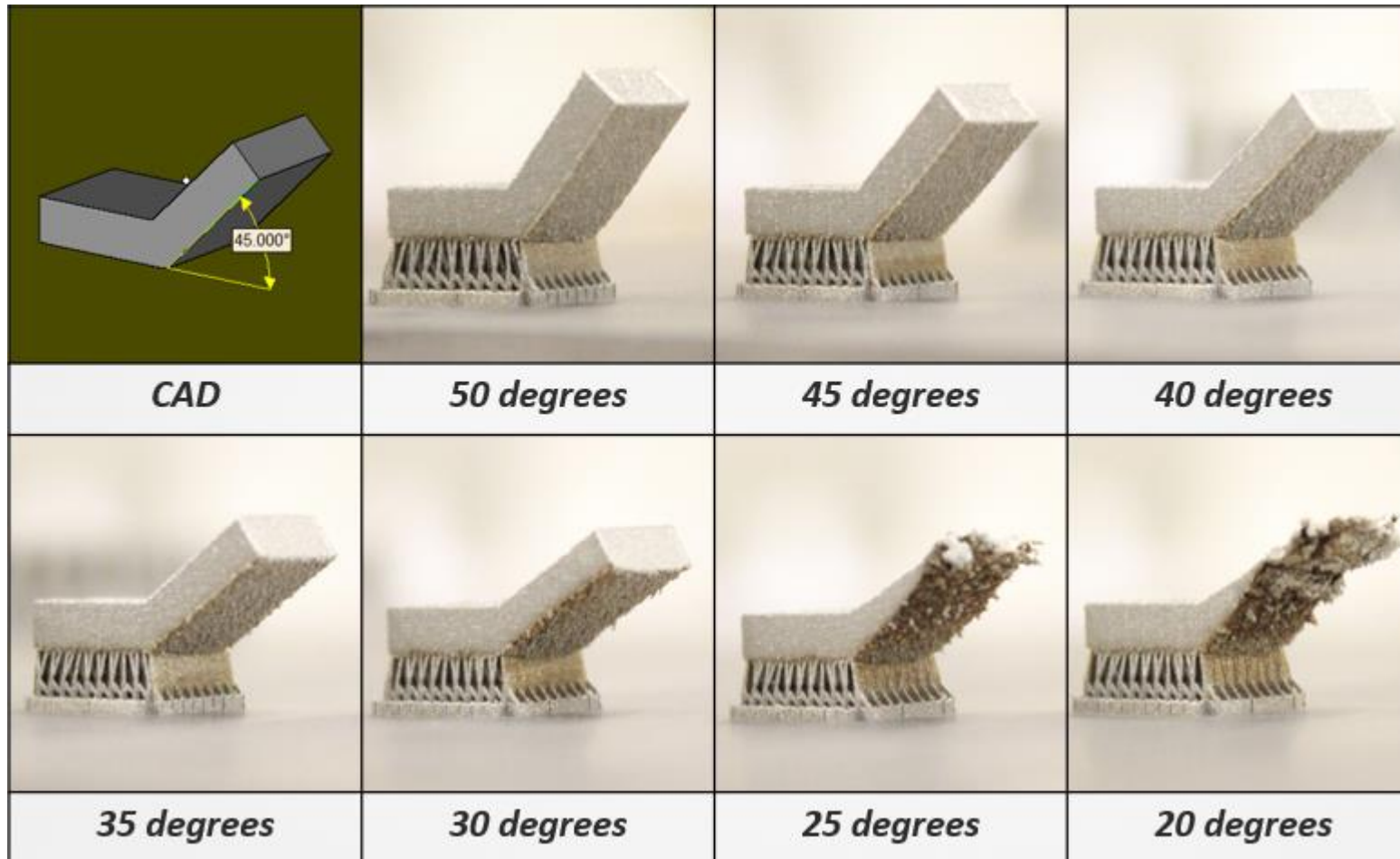
Ray representation, Wu'16



Adaptive rhombic, Wu'16

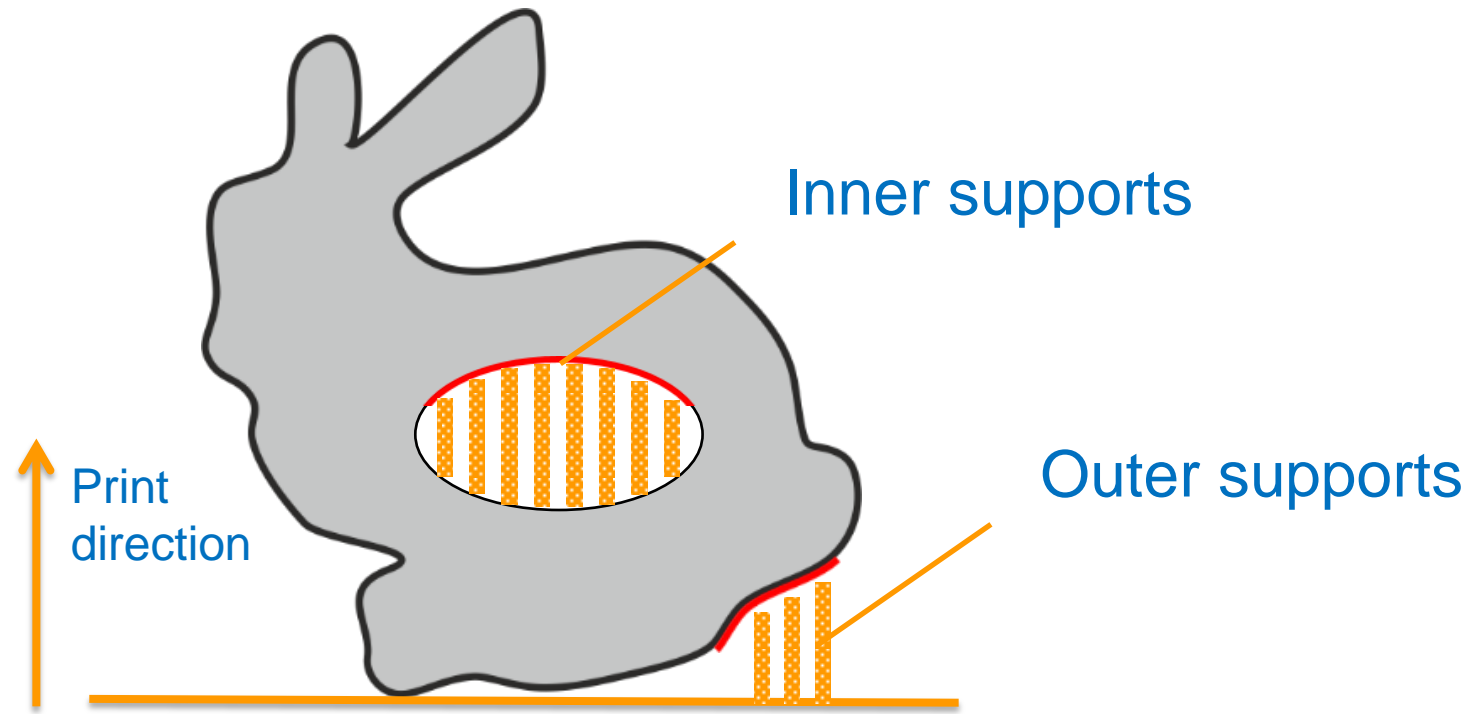
