

# **Rotation-strain Coordinate for Large Elastic Deformation**

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**Background**

# Elastic Simulation

- Traditional Industry: car, ship, plane etc.
- Film, Game, VR: Realistic digital objects.
- Modern Fabrication: 3D printing.
- Medicine, etc.



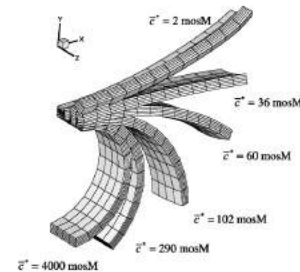
# Foundation and Challenge

- Action

$$S[x, \dot{x}] = \int_0^T T - V dt$$

- The Euler-Lagrange equation

$$\frac{d}{dt} \left( \frac{\partial T}{\partial \dot{x}} \right) - \frac{\partial V}{\partial x} = 0$$



# Foundation and Challenge

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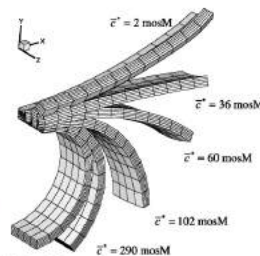
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- The Euler-Lagrange equation

$$\frac{d}{dt} \left( \frac{\partial T}{\partial \dot{x}} \right) - \frac{\partial V}{\partial x} = 0$$

- Key challenges: **Dimension and Non-linearity**

- Large number of nodes: high dimensional  $x \in \mathbb{R}^N$
- Non-linear elastic force:  $f(x)$  is not linear to  $x$



# Linear Subspace

- In much smaller space  $B = [B_1, B_2, \dots, B_r]$ 
  - Linear combination of a few possible deformations  $B_i$
  - A few number of variables  $\tilde{x} \in \mathbb{R}^r, r \ll N$
  - Variable substitution  $x = B\tilde{x}$

A diagram illustrating the equation  $x = B \tilde{x}$ . On the left, a tall, narrow gray rectangle contains the variable  $x$ . To its right is an equals sign. Further right is a wider gray rectangle containing the matrix  $B$ . To the right of the  $B$  rectangle is a small gray rectangle containing the variable  $\tilde{x}$ . A dot is placed between the  $B$  rectangle and the  $\tilde{x}$  rectangle, representing the matrix multiplication.

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- Many methods to construct  $B$ 
  - Modal Analysis
  - Modal Derivatives
  - Mass PCA
  - ...

A diagram illustrating the equation  $x = B \tilde{x}$ . It consists of three rectangular boxes. The first box on the left is tall and narrow, containing the variable  $x$ . To its right is an equals sign. The second box is wider and contains the matrix  $B$ . To its right is a dot, followed by a third box that is tall and narrow, containing the variable  $\tilde{x}$ .

# Linear Subspace

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$$x = B \cdot \tilde{x}$$

- But nothing to do with **Non-linearity**



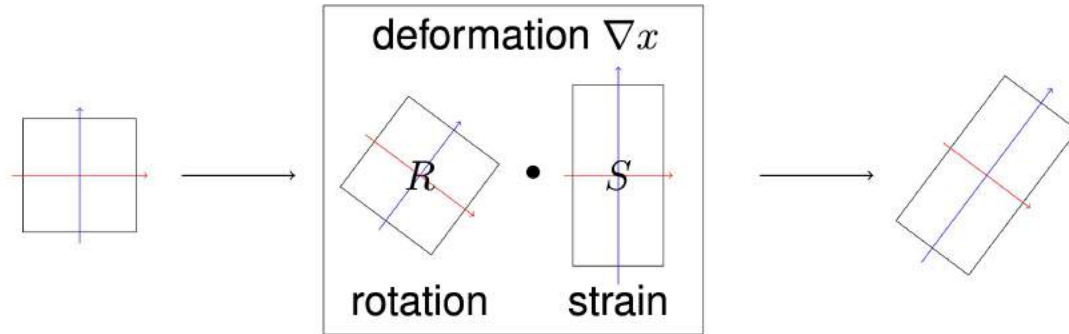
# The Source of Non-linearity

- Geometric nonlinearity
  - displacement-strain relationship (Green strain, etc.)
- Material nonlinearity
  - strain-stress relationship (StVK, Neo-hookean, etc.)

We only consider geometric nonlinearity, with  
linear strain-stress relationship  $\sigma = \mathcal{C} : \epsilon$

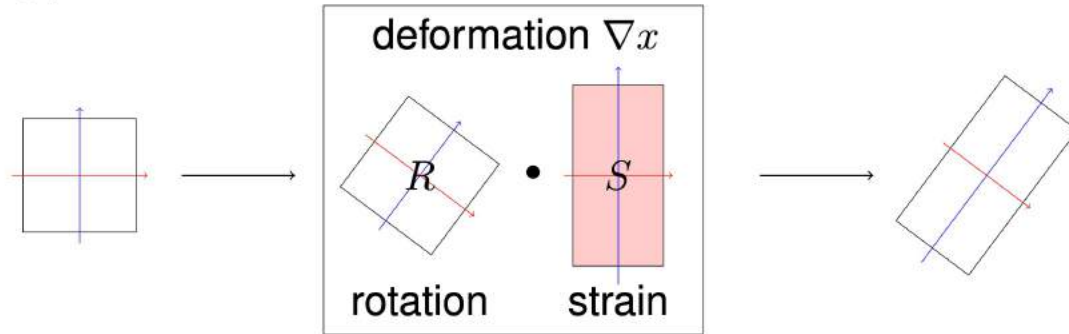
# The Source of Non-linearity

- In the deformation gradient  $\nabla x = RS$ 
  - Rigid rotation  $R$ , non-rigid strain  $S$



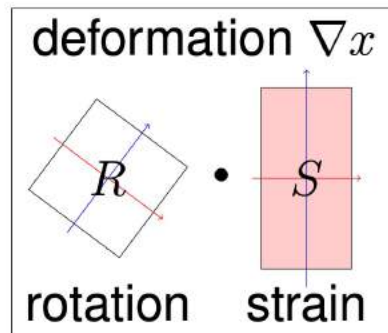
# The Source of Non-linearity

- In the deformation gradient  $\nabla x = RS$ 
  - Rigid rotation  $R$ , non-rigid strain  $S$
- The potential energy just measures the strain  $S$ 
  - $V(x)$  should not depend on rotation  $R$



# The Source of Non-linearity

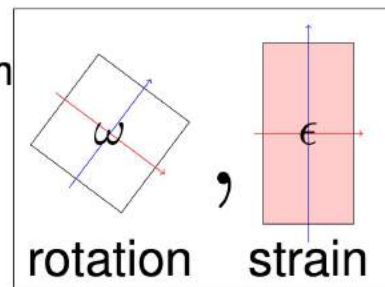
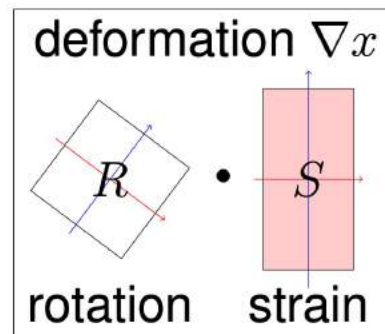
- Typical schemes to remove  $R$  from  $V$ 
  - Co-rotational:  $R^T \nabla x = S$
  - Cauchy-Green:  $\nabla x^T \nabla x = S^2$
  - Invariants: e.g.  $\det(\nabla x)$
- Rotation and strain are mixed in  $\nabla x$ 
  - Non-linear operation needed to decouple them



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  - Invariants: e.g.  $\det(\nabla x)$
- Rotation and strain are mixed in  $\nabla x$ 
  - Non-linear operation needed to decouple them
- Rotation-Strain Coordinates  $y = (\omega, \epsilon)$ 
  - Separately encode the rotation and strain

$$\omega = \log(R), \epsilon = S - Id$$



## From $y$ back to $x$

- Solve Poisson problem

$$x = \operatorname{argmin}_{x^*} \int_{\Omega} \left\| \nabla x^* - \underbrace{\exp(\omega)}_{\mathbf{R}} \underbrace{(\epsilon + Id)}_{\mathbf{S}} \right\|^2, \quad \text{s. t. } \frac{\int_{\Omega} x dV}{\int_{\Omega} dV} = c$$

