



Computational Design and Fabrication of Soft Pneumatic Objects with Desired Deformations

Li-Ke Ma^{*1,2} Yizhong Zhang^{*2} Yang Liu² Kun Zhou³ Xin Tong²

* Joint first authors

1, Tsinghua University

2, Microsoft Research Asia

3, Zhejiang University

SA2017.SIGGRAPH.ORG

CONFERENCE 27 – 30 November 2017 EXHIBITION 28 – 30 November 2017 BITEC, Bangkok, Thailand

Sponsored by

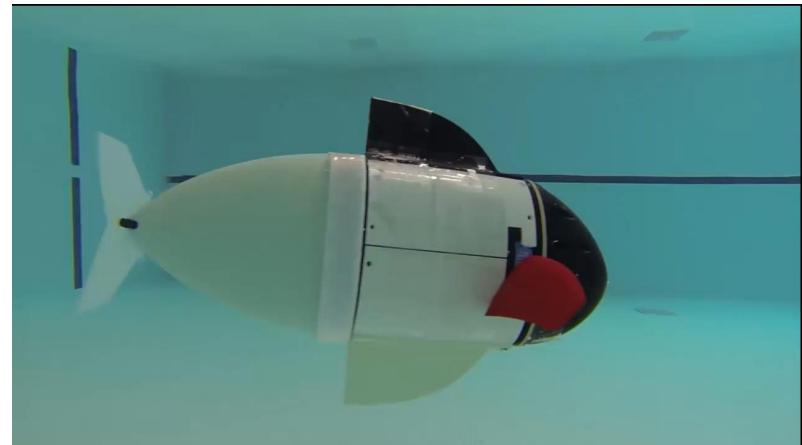
Pneumatic Soft Robotics

Industry Pneumatic Gripper



[Soft Robotics Inc]

Soft Robots



[Marchese et al. 2014, Ariel et al. 2016]

Our Goal

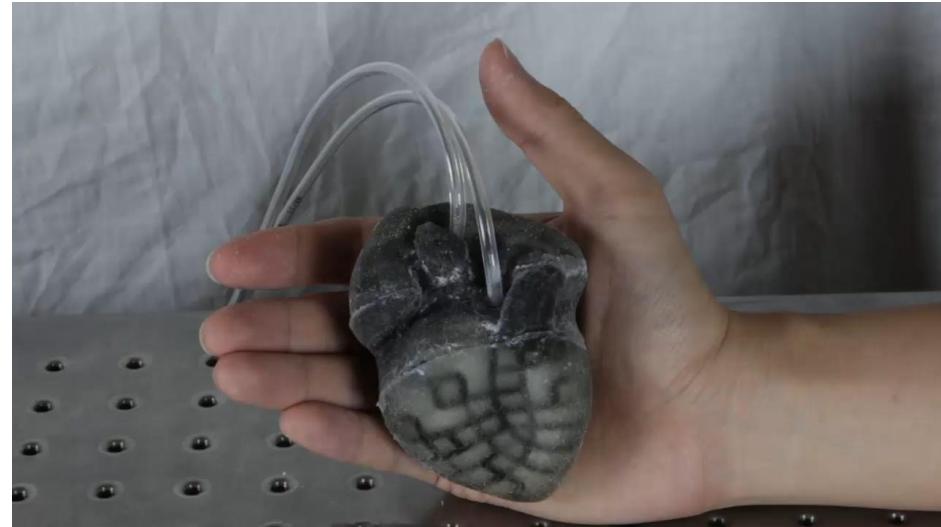


The digital deformable model

Our Goal



The digital deformable model



The fabricated deformable object

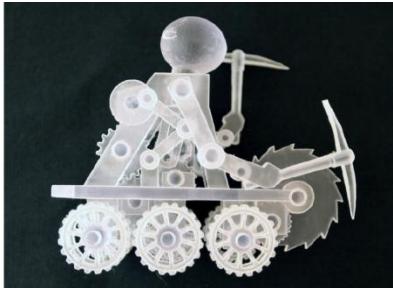
Related Works: Computational Fabrication



[Hasan et al. 2010]



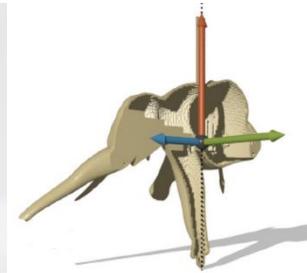
[Coros et al. 2013]



[Megaro et al. 2017]



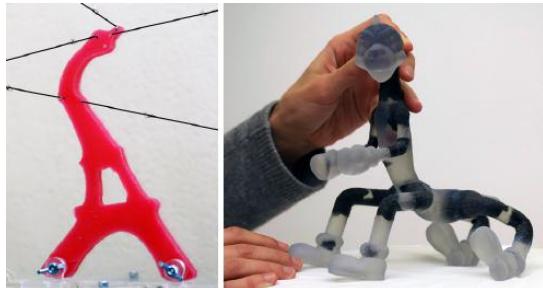
[Prévost et al. 2013]



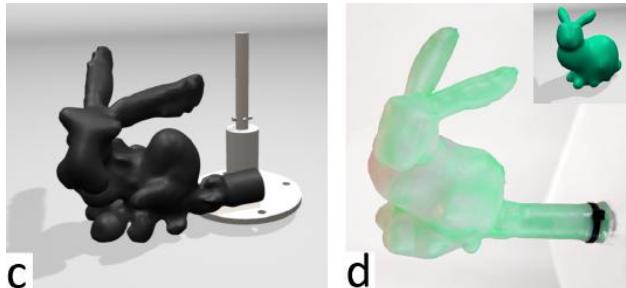
[Bächer et al. 2014]



Related Works: Flexible Object Fabrication



[Mélina et al. 2013]



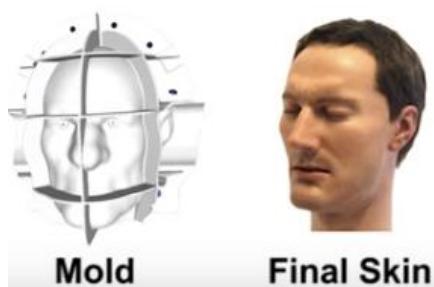
[Mélina et al. 2012]



[Schumacher et al. 2015]



[Chen et al. 2014]

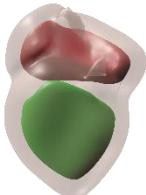


[Bickel et al. 2012]



[Chen et al. 2015]

Key Challenges



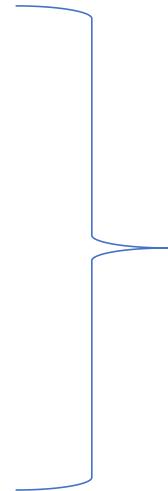
Chambers



Material distribution



Air pressure

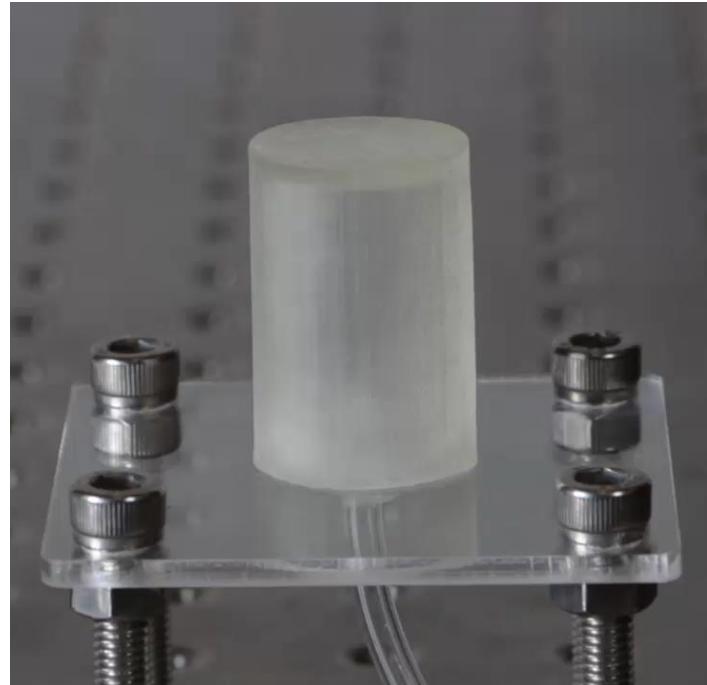


Deformation

Key idea: Chambers (empty space inside the model)

Inflation result in volume increase.

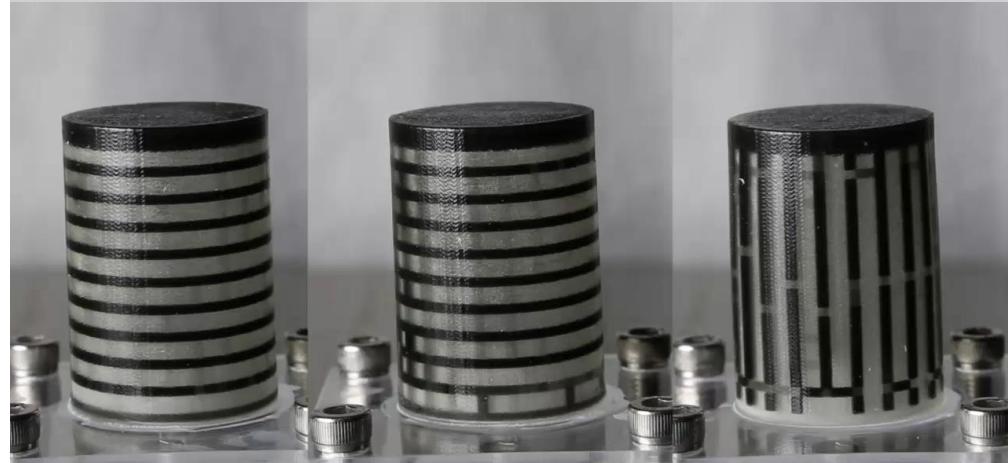
If deformation has volume increase,
we can set a chamber there.



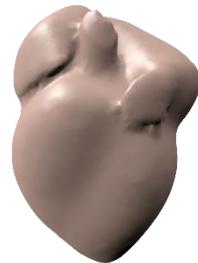
Key idea:
Wireframes



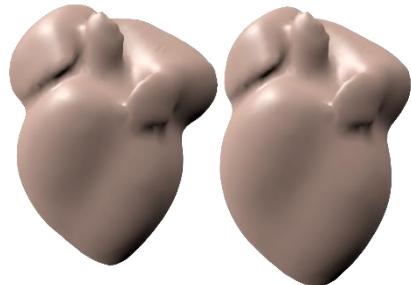
Material distribution affects
physical property