Overhang in Additive Manufacturing

- Support structures are needed beneath overhang surfaces

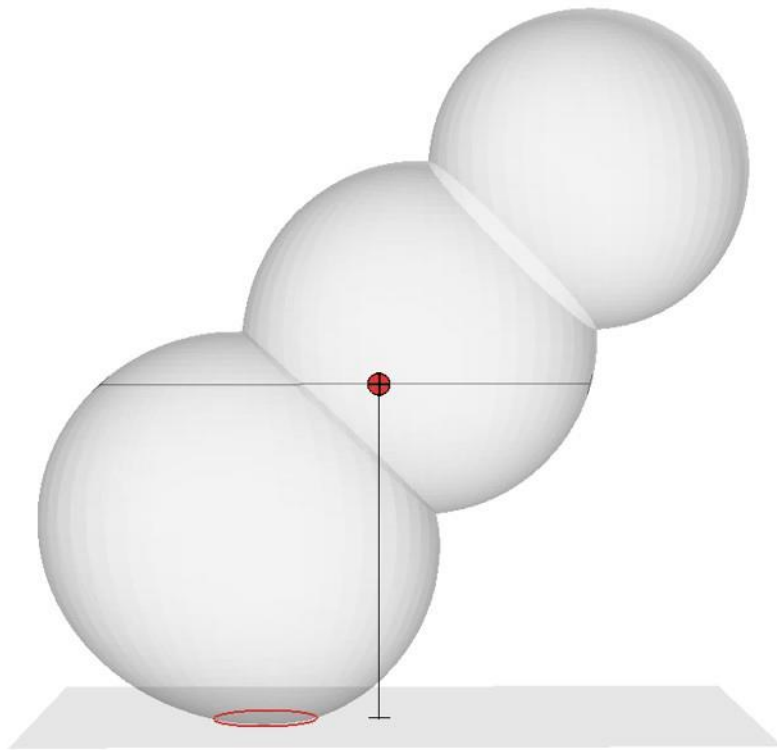