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$$x = \Psi(y)$$

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$$x = \Psi(y)$$

- Part of nonlinearity in  $V(x)$  has been shifted into  $\Psi$



# Reduced RS coordinate

- For infinitesimal deformation

$$\nabla x = Id + \nabla u = Id + \underbrace{\frac{\nabla u + (\nabla u)^T}{2}}_{\epsilon(u)} + \underbrace{\frac{\nabla u - (\nabla u)^T}{2}}_{\omega(u)}$$

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$\omega$  and  $\epsilon$  are linear in  $u$ :  $(\omega, \epsilon)^T = Qu$

- Modal basis  $W \in \mathbb{R}^{3N \times r}$ 
  - A subset of small deformation modes

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$\omega$  and  $\epsilon$  are linear in  $u$ :  $(\omega, \epsilon)^T = Qu$

- Modal basis  $W \in \mathbb{R}^{3N \times r}$ 
  - A subset of small deformation modes
- Form modal coordinate to Euclidean coordinate

$$z \xrightarrow{W} \bar{u} \xrightarrow{Q} (\omega, \epsilon) \xrightarrow{\exp} \nabla \bar{x} \xrightarrow{\Psi} x$$

# As geometric warping

- Fast integration: Cubature [*Ann et al. 2008*]

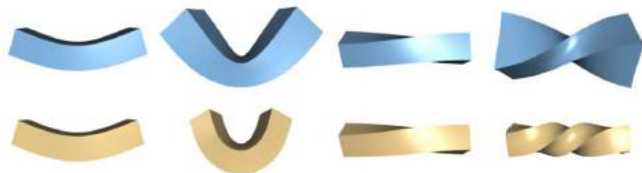


# As geometric warping

- Fast integration: Cubature [Ann et al. 2008]



- Warping for subspace deformation



**Space-time editing [Li 2014]**

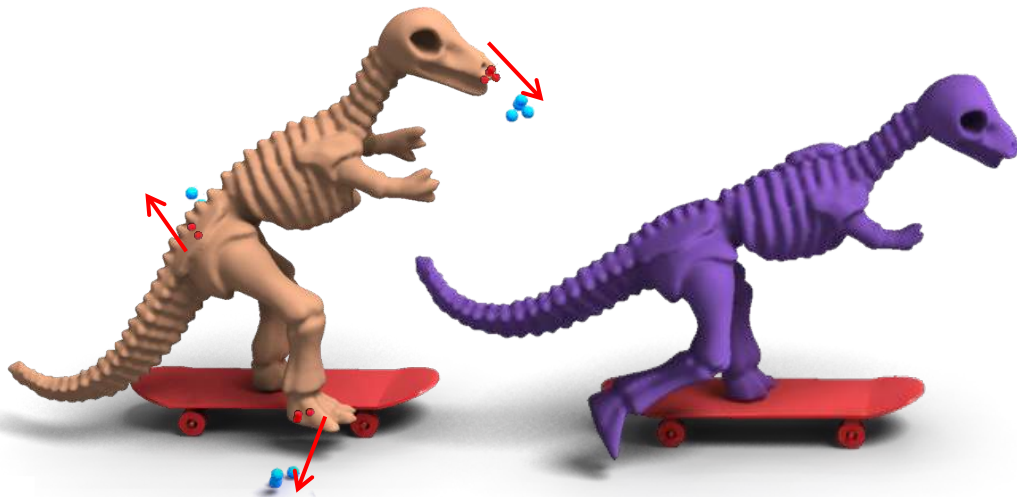
# Introduction

## *Space-time editing*

- Powerful tool for animation editing
- Seeking minimal **control forces**
- Matching the **constraints in space-time**.



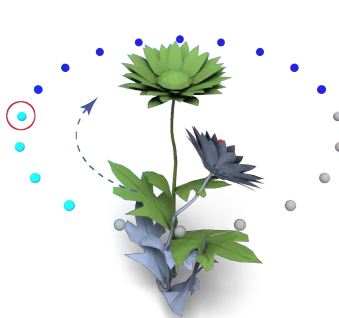
Dynamic or static input  
animation



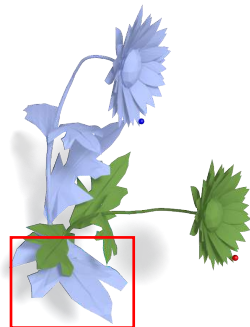
Positional and/or keyframe constraints

# Unsolved problems in practice

- Scalability for complex models
- Lack of control due to linearization



[Barbič et al. 2012]



[Li et al. 2013]

- Elastic material significantly affects animation
  - What is the *right* material?



# Technical contributions

We propose two new techniques to solve these problems.

- ***Reduced RS (Rotation-Strain) approach***

Provides tight positional constraints under large deformation.

- ***Material Optimization***

Provides physically plausible and consistent results.

# Space-Time Editing

For efficiency, we formulate the problem in modal coordinates

Modal coordinates  $\longrightarrow$   $\boxed{z}$   $\arg \min E_f(z) + \gamma E_c(z)$

$$\left\{ \begin{array}{l} E_f(z) = \frac{1}{2} \sum_{i=2}^{Frames-1} \|\ddot{z}_i + D\dot{z}_i + \Lambda z_i\|_2^2 \\ E_c(z) = \frac{1}{2} \sum_{(i,j) \in C} \|u_i^j(W, z_i) - \hat{u}_j^i\|_2^2 \end{array} \right.$$

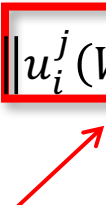
Measures control forces

Measures error in constraints

# Space-Time Editing

For efficiency, we formulate the problem in modal coordinates

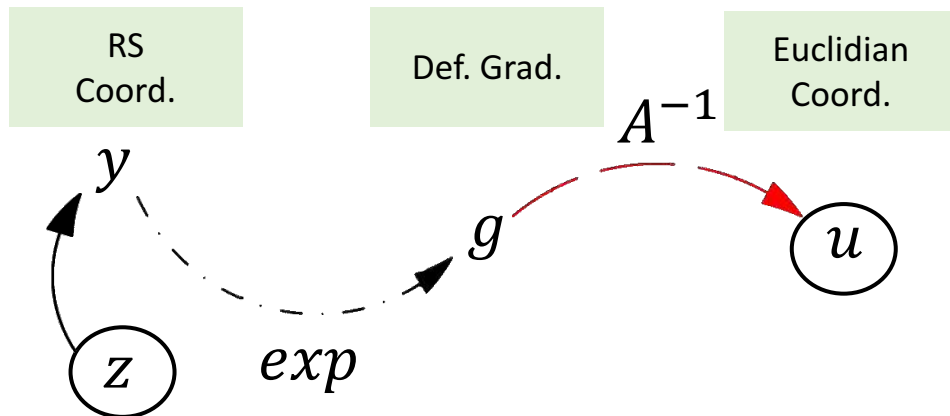
$$\arg \min_z E_f(z) + \gamma E_c(z)$$

$$\left\{ \begin{array}{l} E_f(z) = \frac{1}{2} \sum_{i=2}^{Frames-1} \|\ddot{z}_i + D\dot{z}_i + \Lambda z_i\|_2^2 \\ E_c(z) = \frac{1}{2} \sum_{(i,j) \in C} \|u_i^j(W, z_i) - \hat{u}_j^i\|_2^2 \end{array} \right.$$


*Euclidean coordinates reconstruction*

- Must be robust to large deformation.
- Should only require local evaluations for efficiency.

# Rotation-Strain



Proposed by [Huang et al. 2011].