Pipeline



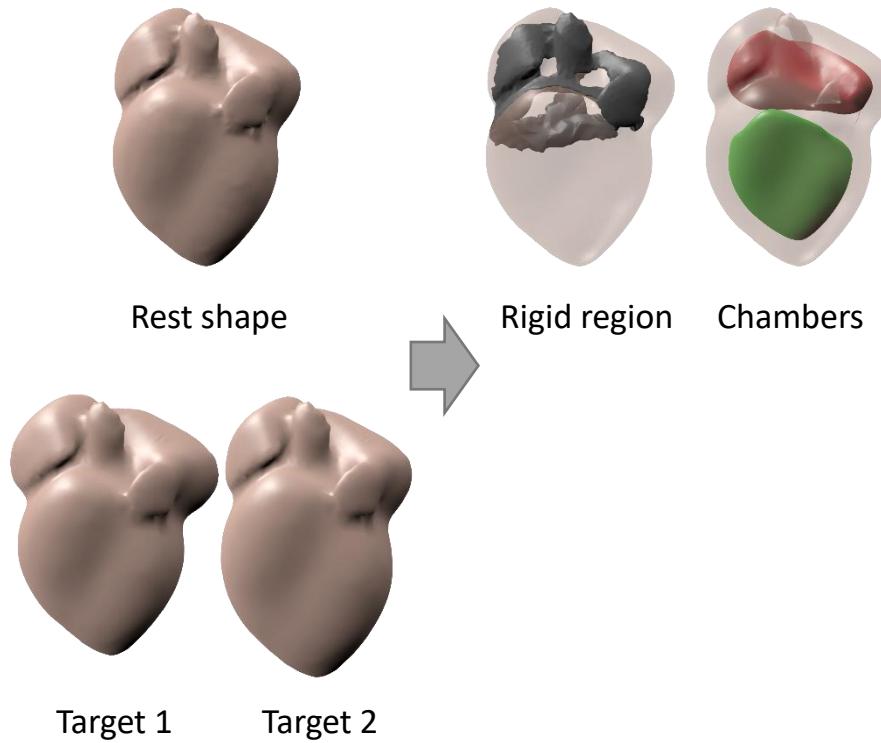
Rest shape



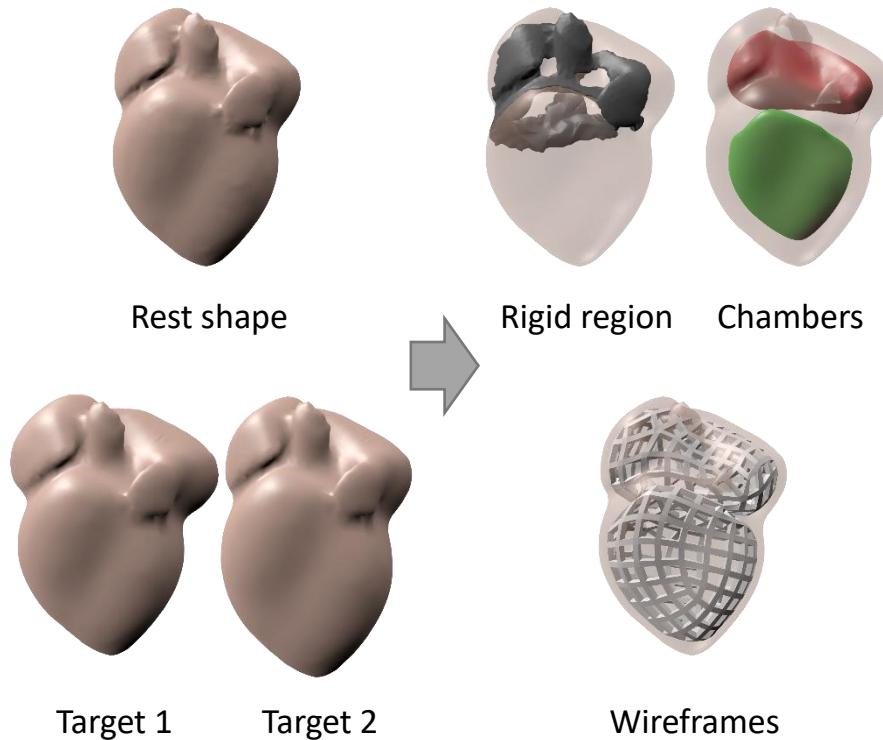
Target 1

Target 2

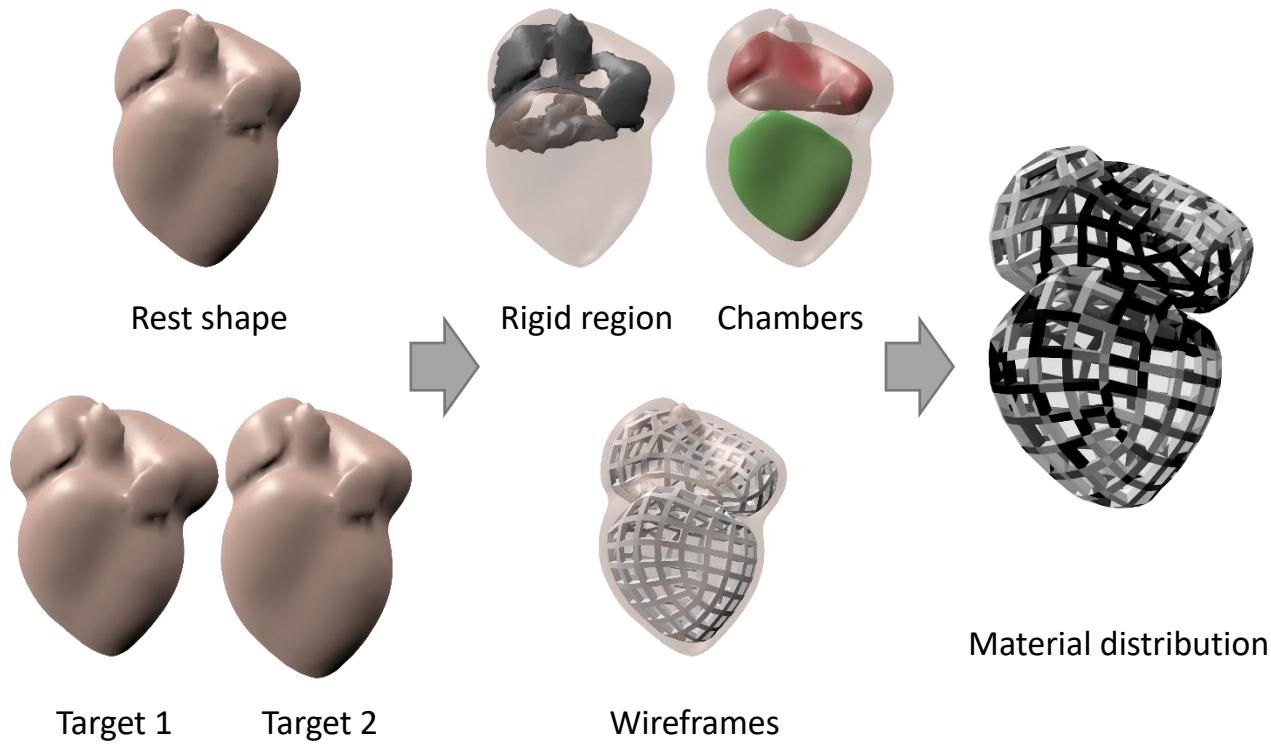
Pipeline



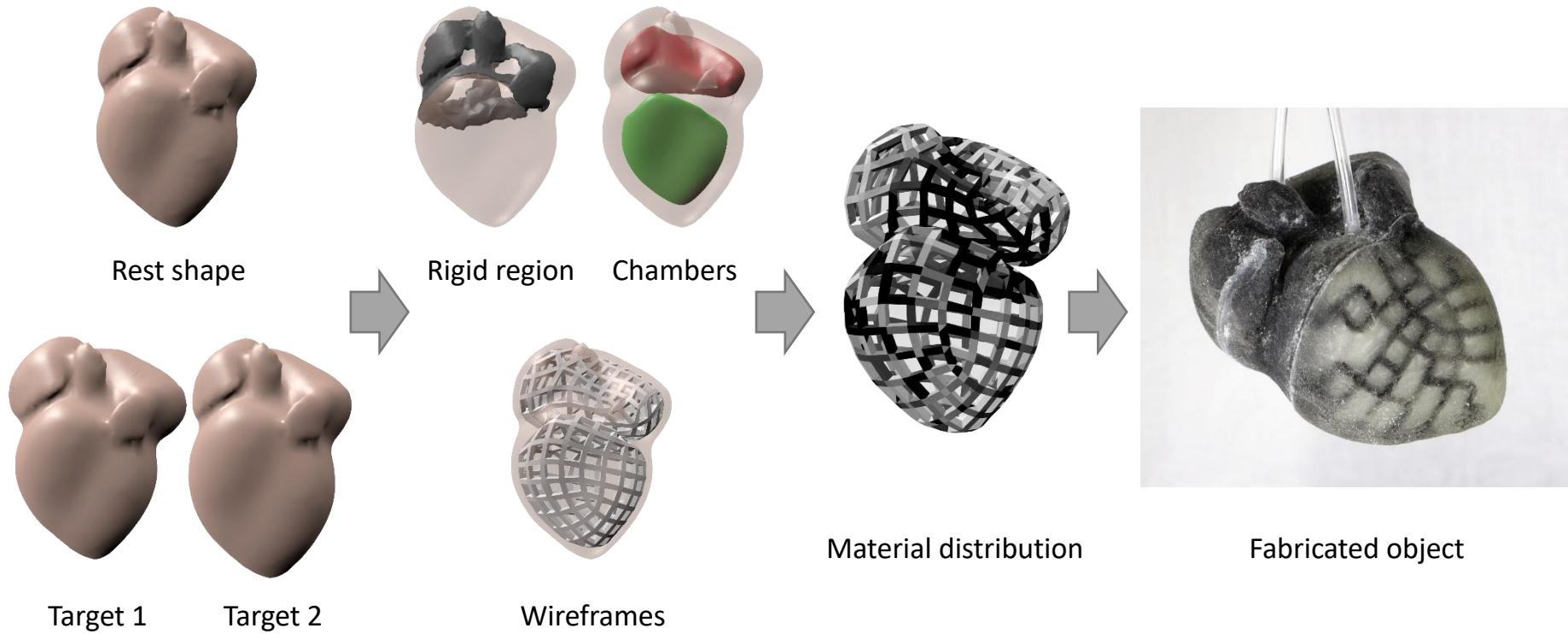
Pipeline



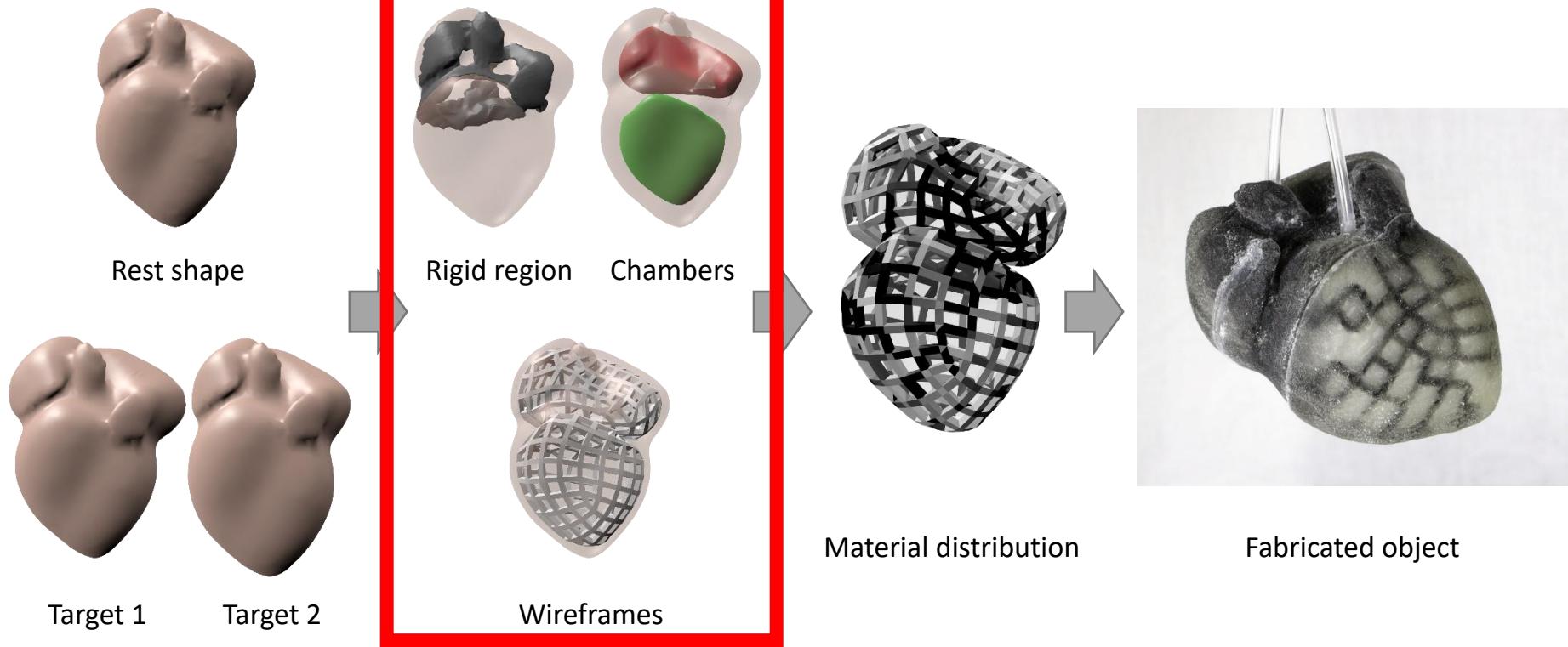
Pipeline



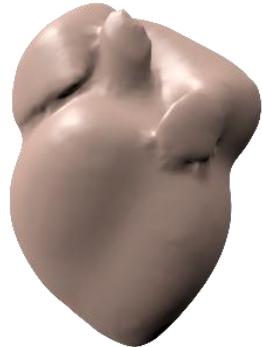
Pipeline



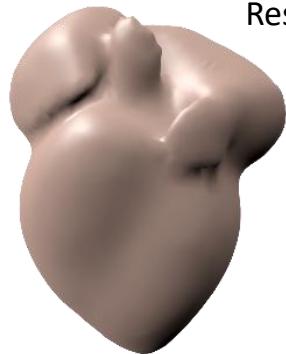
Pipeline : Geometry Setup



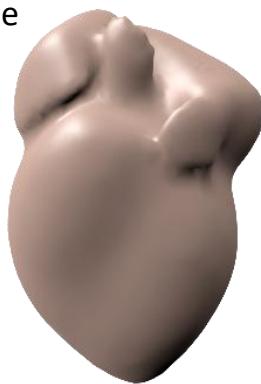
Geometry Setup



Rest shape

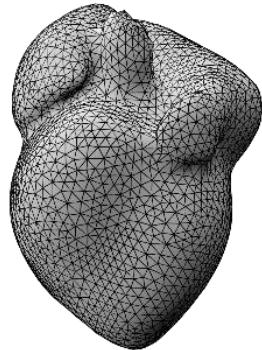


Target 1

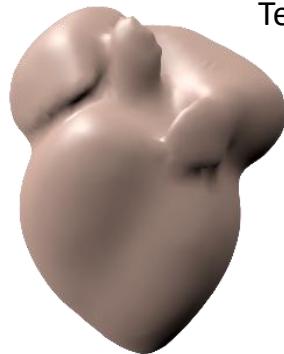


Target 2

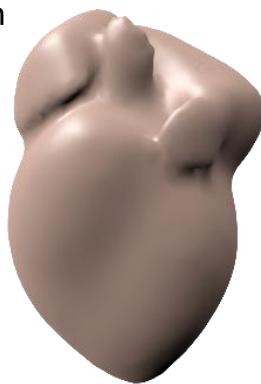
Geometry Setup



Tet mesh

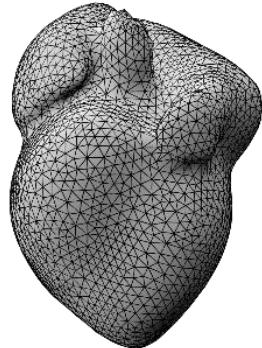


Target 1

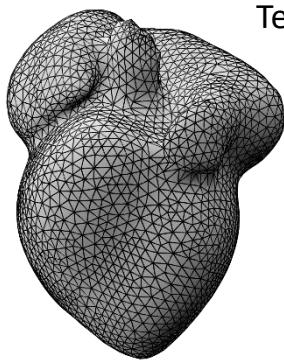


Target 2

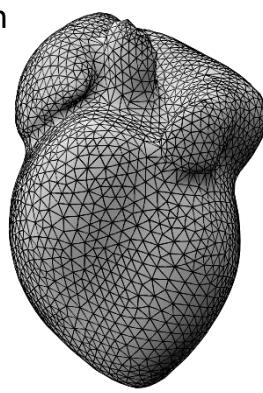
Geometry Setup



Tet mesh

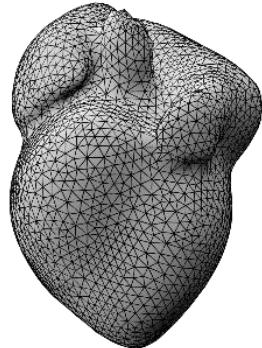


Target 1

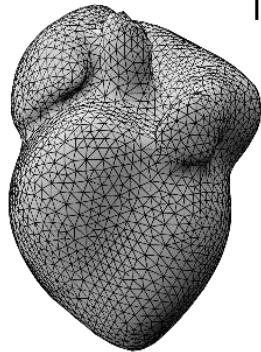


Target 2

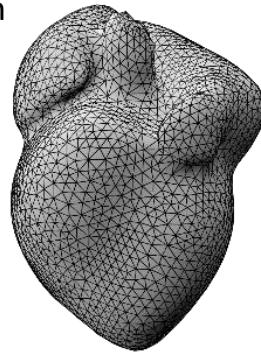
Geometry Setup



Tet mesh

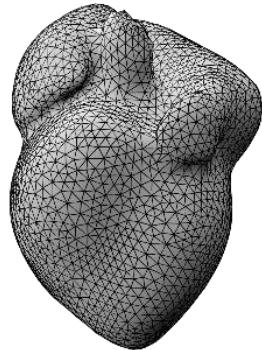


Target 1

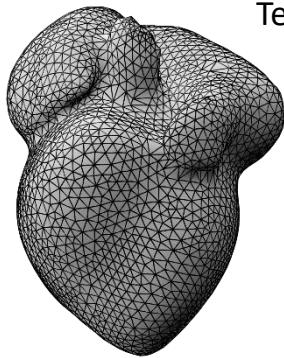


Target 2

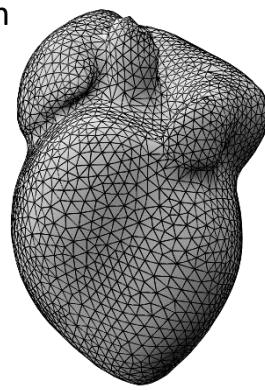
Geometry Setup



Tet mesh

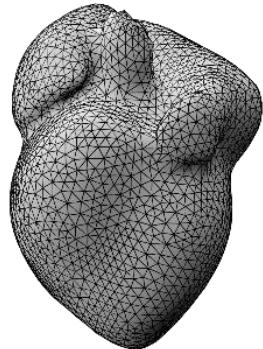


Target 1

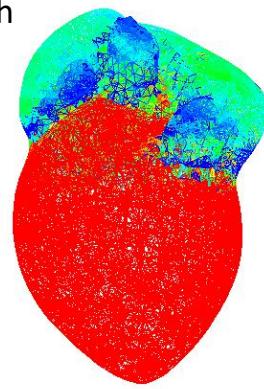
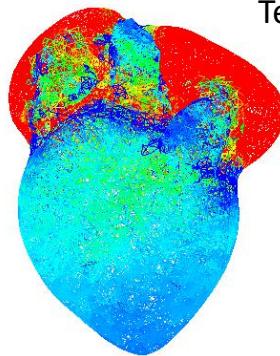