Support Structures in Cavities

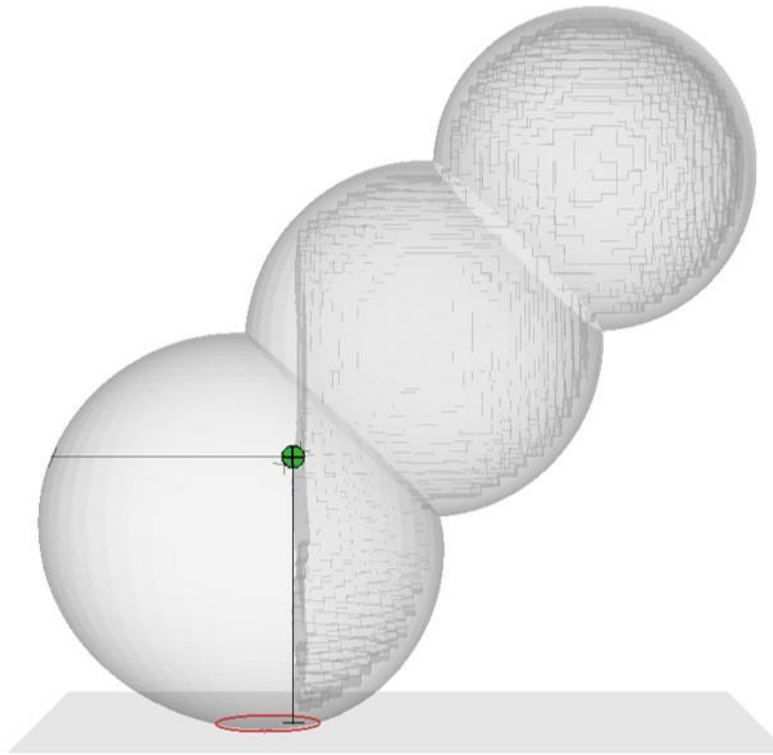
- Post-processing of **inner** supports is problematic