- Compute  $y, g$  for all elements.
- Solving global linear eq.

$$Au = G^T \bar{V} g(y)$$

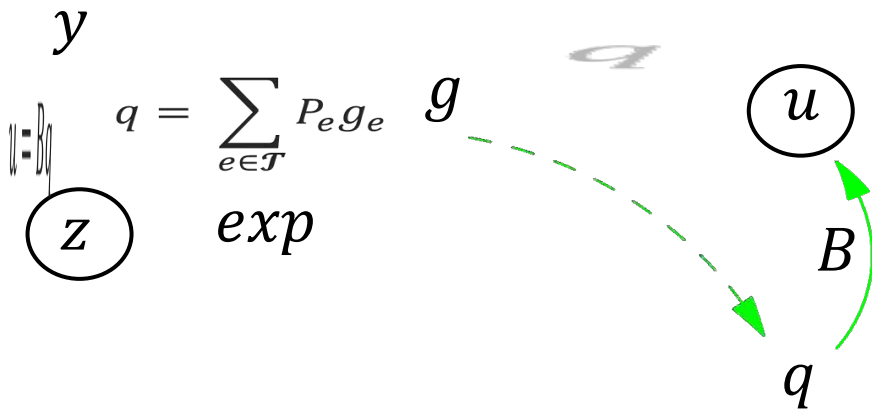
*Inefficient for local evaluations*

# Reduced Rotation-Strain

RS  
Coord.

Def. Grad.

Euclidian  
Coord.



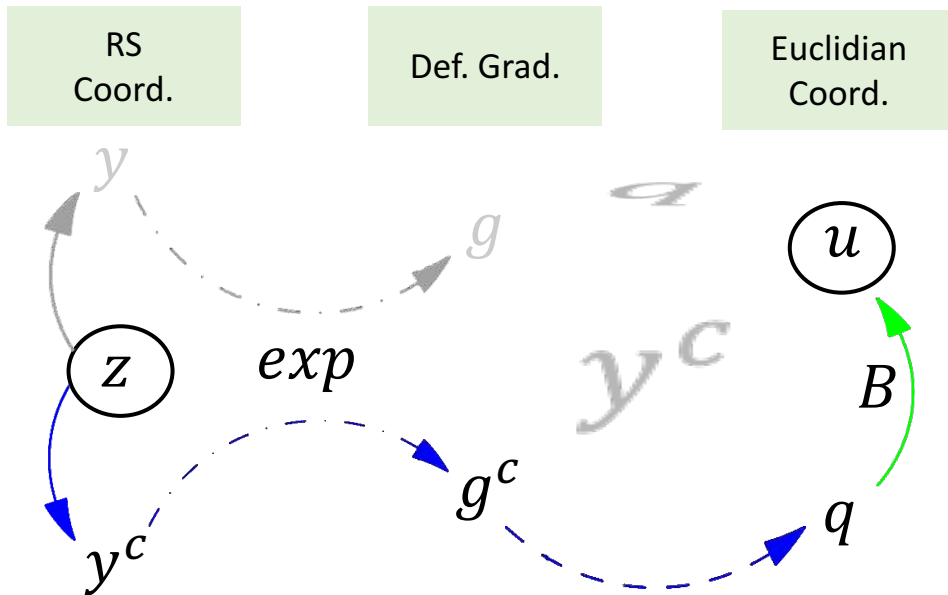
- Geometric reduction.
- Cubature method.

$$u = Bq$$

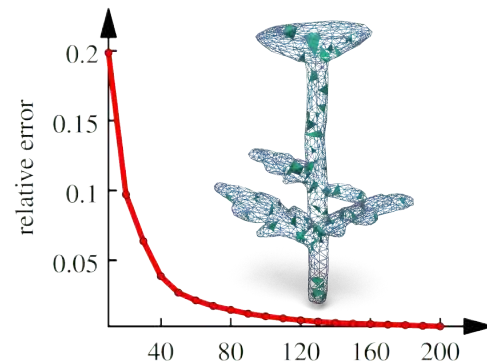
$$q = \sum_{e \in \mathcal{T}} P_e g_e$$

*Avoid global linear solve.*

# Reduced Rotation-Strain



- Geometric reduction.
- Cubature method.



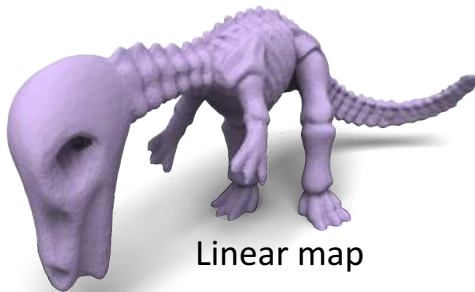
**Compute RS for cubature only.**  
**Partial shape reconstruction**

# Comparison

Different method for the mapping from  $z$  to  $u$



Rest shape



Linear map



RS



Reduced RS

## *Reduced RS method*

- Robust to large deformation.
- Two orders of magnitude faster than full RS.
- Allows local evaluations of 3D coordinates.



# Material optimization

*How to pick a good elastic material?*

***Introduce material as new DOFs, and Optimize!***

$$\arg \min_{z, \Lambda, D, W} E_f(z, \Lambda, D) + \gamma E_c(W, z)$$

Material in modal space: frequency, damping, and modal basis.



# Material optimization

*How to set the proper elastic material?*

*Introduce material as new DOFs, and Optimize it!*

$$\arg \min_{z, \Lambda, D, W} E_f(z, \Lambda, D) + \gamma E_c(W, z)$$

Material in modal space: frequency, damping and modal basis.

Dimension is too large, so introduce **basis sampling**,

$$W = \hat{W}S$$

Optimize **smaller** sampling basis  $S$  instead of  $W$ .

# Material optimization

Formulation for material optimization

Regularization term.

$$\arg \min_{z, \Lambda, D, S} E_f(z, \Lambda, D) + \gamma E_c(S, z) + \mu E_s(S)$$

$$\text{subject to } \lambda_k, d_k \geq 0 \quad \forall k \in [1, r]$$

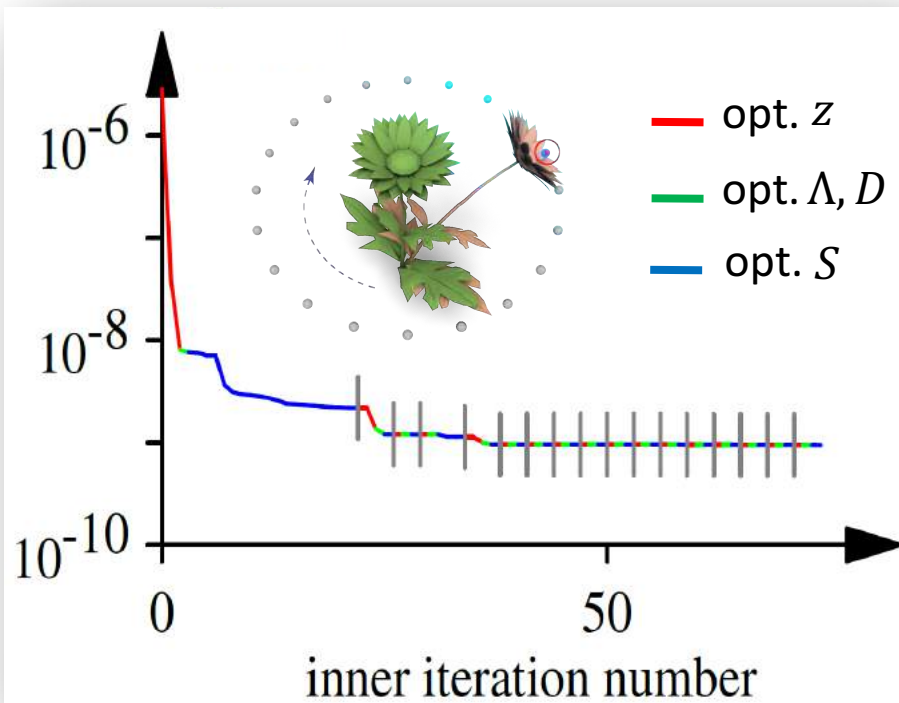
***Nonlinear, but all variables are in subspace.***