Target 2

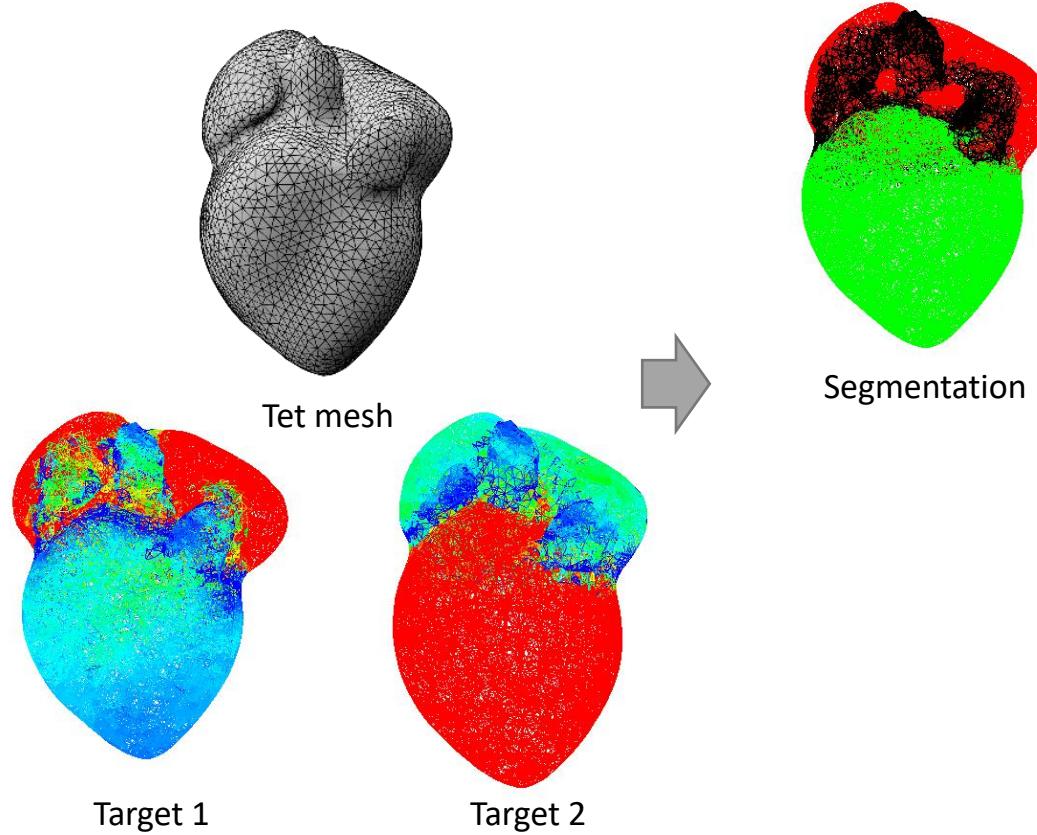
Geometry Setup



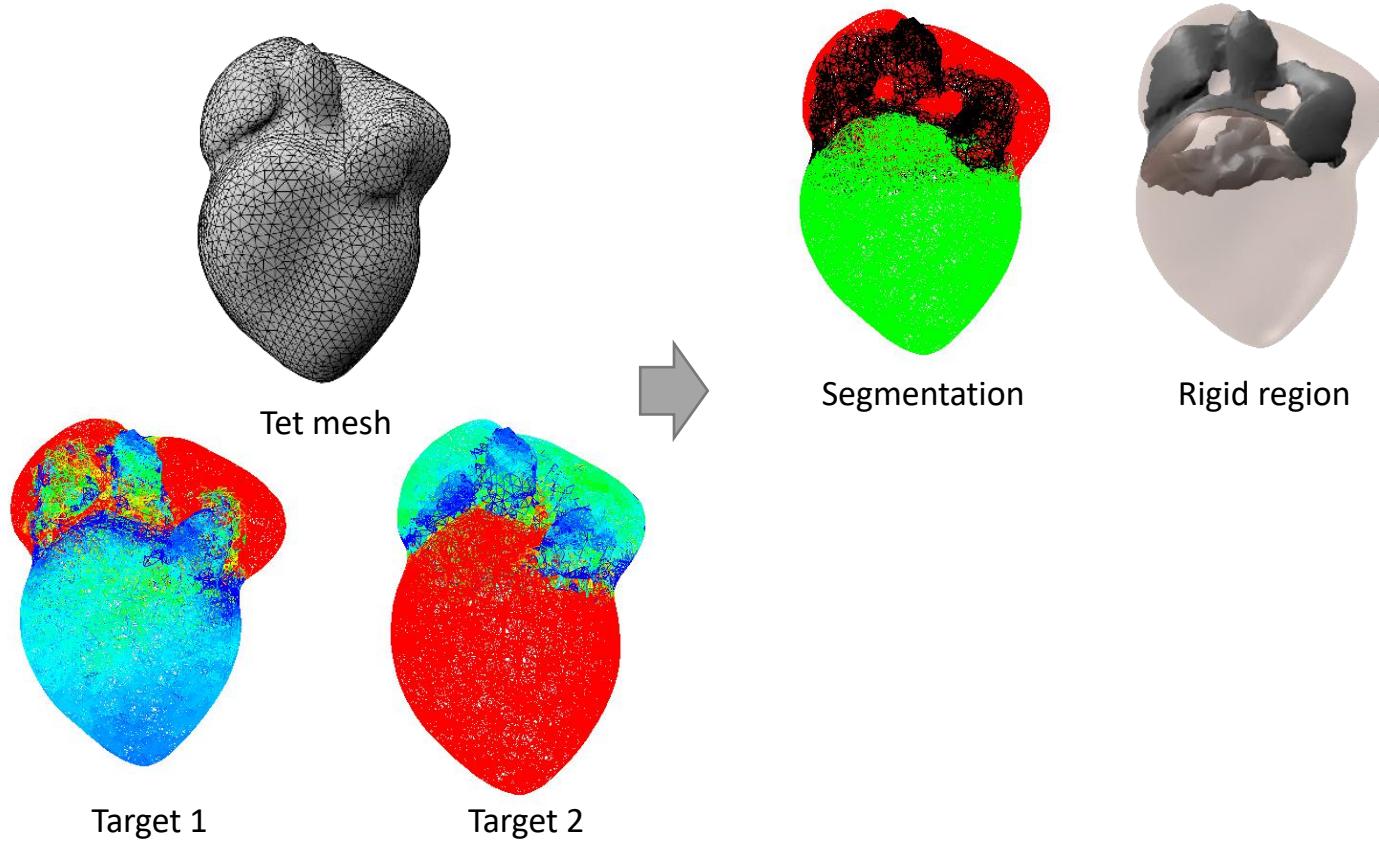
Tet mesh



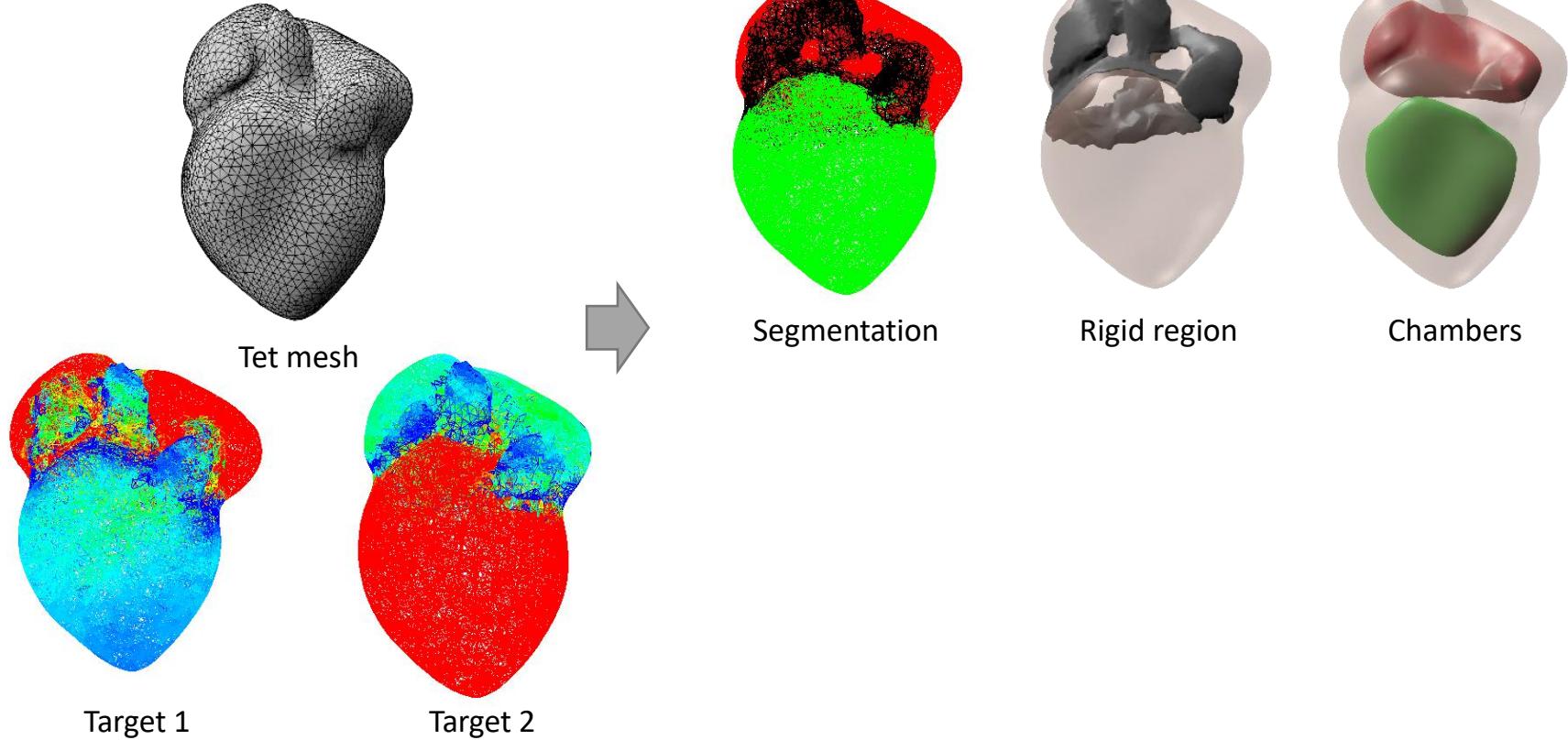
Geometry Setup



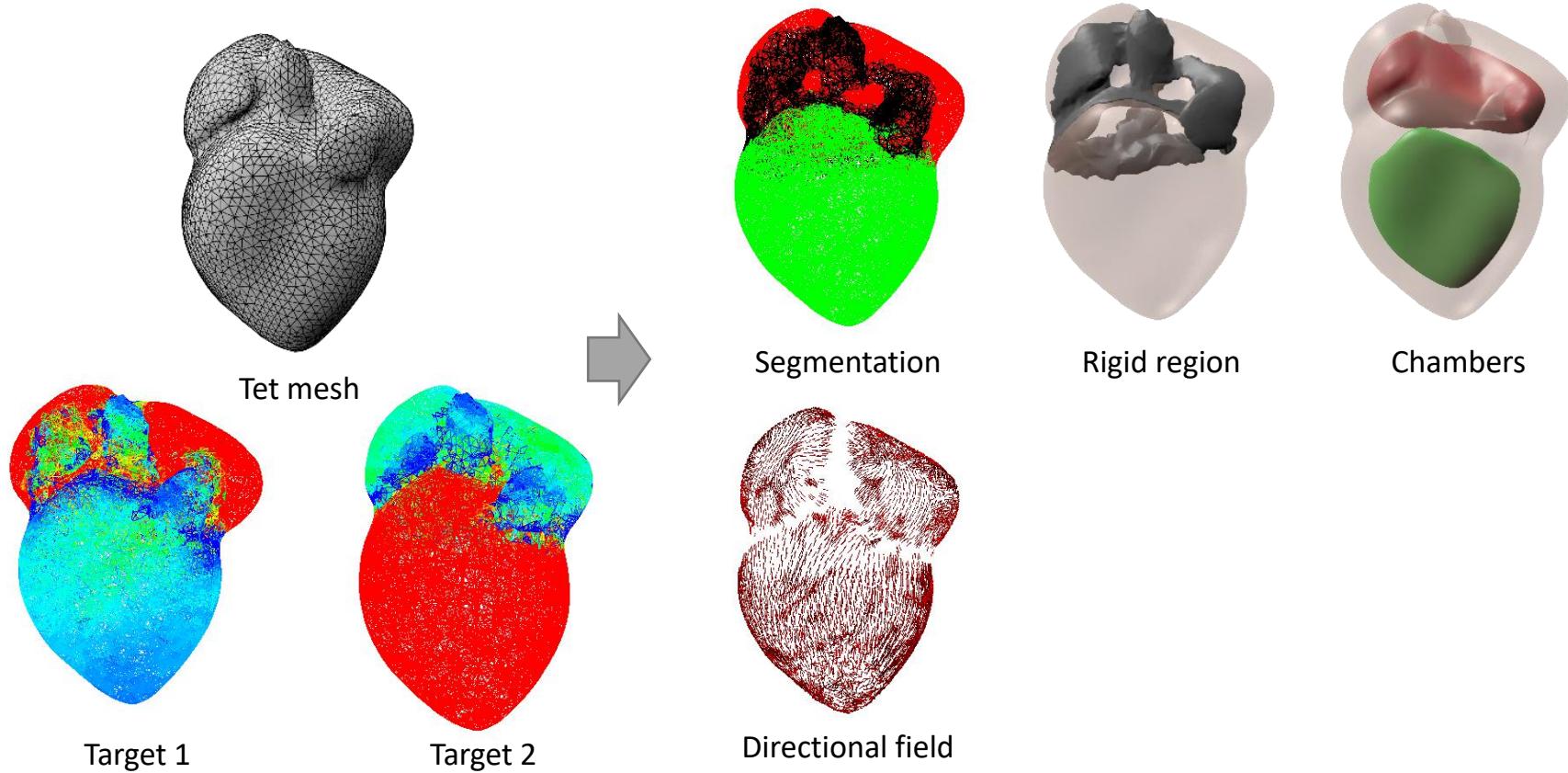
Geometry Setup



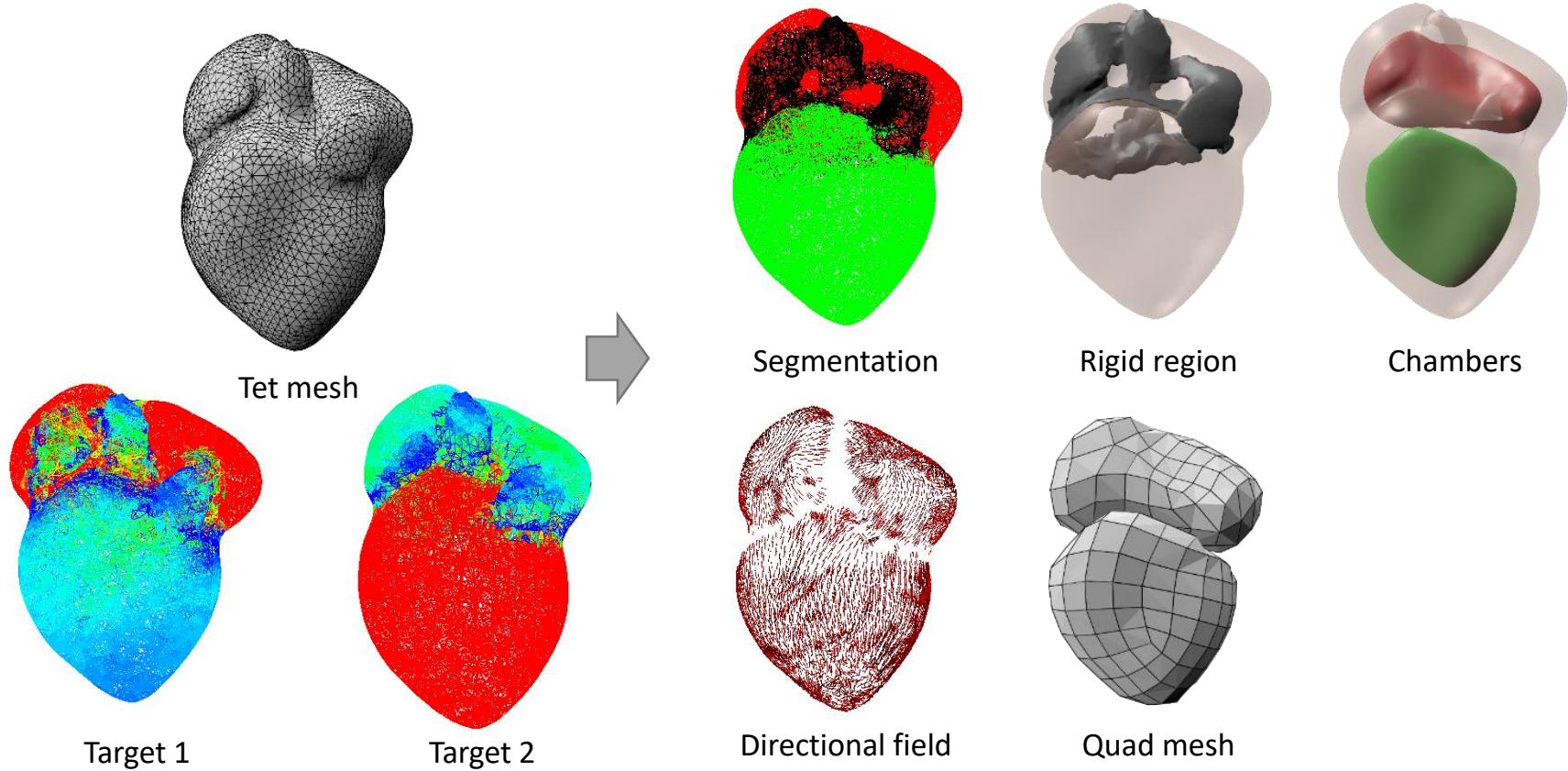
Geometry Setup



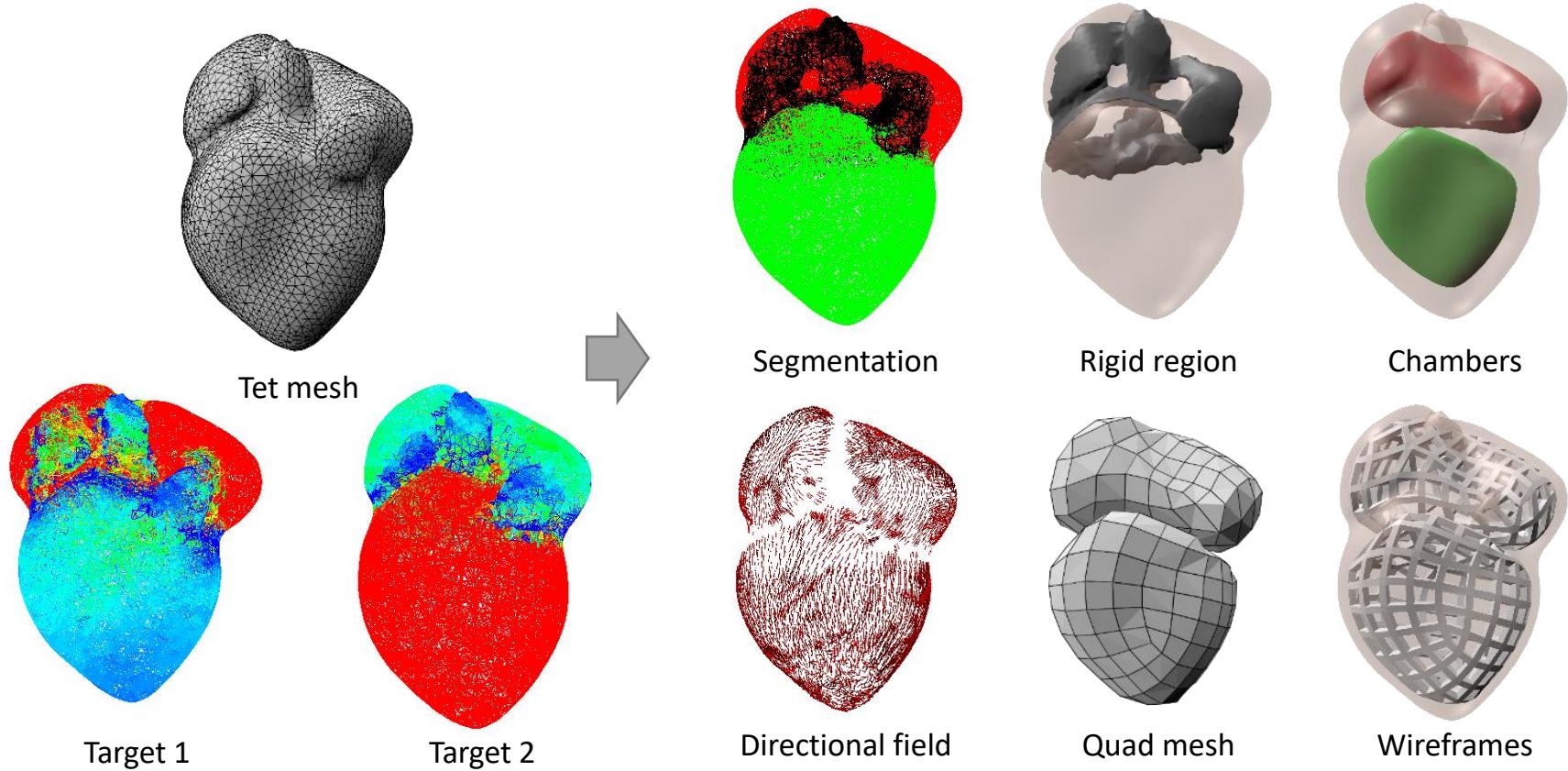
Geometry Setup



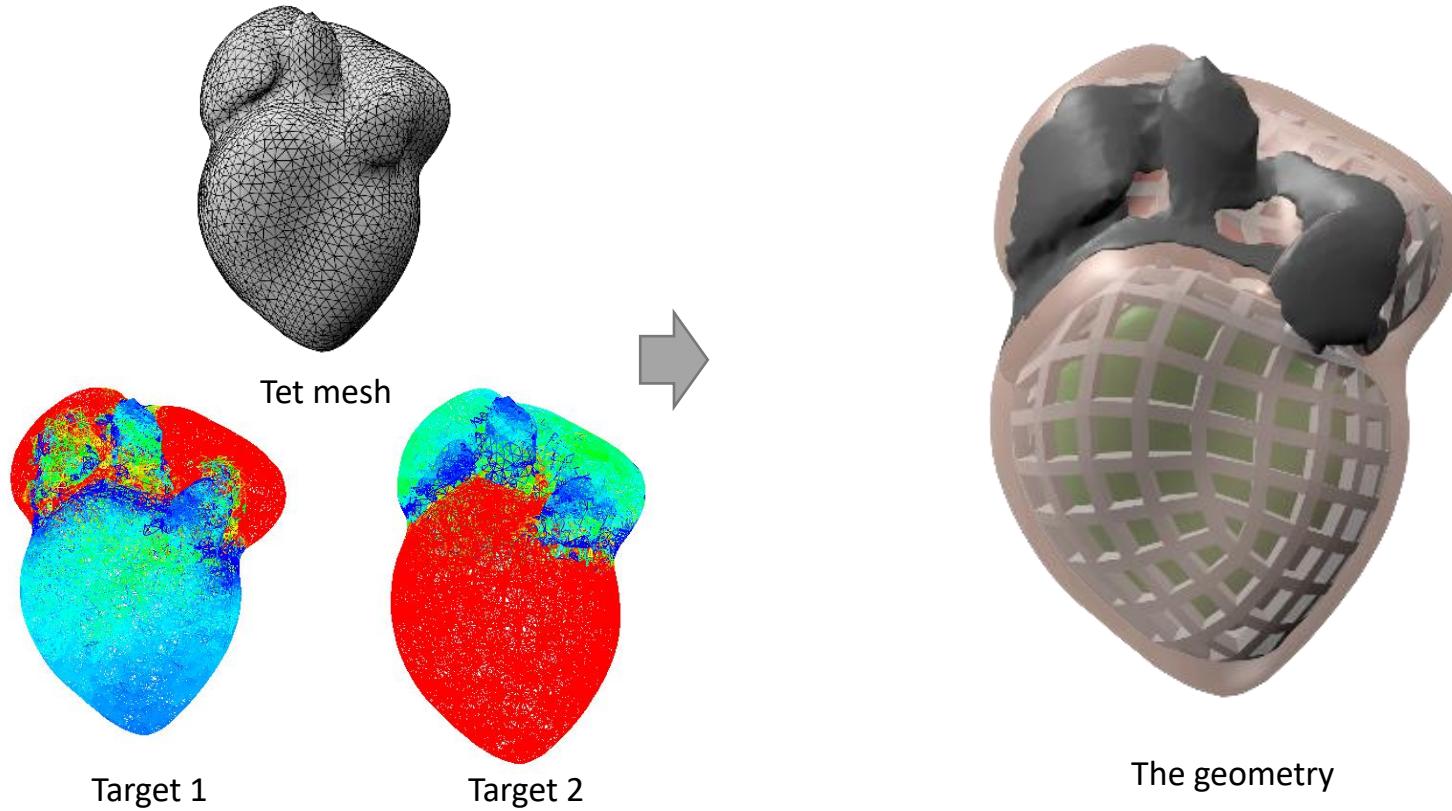
Geometry Setup