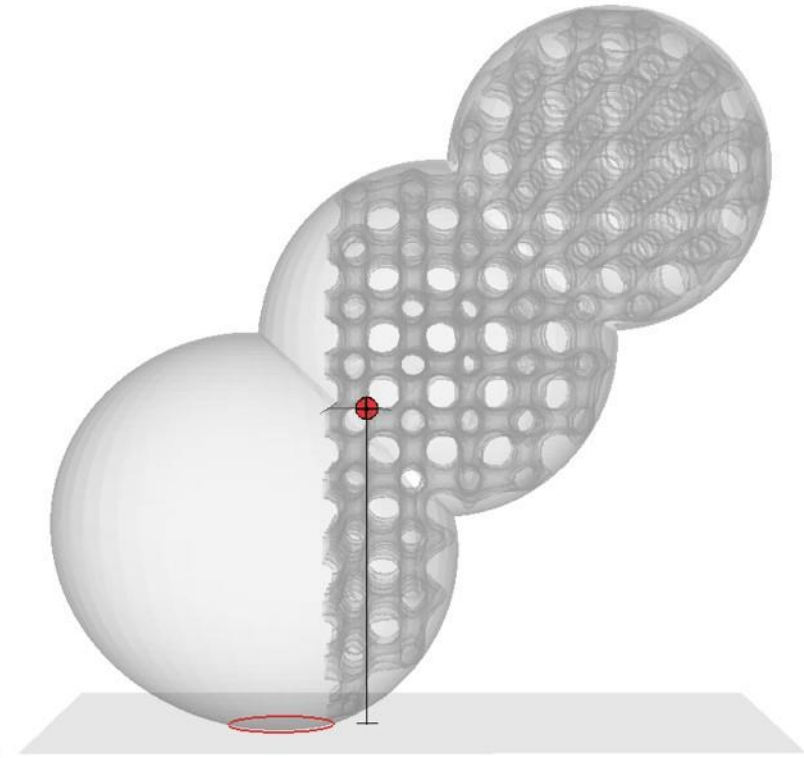
Infill & Optimization Shall Integrate



Solid,
Unbalanced



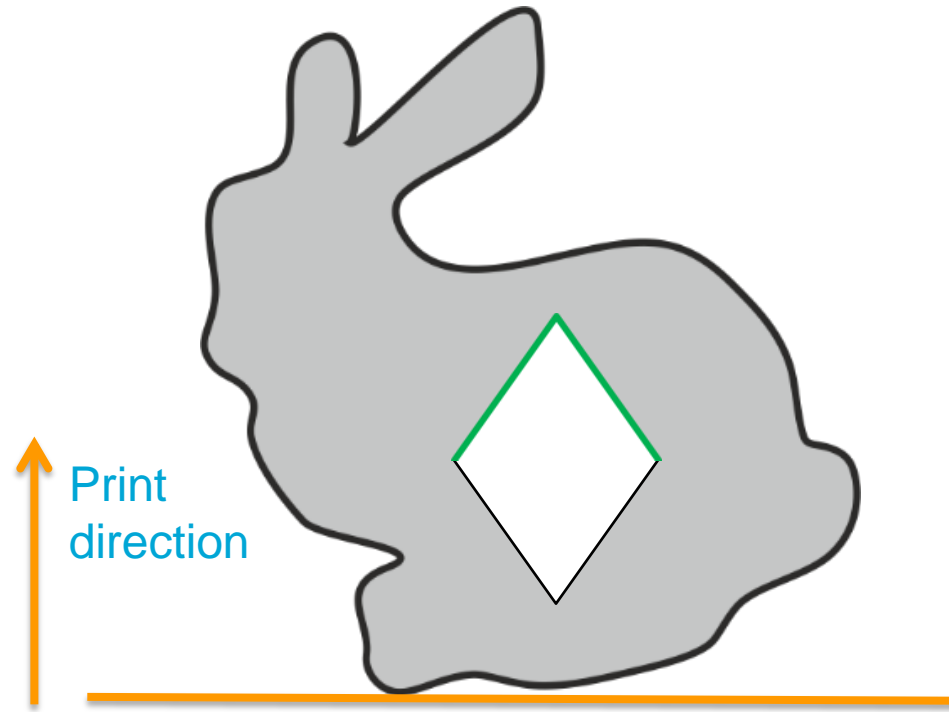
Optimized,
Balanced



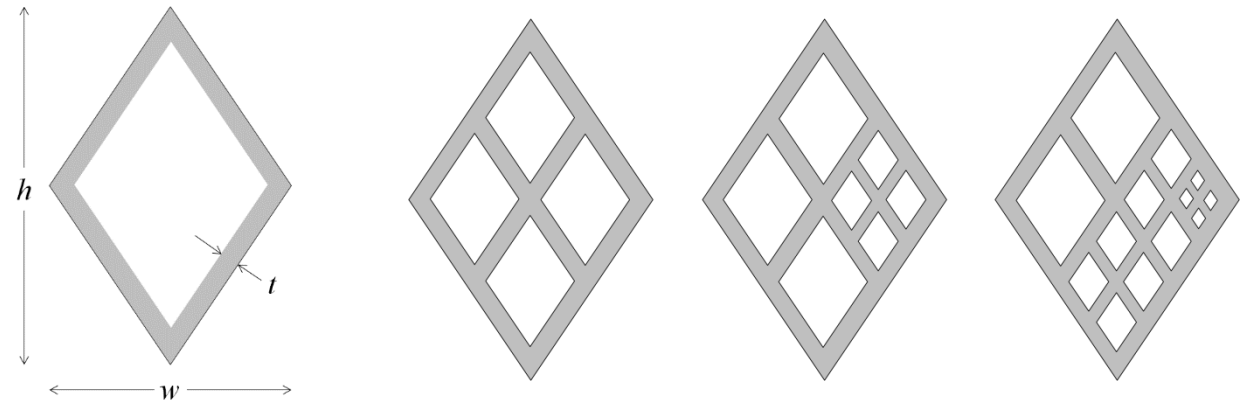
With infill,
Unbalanced

The Idea

- Rhombic cell: to ensure self-supporting
- Adaptive subdivision: as design variable in optimization