# Numerical method

Optimize the variables one by one

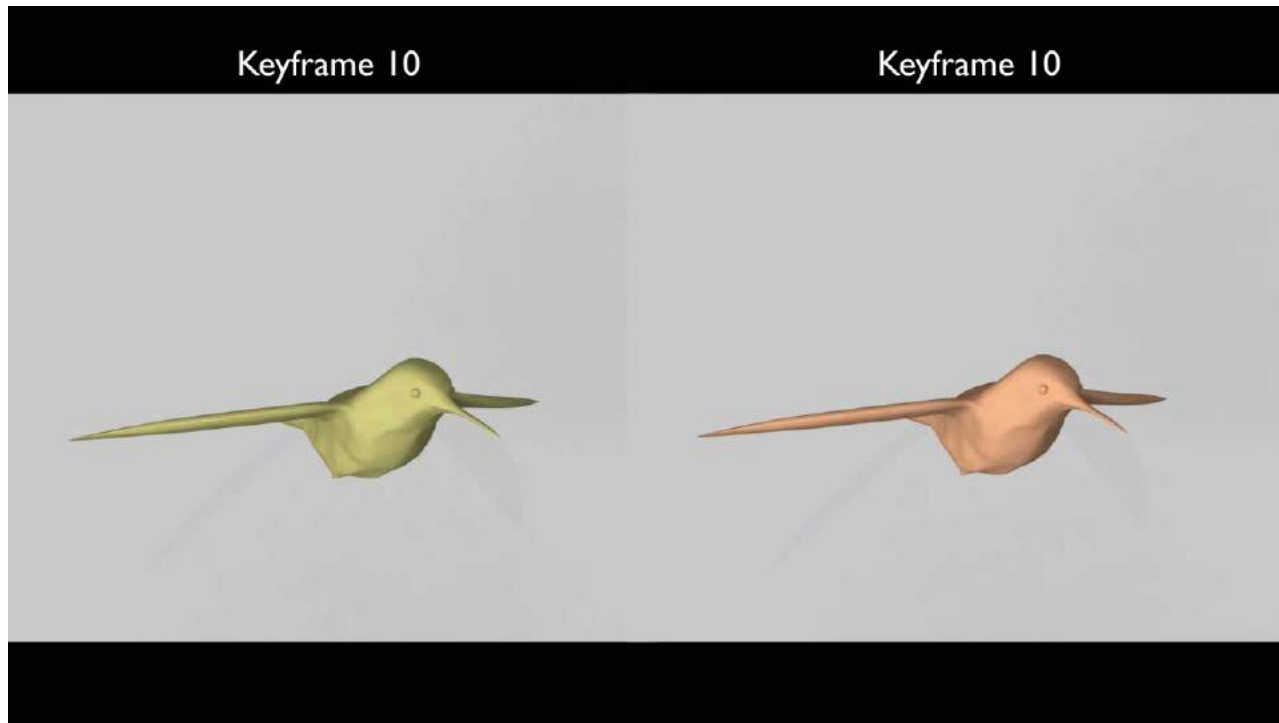
- Fix  $\Lambda, D, S$ , optimize  $z$
- Fix  $z, S$ , optimize  $\Lambda, D$
- Fix  $z, \Lambda, D$ , optimize  $S$

*Guarantees monotone decrease!*



# Animation editing

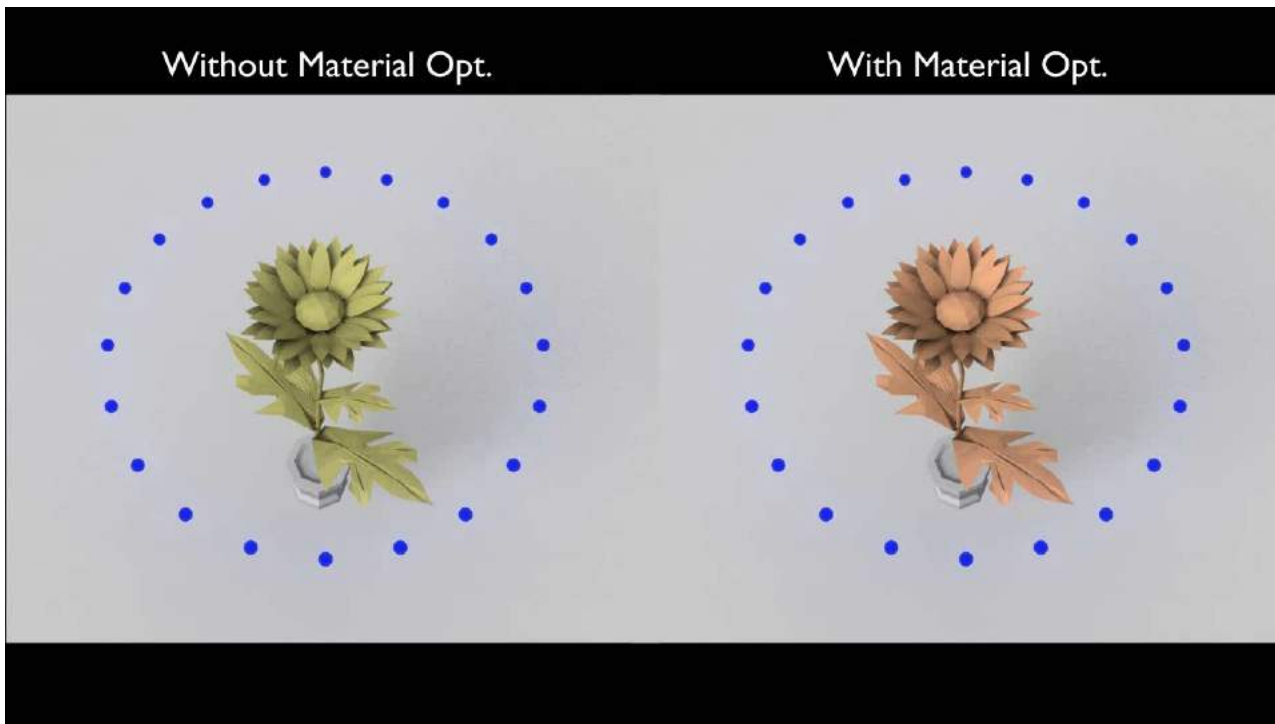
With material optimization, the resulting animation is more consistent!



# Animation editing

With material optimization, the resulting animation is more ***consistent!***

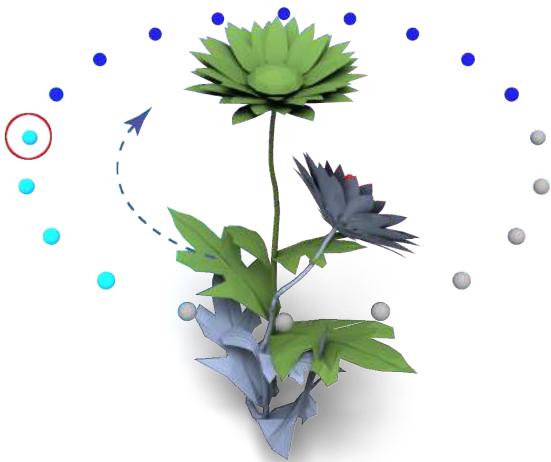
Abrupt  
suddenly



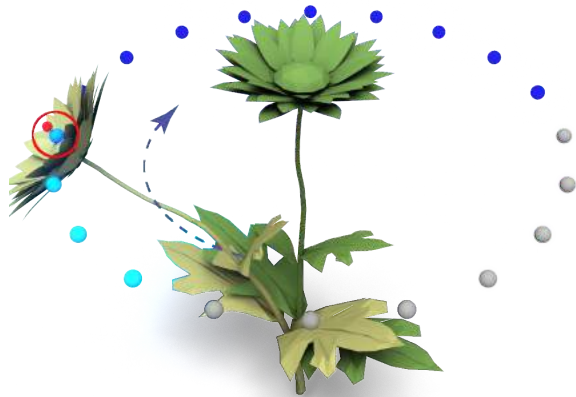
Keep  
circular  
motion

# Comparison

Our method provides ***tight positional constraints***, even for large edits.