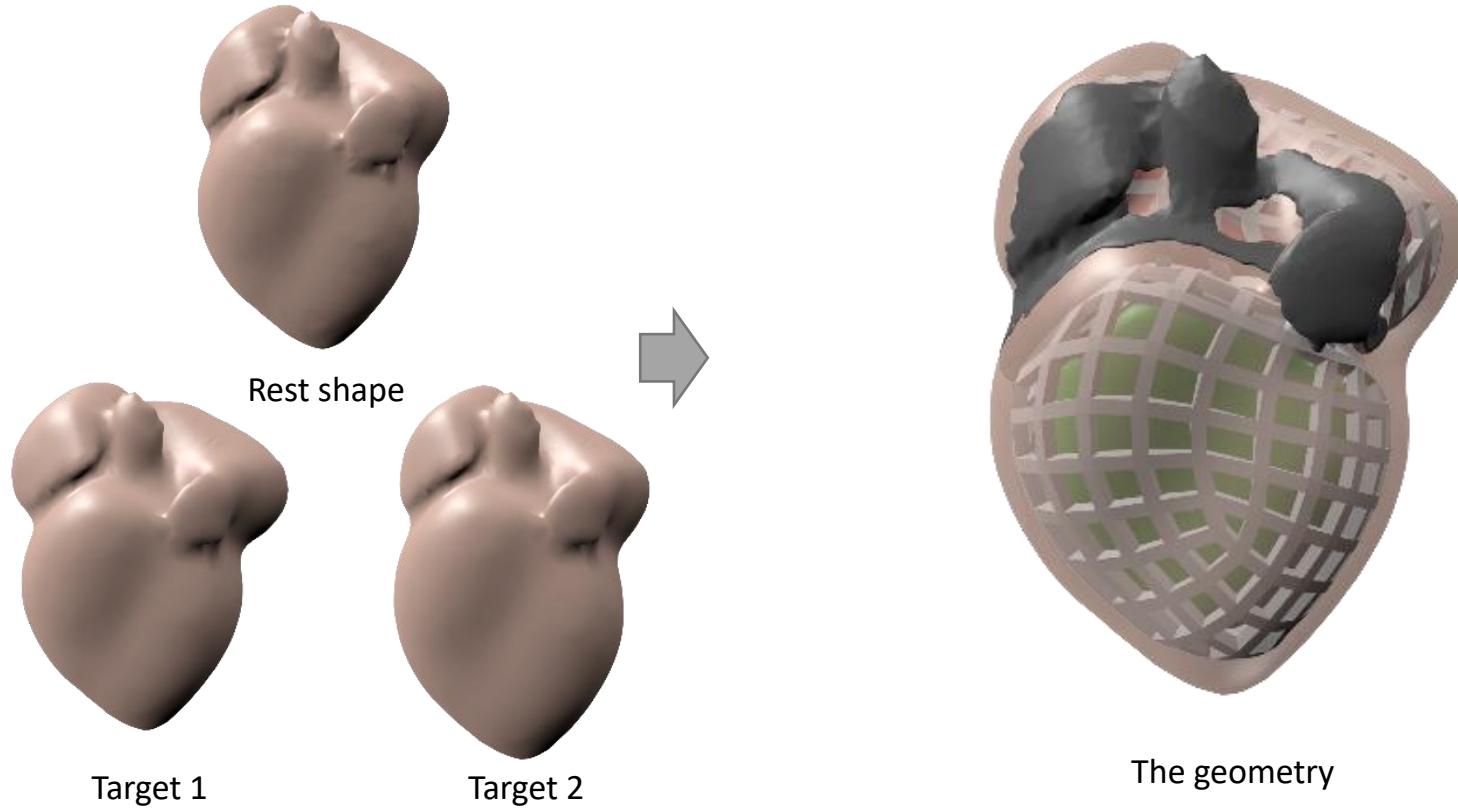
Geometry Setup



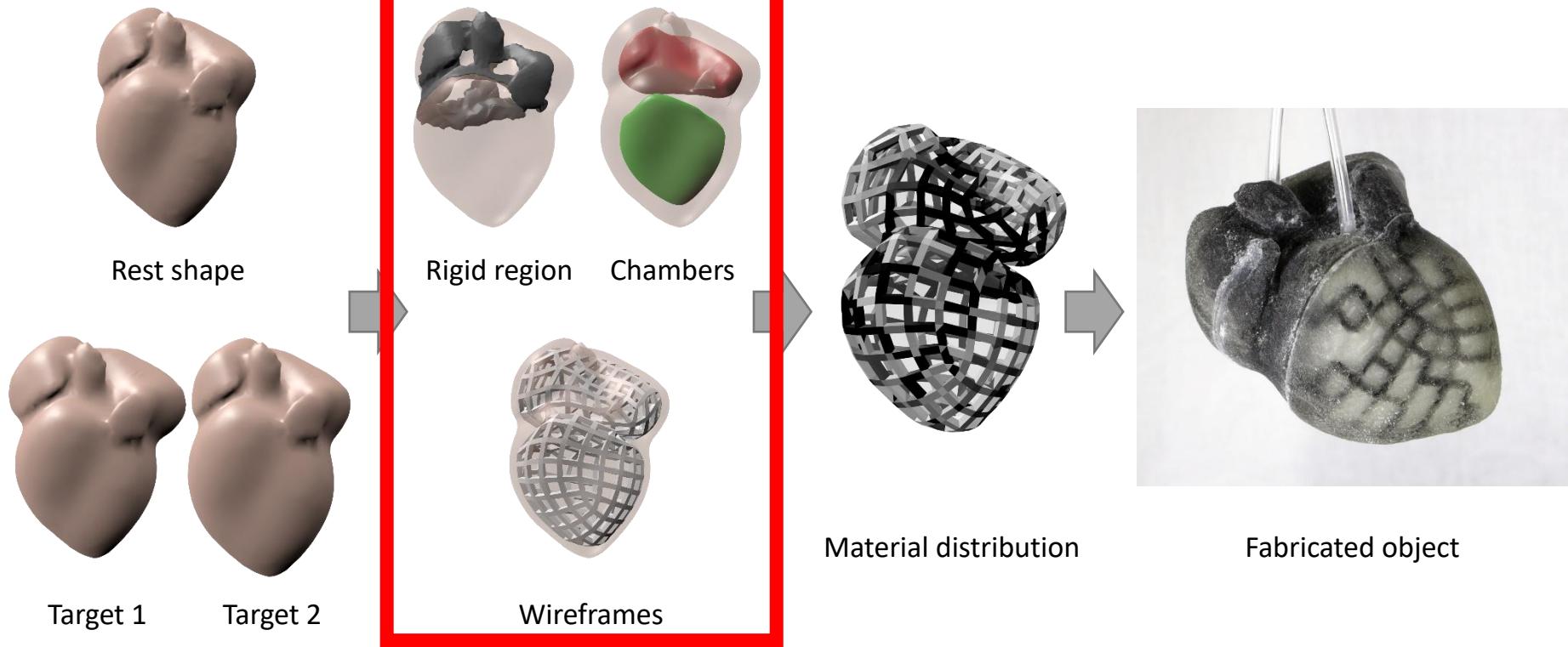
Geometry Setup



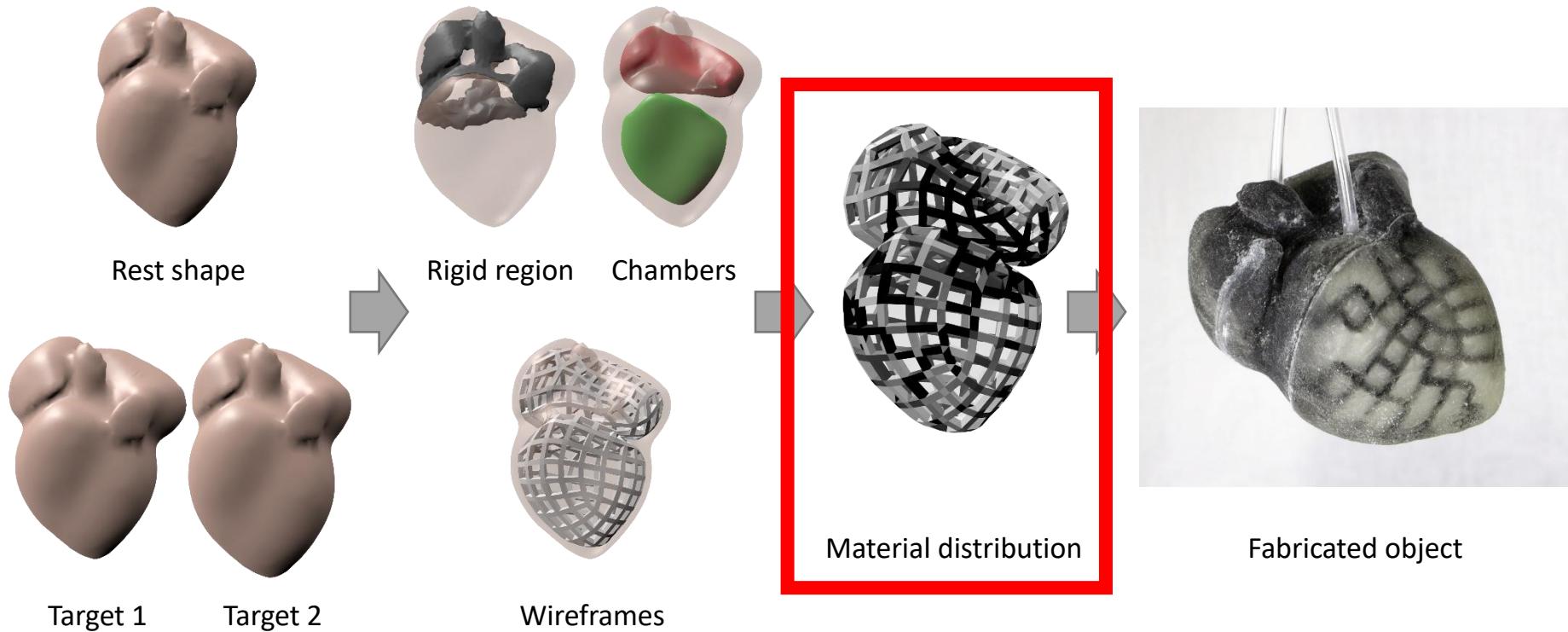
Geometry Setup



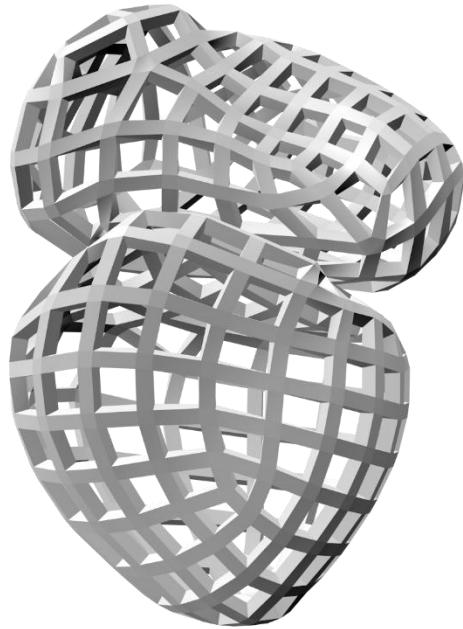
Pipeline : Geometry Setup



Pipeline : Material Optimization

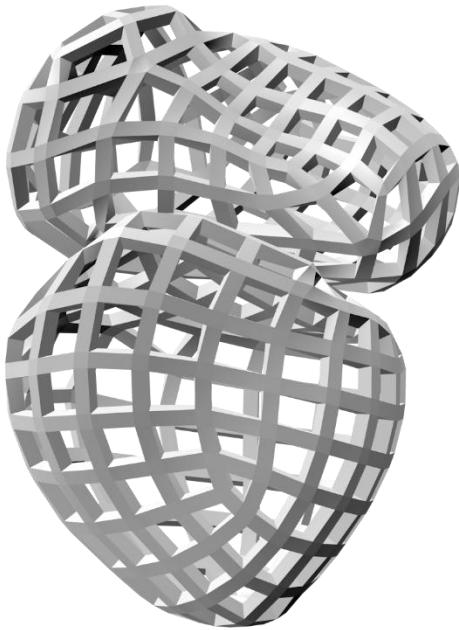


Material Optimization

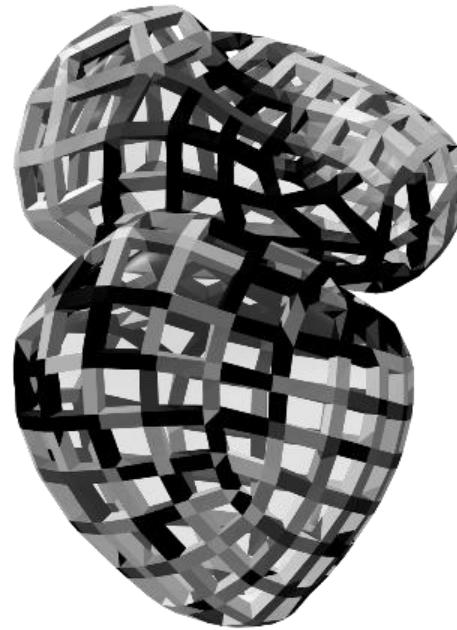


wireframe

Material Optimization