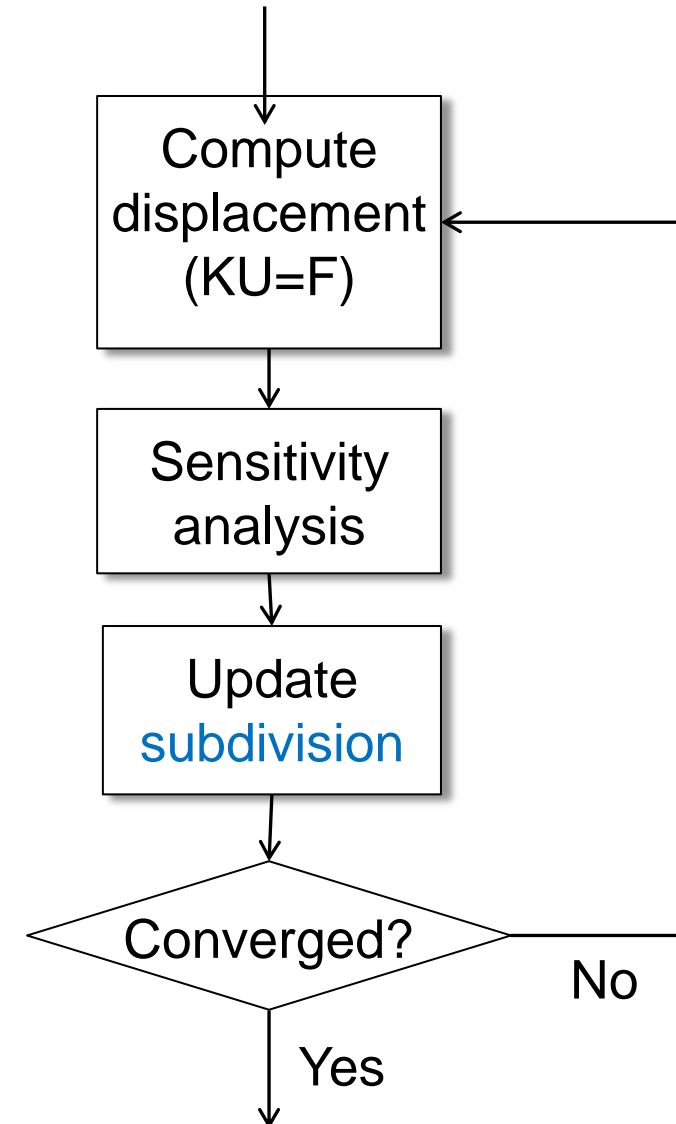