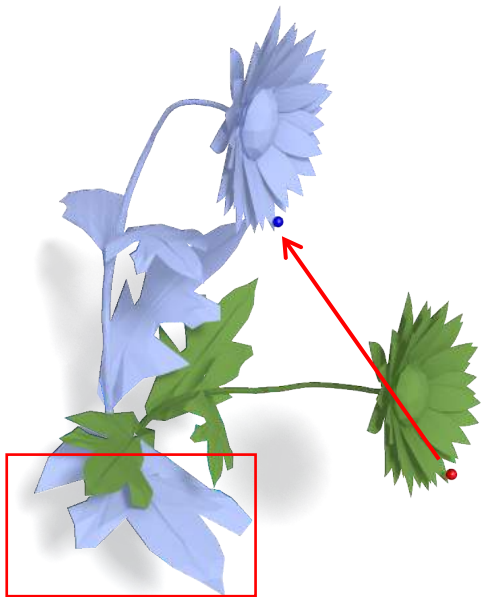
[Barbič et al. 2012]



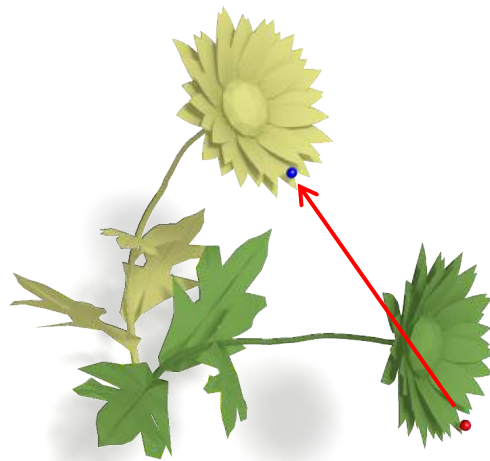
Our result

# Comparison

Our method supports *large edits* without visual artifacts.



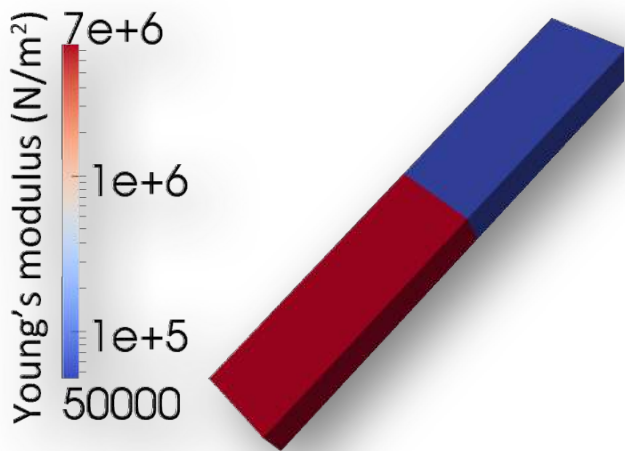
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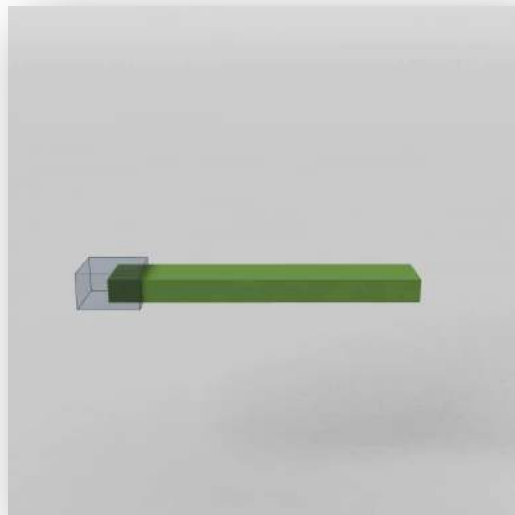
Our result

# Recovering material parameters

We use input animation as keyframes in the space-time editing.



Non-uniform material for  
the experiments.

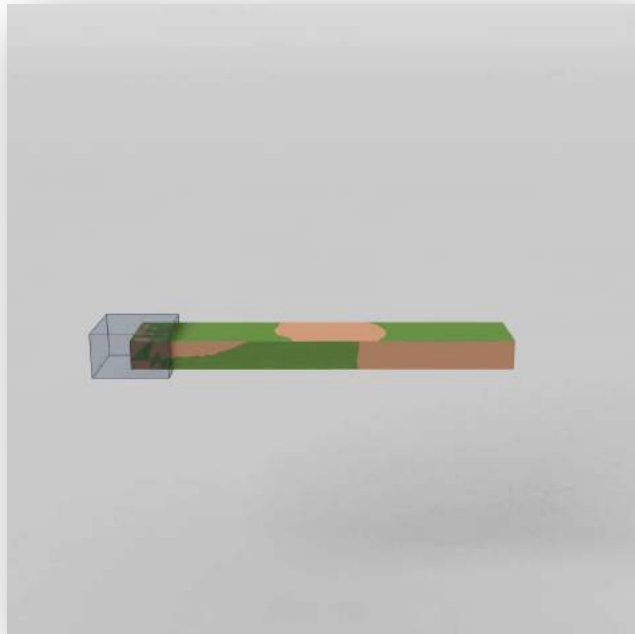


Input animation, with  
first 150 frames as constraints,  
last 150 frames for comparison.