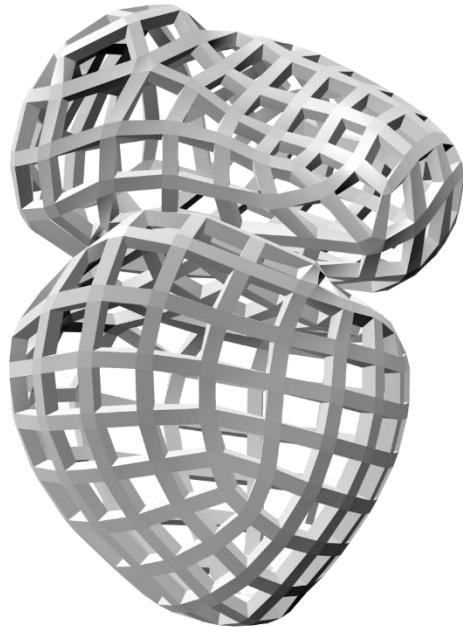


wireframe



material distribution

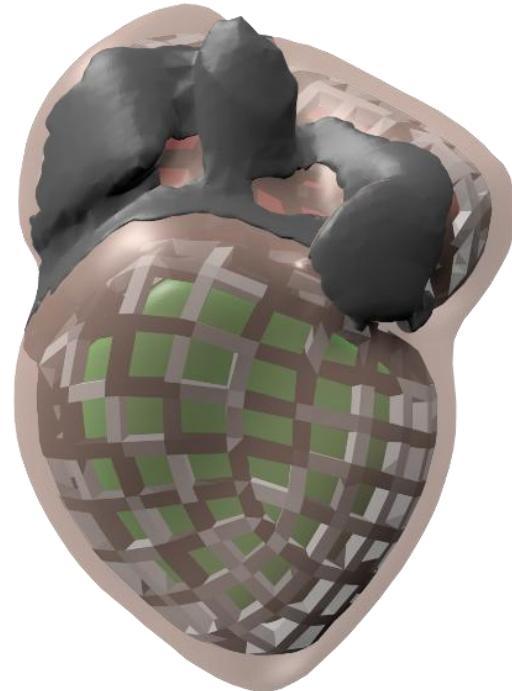
Material Optimization



wireframe



material distribution



the model

Material Optimization



Anisotropic

Isotropic

Material Optimization

Neo-Hookean model

$$\Psi_i = \frac{\mu_i}{2} \{ \text{tr}(F_i^T F_i) - \log[\det(F_i^T F_i) - 3] \} + \frac{\lambda_i}{8} \log^2[\det(F_i^T F_i)]$$