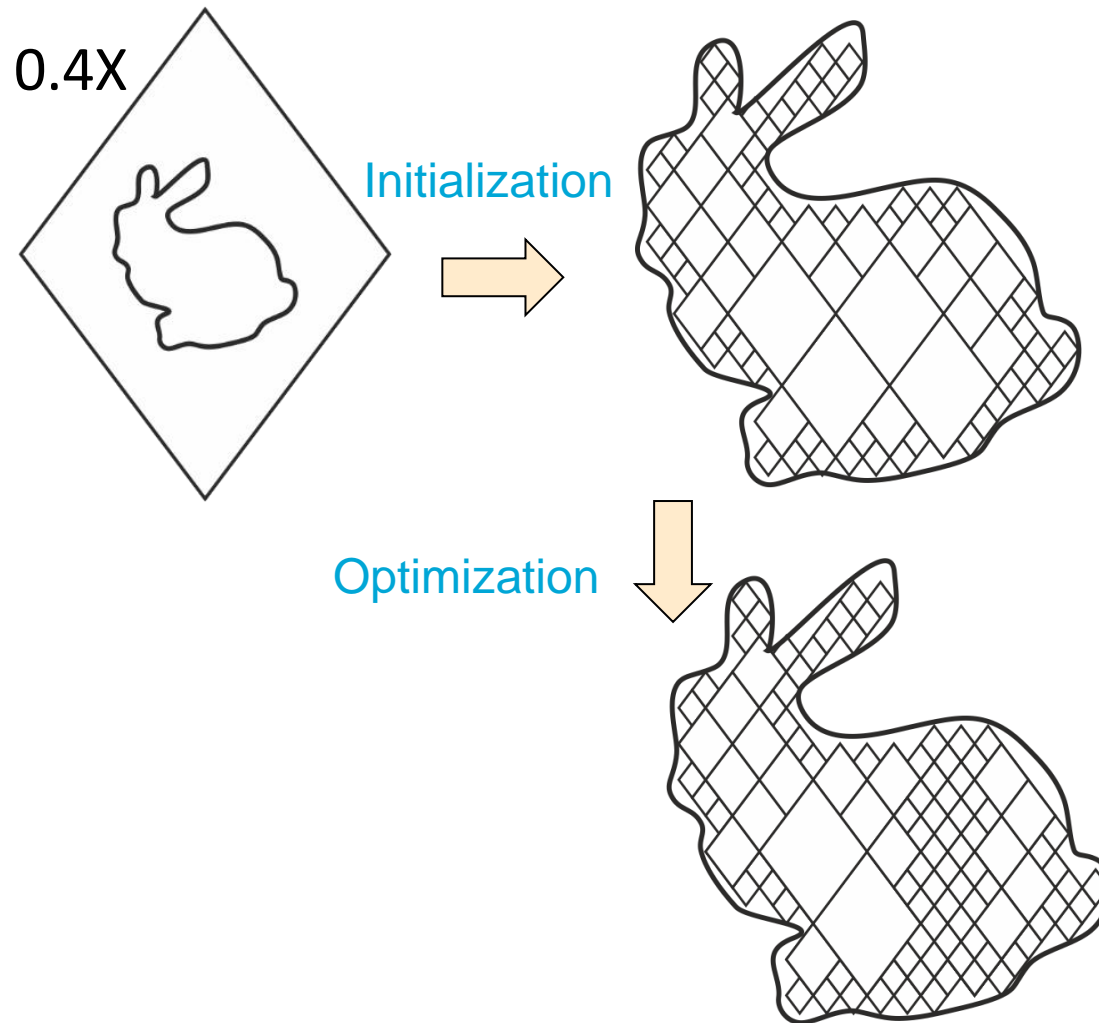