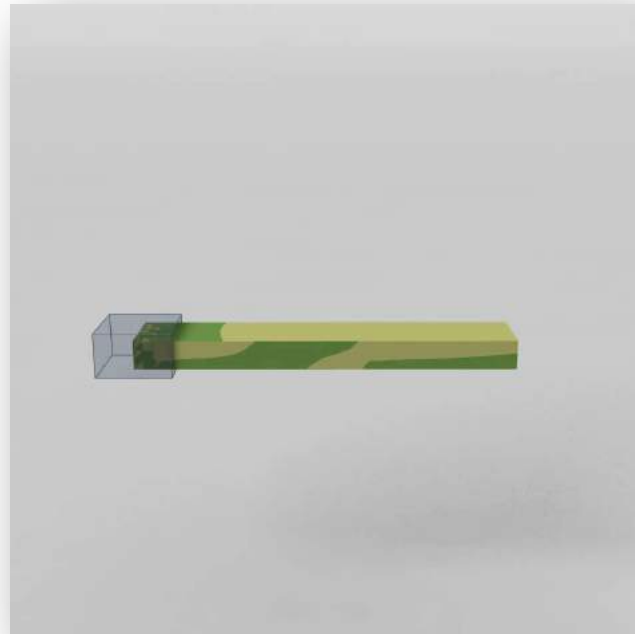


# Recovering material parameters

*Compare the simulated results with the last 150 frames.*



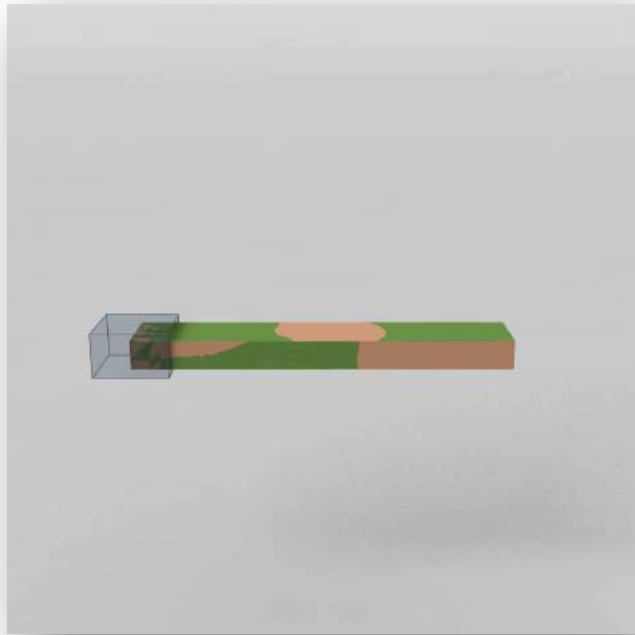
***Recovered*** material



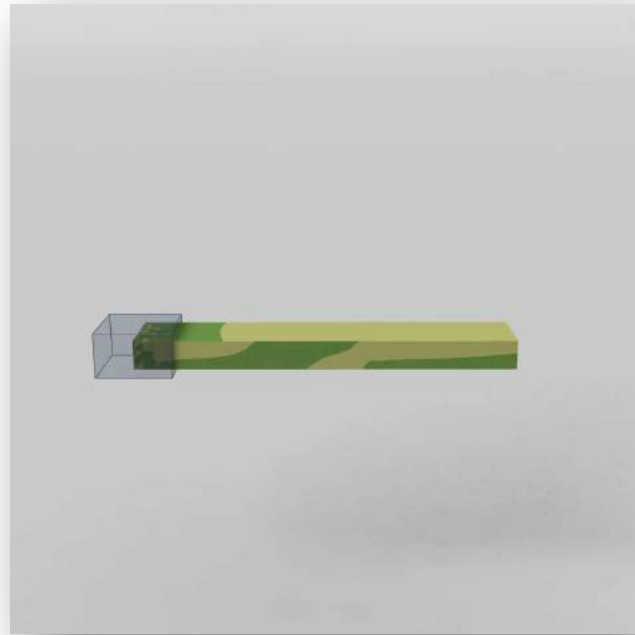
***Uniform*** material

# Recovering material parameters

*Compare the simulated results with the last 150 frames.*



***Recovered*** material



***Uniform*** material

T.rex King Kong

## **General simulation [Pan 2015]**

# Rotation-Strain Space

- RS as general coordinate

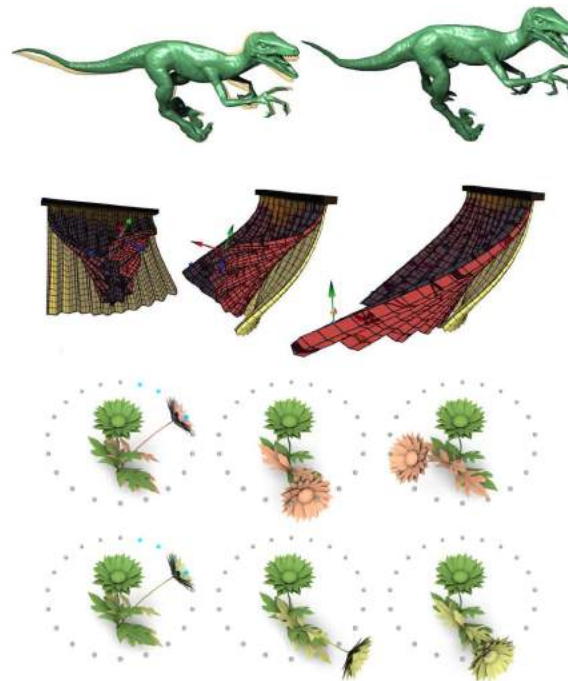
$$y = (\omega, \epsilon)$$

- Potential energy  $V(y) = V(\epsilon)$

- Reduce the non-linearity a lot!

- For linear elastic material:

$$V(y) = \frac{1}{2} y^T \tilde{K} y$$



# Rotation-Strain Space

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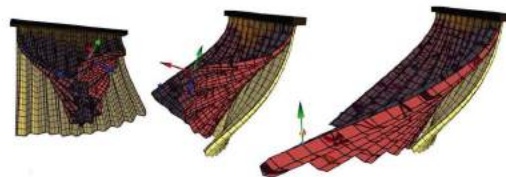
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- Kinetic energy  $T$ ?



# Rotation-Strain Space

- RS as general coordinate

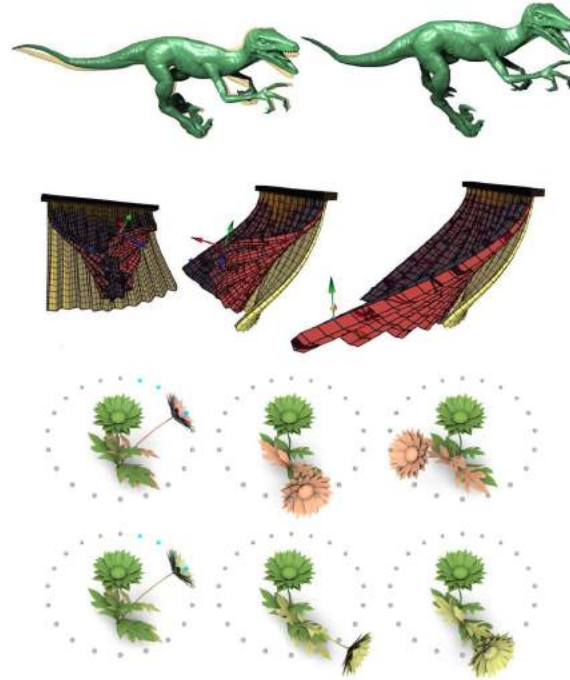
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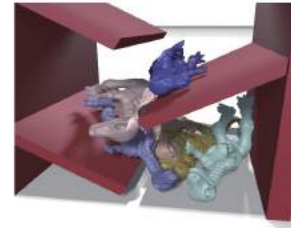
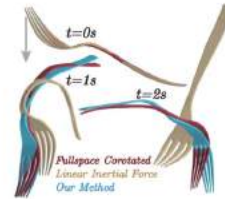
$$V(y) = \frac{1}{2} y^T \tilde{K} y$$

- Kinetic energy  $T$ ?
- External force  $g$ ?



# Contributions of This Paper

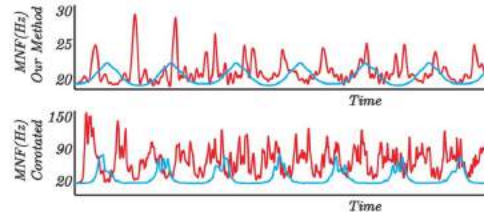
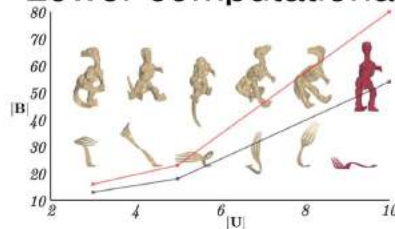
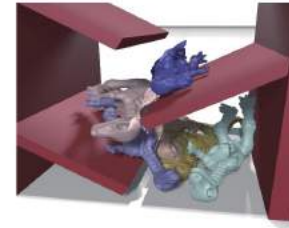
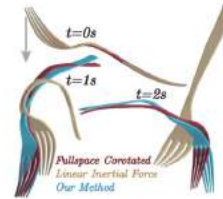
- A full featured dynamical model in RS space
  - Non-linear elastic material
  - Correct kinetic energy
  - External force and constraints





# Contributions of This Paper

- A full featured dynamical model in RS space
  - Non-linear elastic material
  - Correct kinetic energy
  - External force and constraints
- Advantages
  - Lower dimensional subspace for dynamics
  - Lower computational complexity



# Non-linear Elastic Material

- Directly apply to strain  $\epsilon$ 
  - StVK material using Green-Lagrange strain  $\frac{1}{2}(J^T J - I) = \frac{1}{2}\epsilon^2 + \epsilon$
- Replace Green-Lagrange strain by Cauchy strain
  - Less non-linearity but still rotation invariant

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- Replace Green-Lagrange strain by Cauchy strain
  - Less non-linearity but still rotation invariant
- For example, Fung's model