$$\mu_i = \frac{E_i}{2(1 + \nu_i)} \quad \lambda_i = \frac{E_i}{3(1 - 2\nu_i)}$$

Material blend

$$E_{blend} = (1 - \beta)E_{soft} + \beta E_{stiff}$$

$$E_{elas}(\boldsymbol{x}, \beta) := \sum_{\epsilon_i} \Phi[F_i(\boldsymbol{x}); \beta] \text{vol}(\epsilon_i)$$

Equilibrium

$$\left(-\frac{\partial E_{elas}}{\partial \boldsymbol{x}} + \boldsymbol{p}^T \frac{\partial V}{\partial \boldsymbol{x}} - p_0 \frac{\partial V_0}{\partial \boldsymbol{x}} \right) |_{\boldsymbol{x}=\boldsymbol{x}_{eq}(\boldsymbol{p}, \beta)} = 0$$

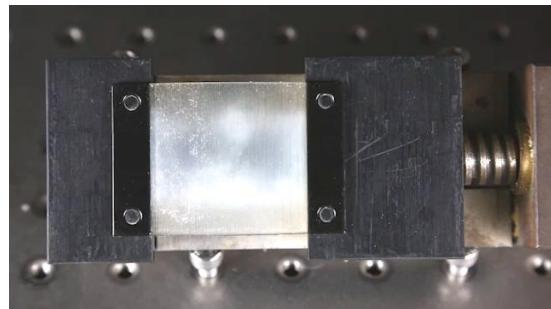
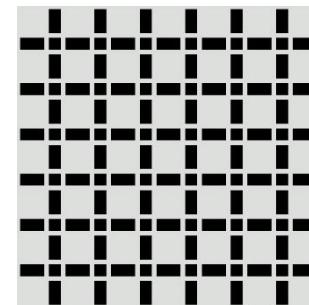
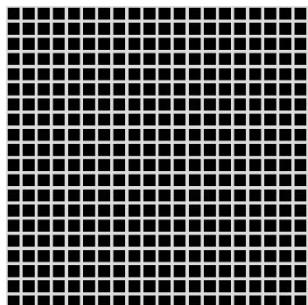
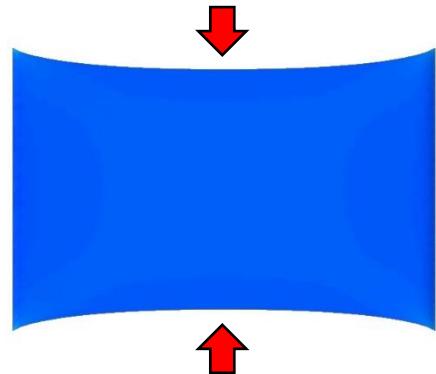
Energy

$$W_{match}^{(j)}(\boldsymbol{x}) := \|\boldsymbol{x} - \boldsymbol{X}^{(j)}\|^2$$

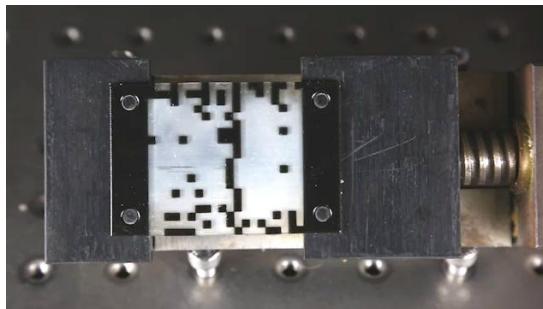
Optimization

$$\min_{\beta, p^{(1)}, \dots, p^{(K)}} \sum_{j=1}^K W_{match}^{(j)}[x_{eq}(p^{(j)}, \beta)] + \alpha \sum_{j=1}^K E_{elas}[x_{eq}(p^{(j)}, \beta), \beta]$$

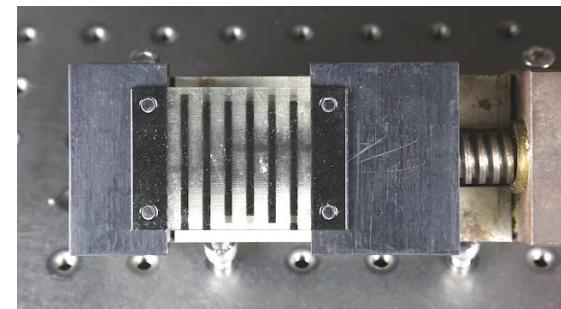
Wireframe vs. Full Space



Homogeneous

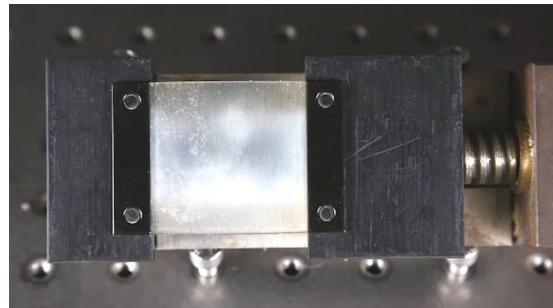
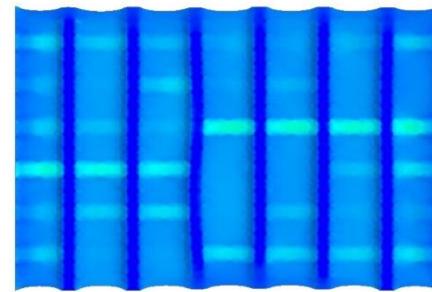
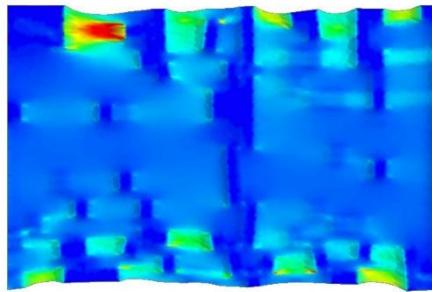