Rhombic cell



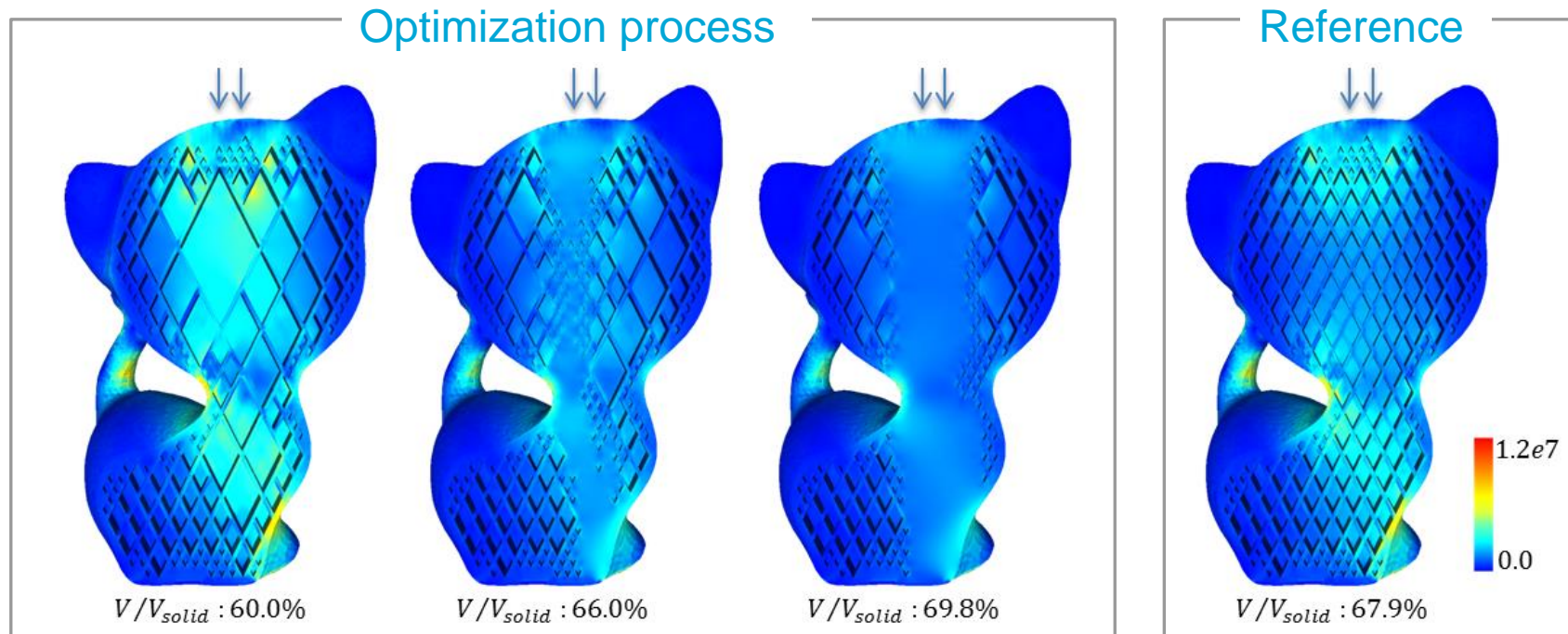
Adaptive subdivision

Self-Supporting Rhombic Infill: Workflow



Self-Supporting Rhombic Infill: Results

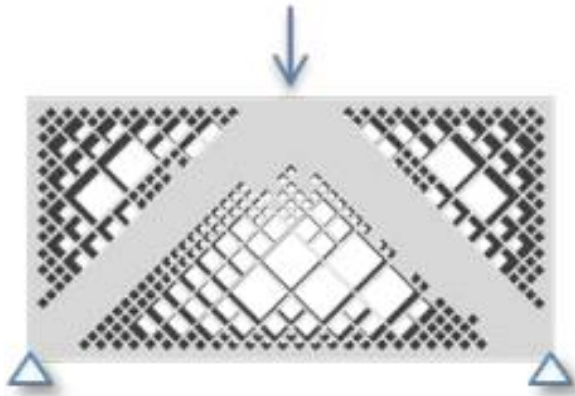
- Optimized mechanical properties, compared to regular infill
- No additional inner supports needed



Mechanical Tests

Under same force (62 N)

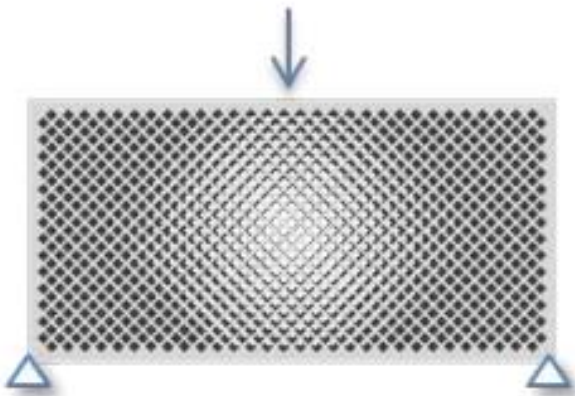
Under same displacement (3.0 mm)