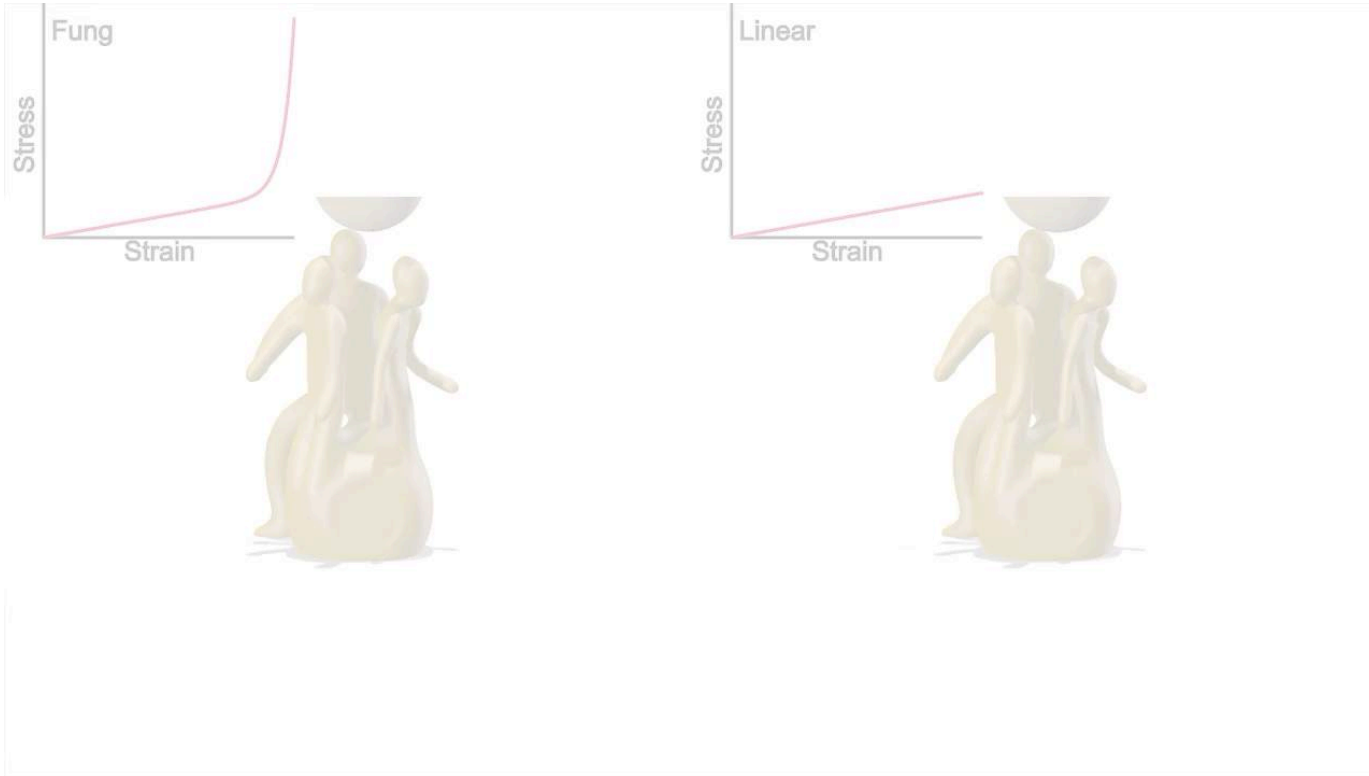
$$W_{StVK}(J, \mu_1, \lambda_1) + c \left( e^{W_{StVK}(J, \mu_2, \lambda_2)} - 1 \right)$$

$\Rightarrow$

$$\frac{1}{2}y^T K_1 y + c \left( e^{\frac{1}{2}y^T K_2 y} - 1 \right)$$



# Video



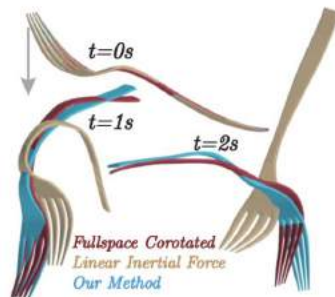
# Correct Kinetic Energy

- Substitute  $y$  into  $T(\dot{x})$

$$T(\dot{y}, y) = \frac{1}{2} \dot{x}(y)^T M \dot{x}(y) = \frac{1}{2} \dot{y}^T \left( \frac{\partial x^T}{\partial y} M \frac{\partial x}{\partial y} \right) \dot{y}$$

- From the Lagrange  $L = T - V$

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{y}} - \frac{\partial L}{\partial y} = 0 \Rightarrow \boxed{\frac{\partial x}{\partial y}}^T M \ddot{x} + \frac{\partial V}{\partial y} = 0$$



# Correct Kinetic Energy

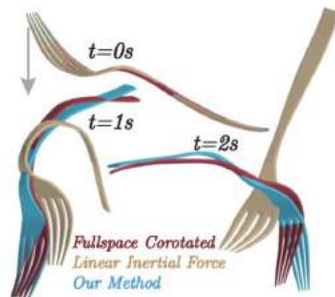
- Substitute  $y$  into  $T(\dot{x})$

$$T(\dot{y}, y) = \frac{1}{2} \dot{x}(y)^T M \dot{x}(y) = \frac{1}{2} \dot{y}^T \left( \frac{\partial x^T}{\partial y} M \frac{\partial x}{\partial y} \right) \dot{y}$$

- From the Lagrange  $L = T - V$

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{y}} - \frac{\partial L}{\partial y} = 0 \Rightarrow \boxed{\frac{\partial x}{\partial y}}^T M \ddot{x} + \frac{\partial V}{\partial y} = 0$$

- More details in the paper
  - Coupling with floating frame
  - Temporal discretization



# External Force and Constraints

- Force  $g$ : gradient of a potential energy  $V_g$ 
  - E.g. gravity  $g$ :  $V_g(x) = mg^T x$
- Constraints
  - Equality  $c(x) = 0$
  - Inequality  $c(x) > 0$



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- Constraints

- Equality  $c(x) = 0$

- Inequality  $c(x) > 0$

- Involve the derivatives

$$\frac{\partial V_g}{\partial y} = \frac{\partial V_g}{\partial x} \frac{\partial x}{\partial y}, \quad \frac{\partial c}{\partial y} = \frac{\partial c}{\partial x} \frac{\partial x}{\partial y}$$





# Accelerate the Integration

- Identifying bottleneck
  - Coordinates transformation

$$(\epsilon, \omega) \xrightarrow{\tilde{\nabla}} \nabla \mathbf{x} \xrightarrow{\Phi} (x_1, x_2, x_3)$$

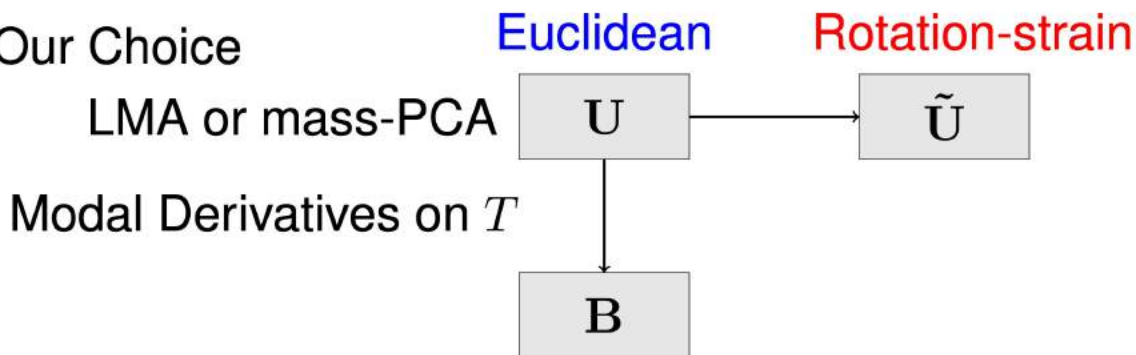
- Energy evaluation
  - Potential energy  $V(\epsilon)$
  - Kinetic energy  $T(x(y))$

# Inspiration

- Existing methods for Euclidean space simulation
  - Linear modal analysis [*Pentland and Williams 1989*]
  - Modal derivatives [*Barbič and James 2005*]
  - Polynomial precomputation [*Barbič and James 2005*]
  - Cubature [*Ann et al. 2008*]
- Natural to transfer these methods from Euclidean to RS.

# Choice of Basis

- Any set of basis can be used for  $x$  and  $y$  respectively
  - Set  $\tilde{U}, B$  to identity matrix  $\Rightarrow$  Full space
  - Fewer basis  $\Rightarrow$  Linear subspace
  - Expressivity and number of basis?
- Our Choice