Full space

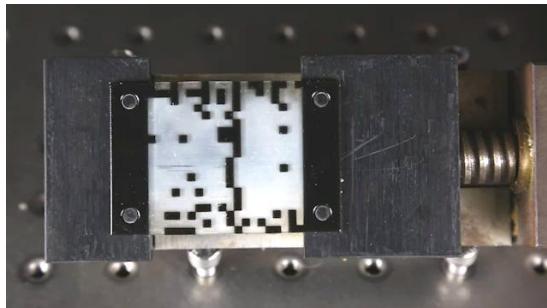


Wireframe

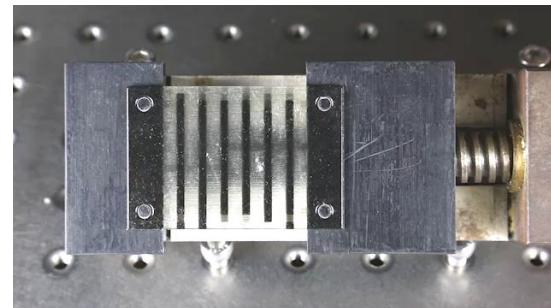
Wireframe vs. Full Space



Homogeneous

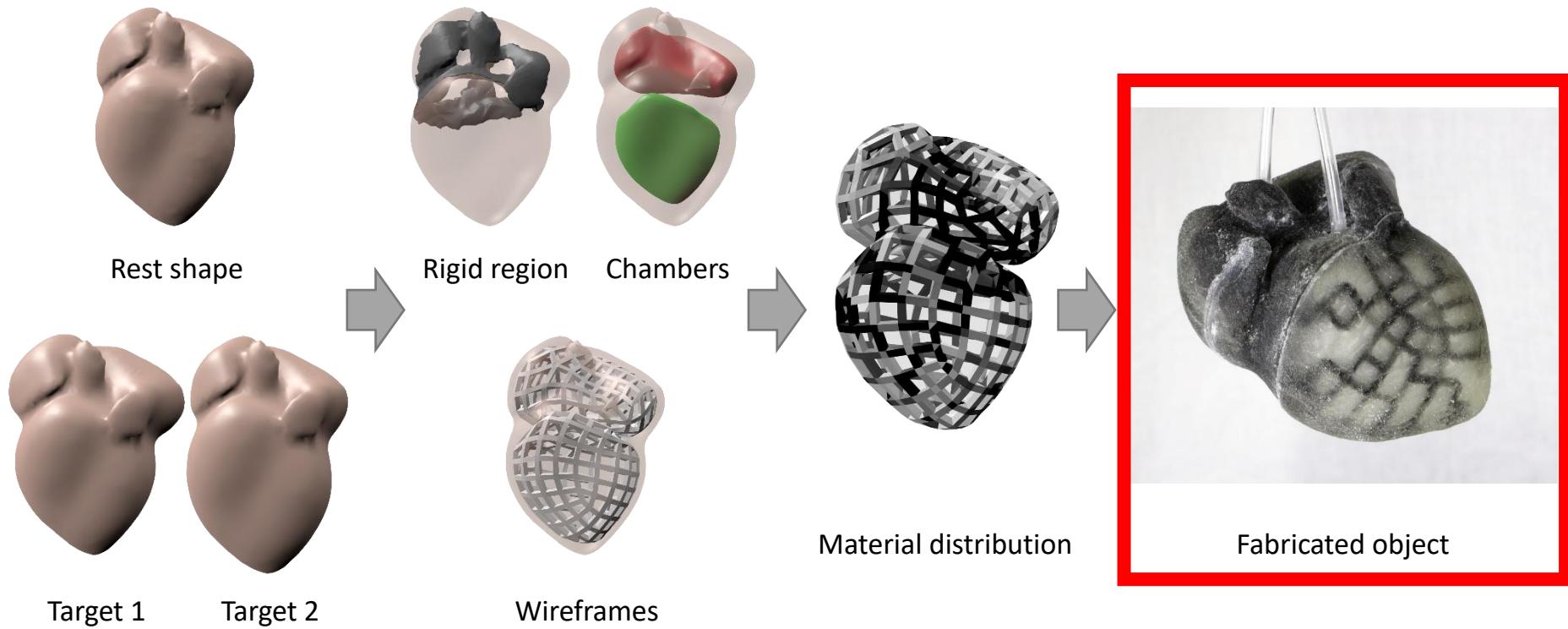


Full space



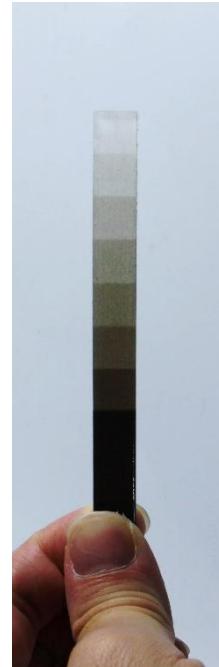
Wireframe

Pipeline

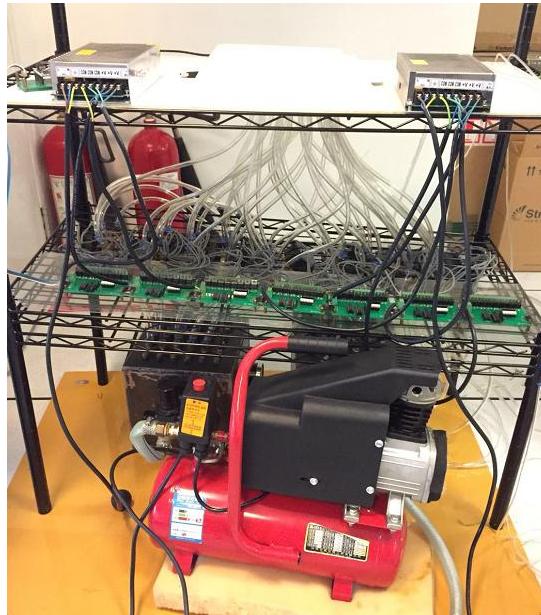


Physical Realization

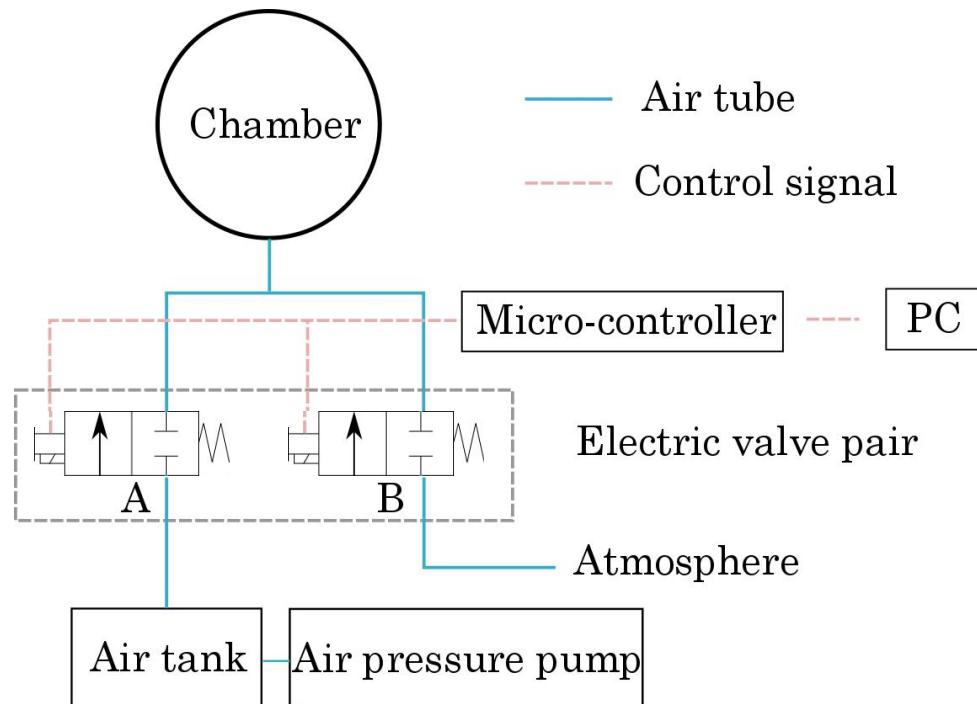
Fabrication Process



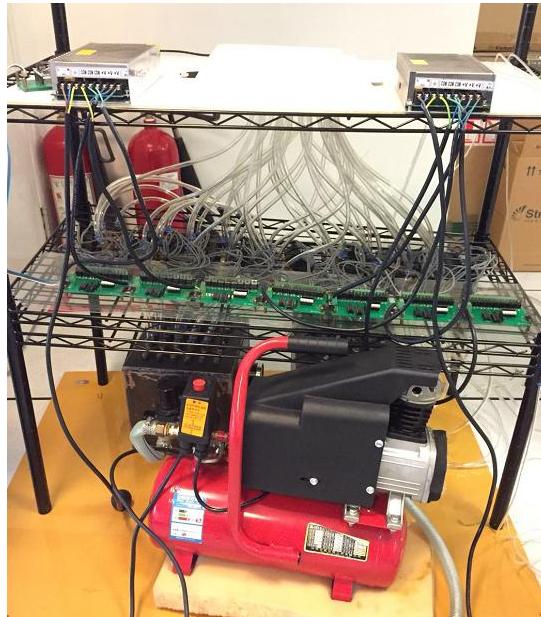
Pneumatic Control System



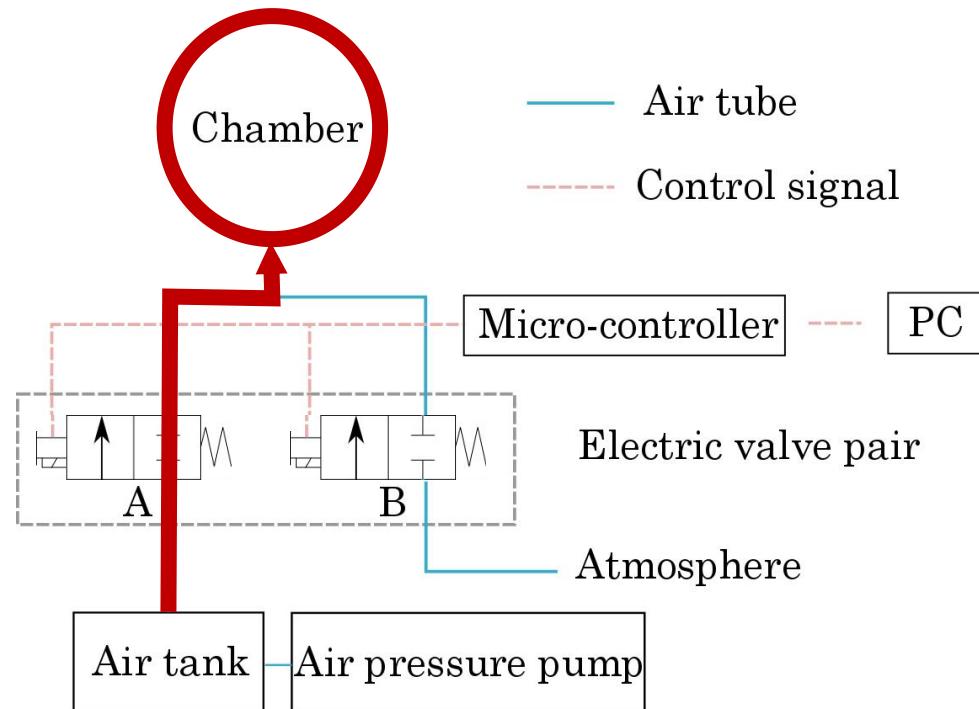
[Hachisu et al. 2014]



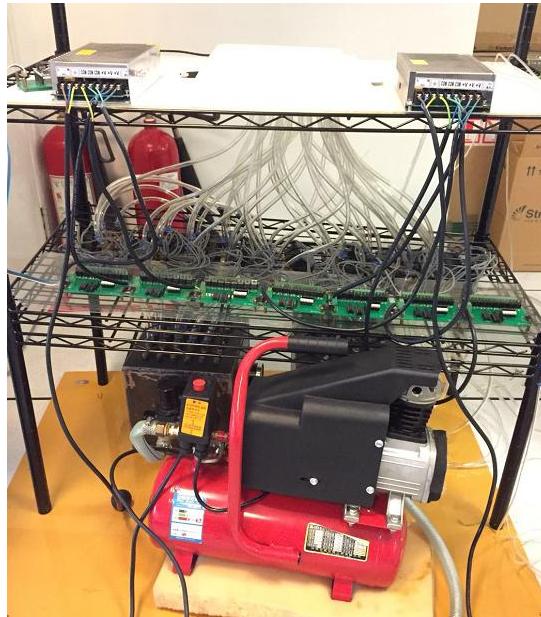
Pneumatic Control System



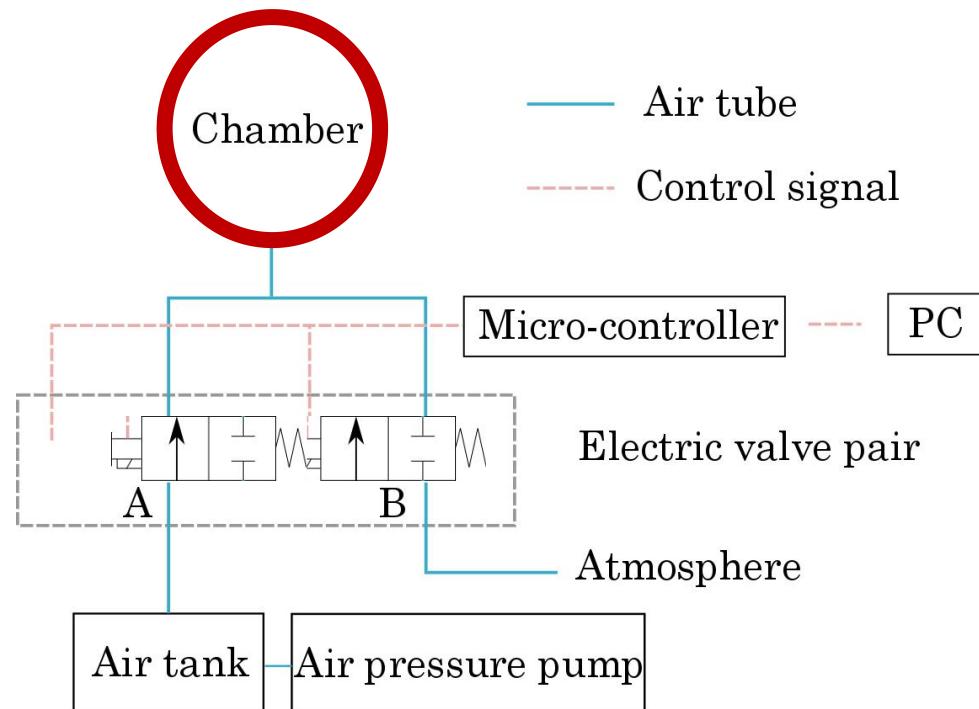
[Hachisu et al. 2014]



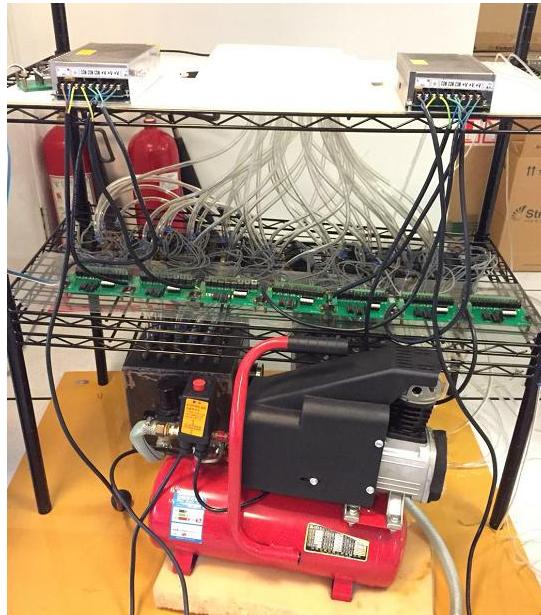
Pneumatic Control System



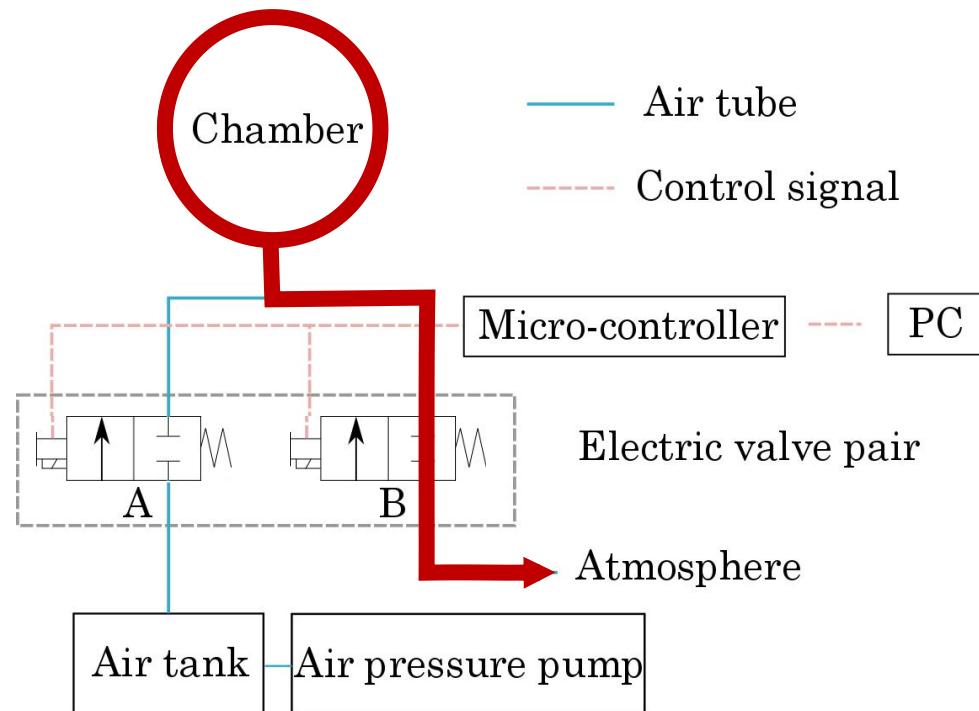
[Hachisu et al. 2014]



Pneumatic Control System



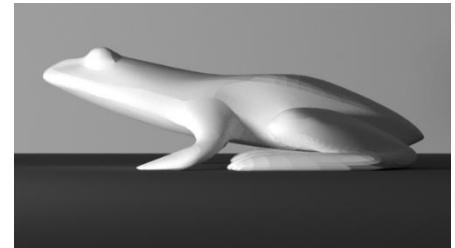
[Hachisu et al. 2014]