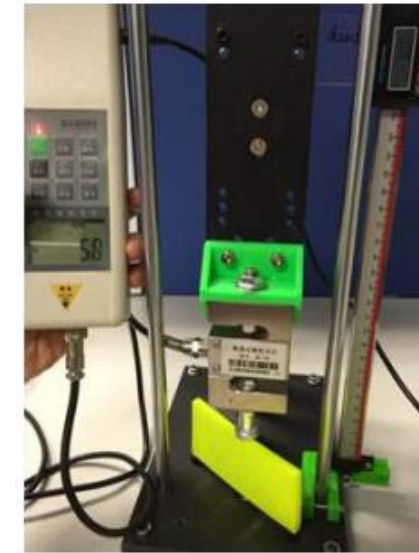
Dis.
2.11 mm



Force
90 N



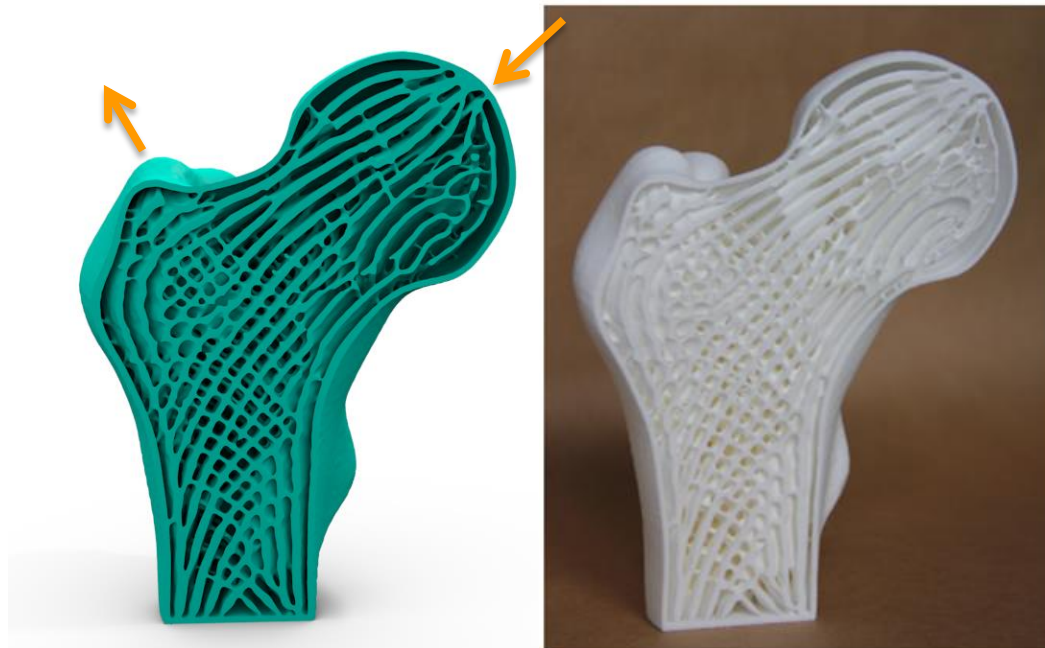
Dis.
4.08 mm



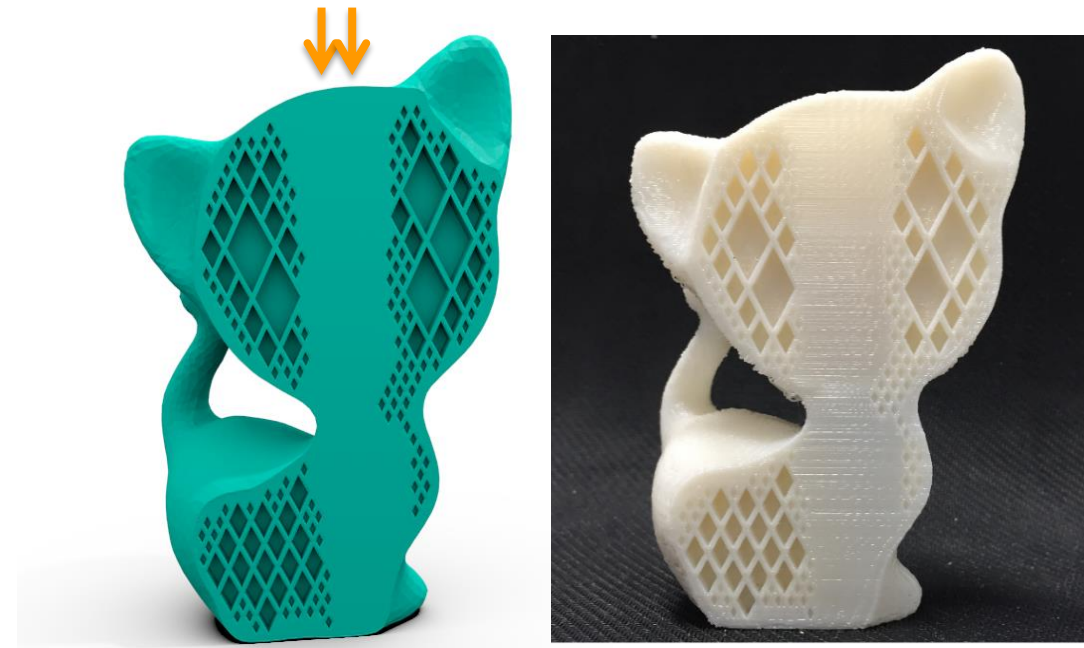
Force
58 N

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Bone-inspired infill



Self-supporting infill

Topology Optimization

- Lightweight
- Free-form shape
- Customization
- Mechanically optimized



Additive Manufacturing

- Customization
- Geometric complexity

Thank you for your attention!

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