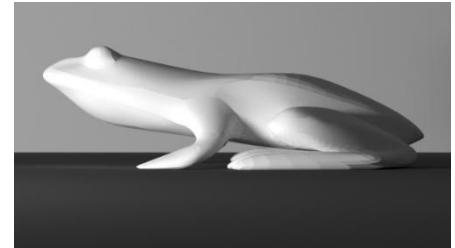
Physical Realization



$\times 2$



Rest pose



Target pose

Results : optimization timing



9 min



8 min



9 min



29 min



3 min



1 min



34 min



3.5 h

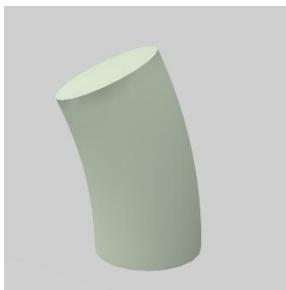


1 h

extrude



bend



fat

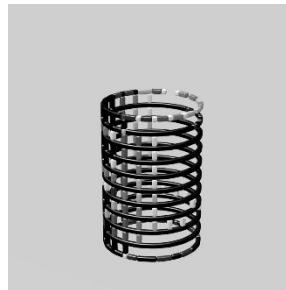
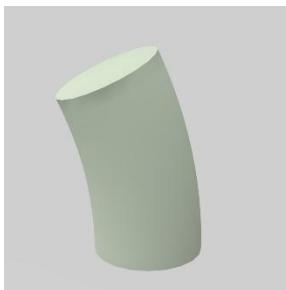


target

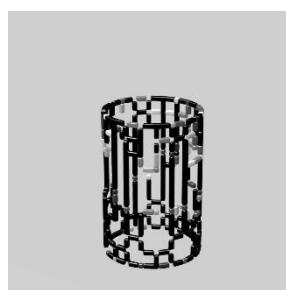
extrude



bend



fat



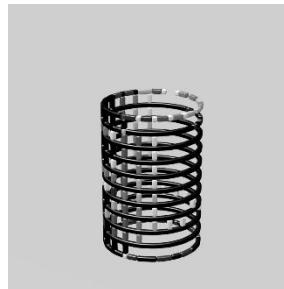
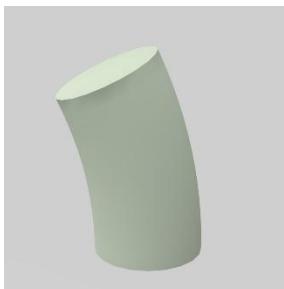
target

material

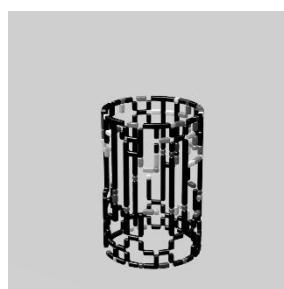
extrude



bend



fat



target

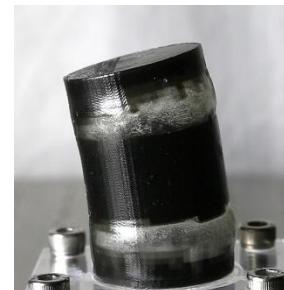
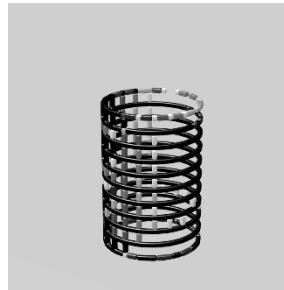
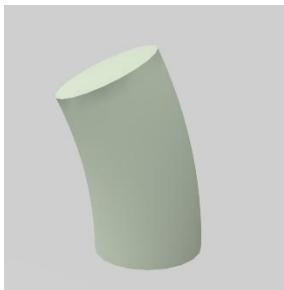
material

our result

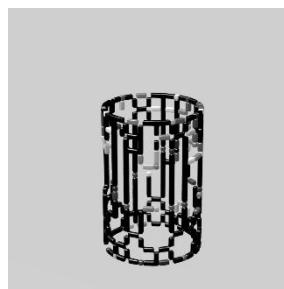
extrude



bend



fat



target

material

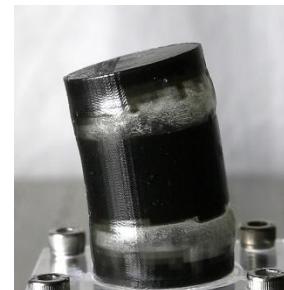
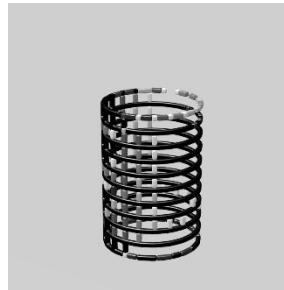
our result

full space

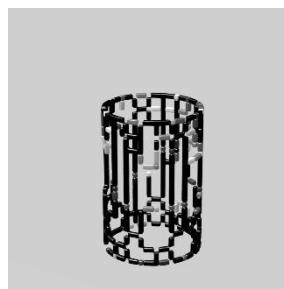
extrude



bend



fat



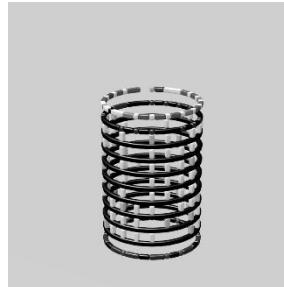
target

material

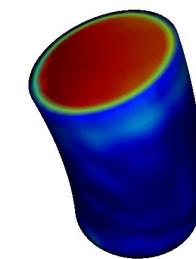
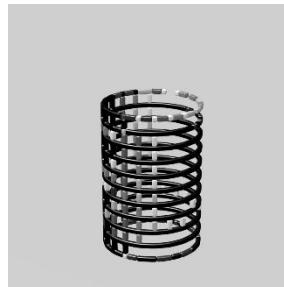
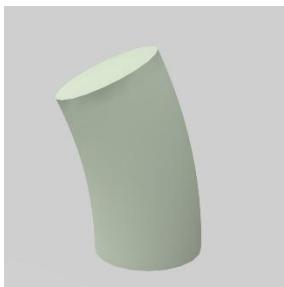
our result

full space

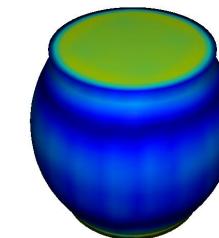
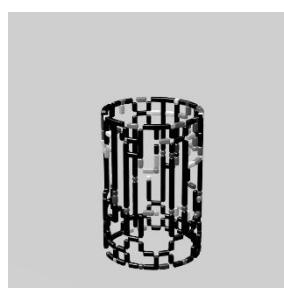
extrude



bend



fat



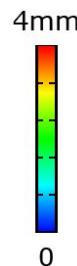
target

material

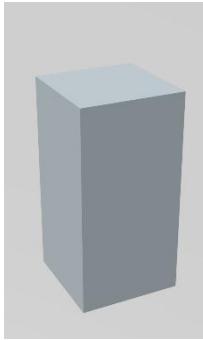
our result

full space

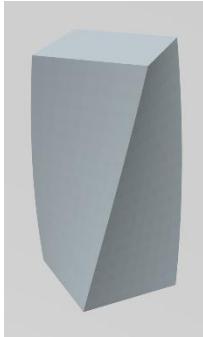
error



Single Chamber Result: Twisted Bar



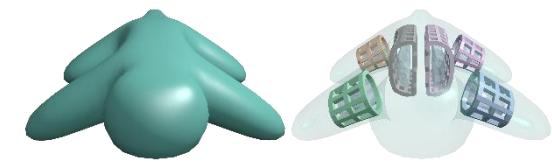
Rest pose



Target pose



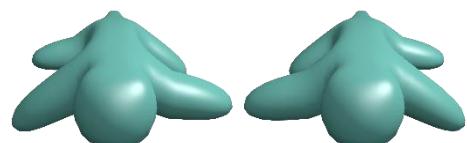
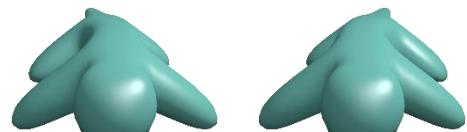
Multi-Chamber Results: Crawling Creature



Rest pose



Chamber & Wireframes



Target poses

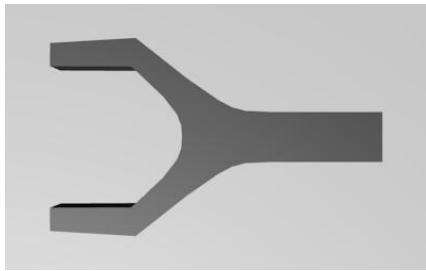


Multi-Chamber Results: Crawling Creature

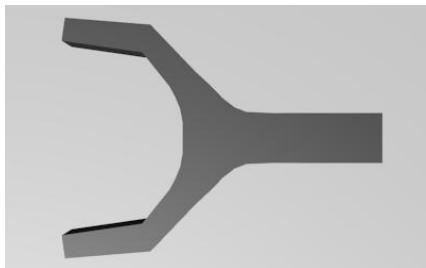


×2

Application: Pneumatic Gripper



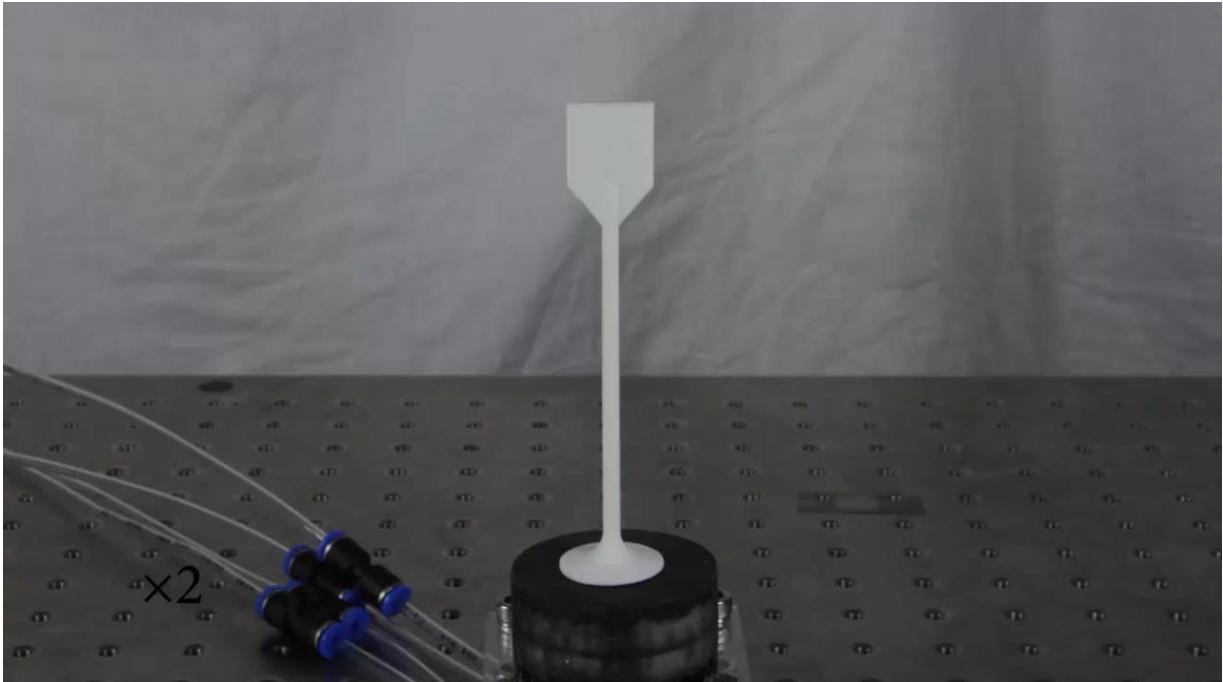
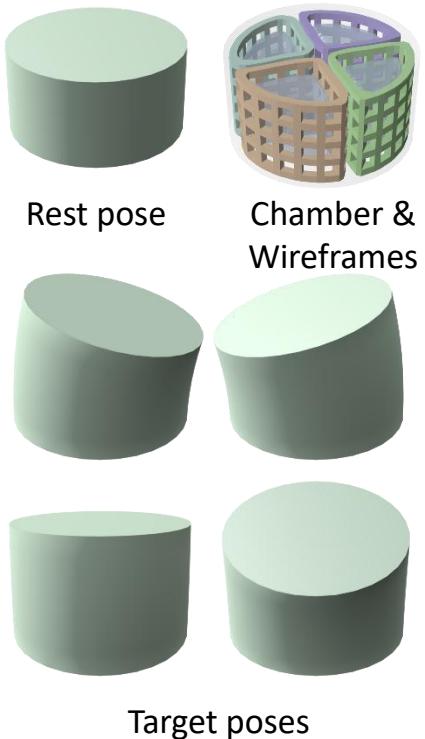
Rest pose



Target pose

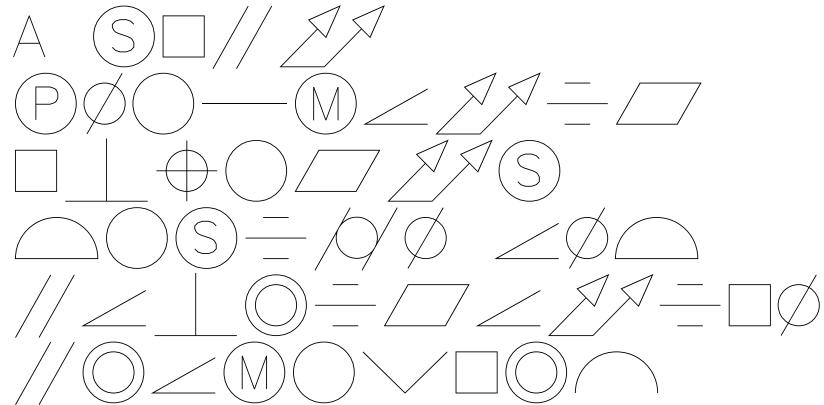
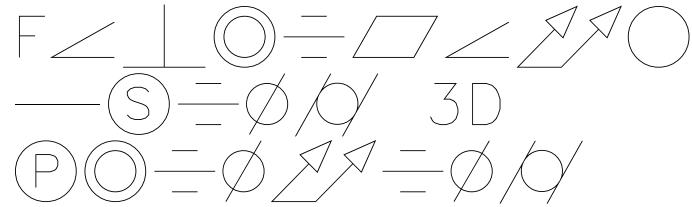


Application: Multi-directional Pneumatic Module





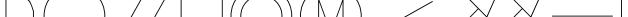
Conclusion

- A 
- F 
- C 



Limitations

- 
 - 





Future Work

- M   



Acknowledgements

- A $\emptyset \square \emptyset$ \rightarrow $\circ M \square \rightarrow \circ S$
 $\circ \circ \square \sqcup \sqcap \circ \checkmark \circ \circ S$
- T $\angle \circ \rightarrow H \angle \square \nearrow \equiv \circ S \rightarrow$
 $\angle \emptyset \square M \angle \circ S \angle \angle \circ \equiv$
 $F \angle \circ \rightarrow M \square \nearrow \square \nearrow \square // \square \circ$
 $\circ S \nearrow \angle \circ \equiv \emptyset \emptyset$
 $\circ P \emptyset \circ \rightarrow M \angle \nearrow \nearrow \equiv \square$
 $\circ S \rightarrow \circ S \nearrow \nearrow \circ M$
- S $\nearrow \nearrow \circ P \nearrow \circ \emptyset L \equiv \emptyset // \square \circ$
 $\circ P \circ \square \square // \circ \circ \angle \circ \equiv \emptyset \emptyset$

Computational Design and Fabrication of Soft Pneumatic Objects with Desired Deformations

Li-Ke Ma^{*1,2} Yizhong Zhang^{*2} Yang Liu² Kun Zhou³ Xin Tong²

* Joint first authors

1, Tsinghua University

2, Microsoft Research Asia

3, Zhejiang University