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Euclidean

Rotation-strain

LMA or mass-PCA

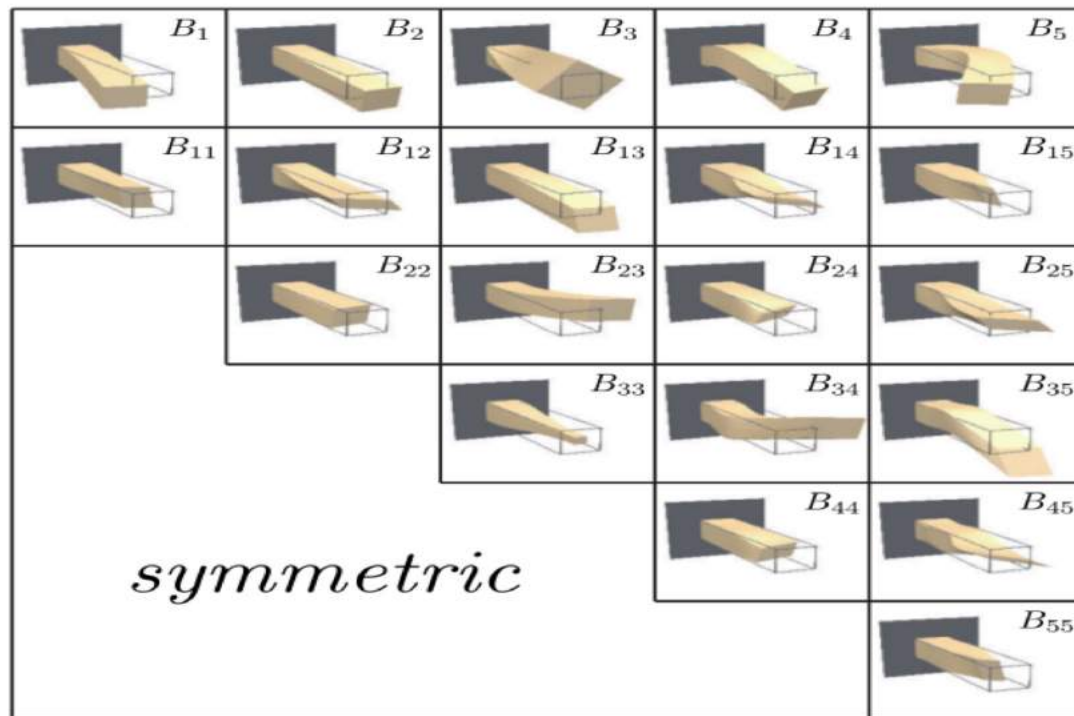
$U$

$\tilde{U}$

Modal Derivatives on  $T$

$$\left[ (\nabla^T D \nabla)^{-1} \nabla^T D \frac{\partial \tilde{\nabla}}{\partial y_i}(\mathbf{0}), (\nabla^T D \nabla)^{-1} \nabla^T D \frac{\partial \tilde{\nabla}}{\partial y_i y_j}(\mathbf{0}), \right]$$

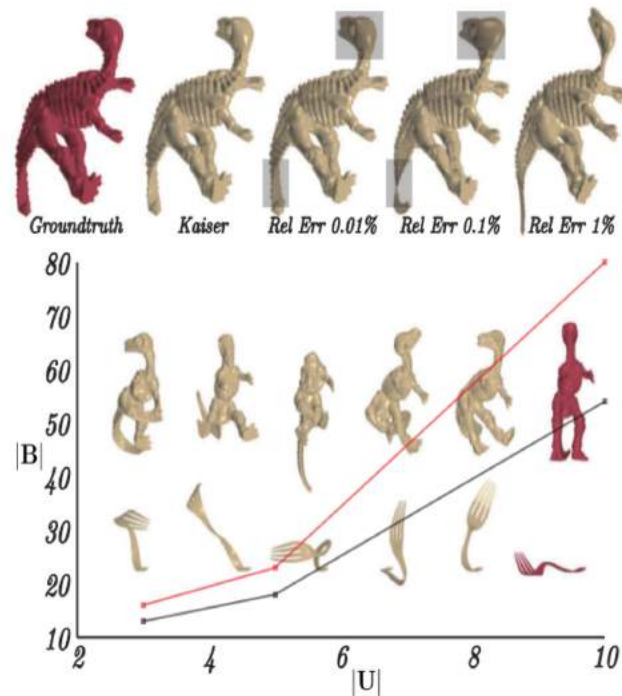
# Choice of Basis



# Validation

## Experiment Settings

- Run simulation with  $B = Id$  and  $\tilde{U} = 3, 5, 10$
- Reconstruct the shape using reasonably small subspace  $B$
- Truncation criterion
  - $\lambda_i > 1$
  - $\lambda_i > 0.01\% \lambda_{max}$

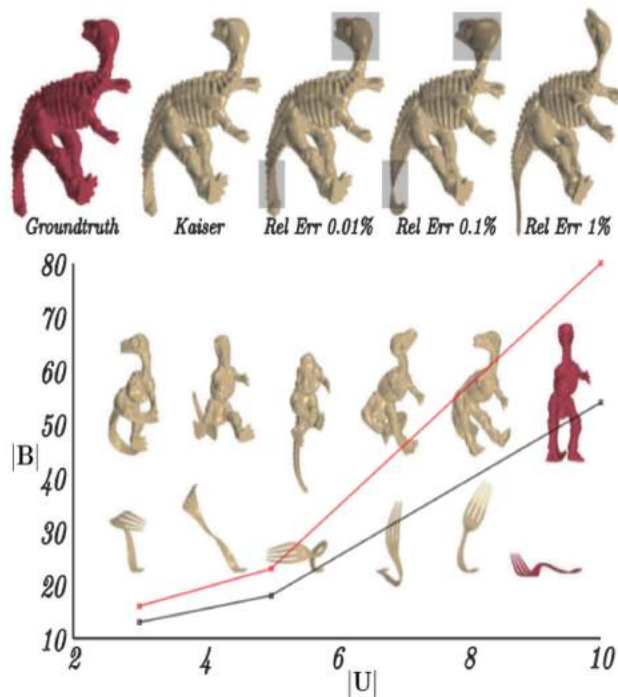


# Validation

## Experiment Settings

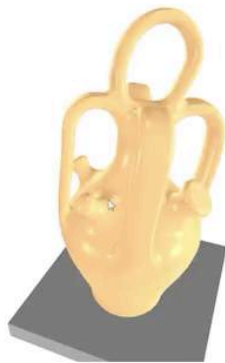
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$$|\mathbf{B}| = \mathcal{O}(|\tilde{\mathbf{U}}|^2)$$

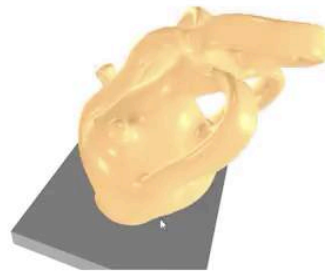


## Realistic Dynamics

Our Method  $p=3$   $q=2$   
FPS: 25

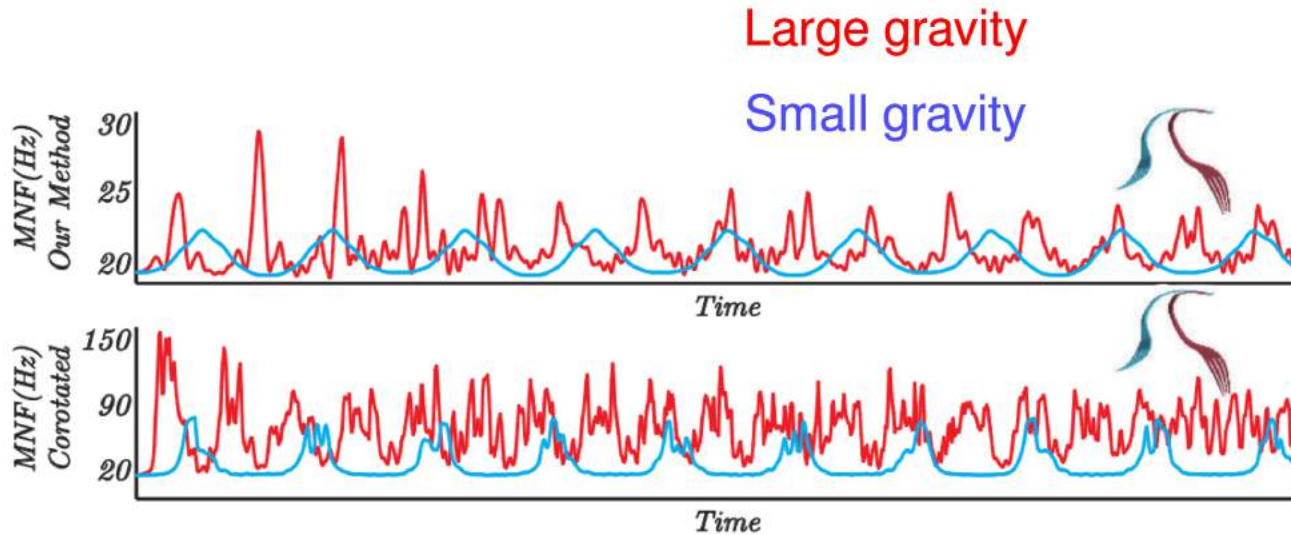


Our Method Cubature  
FPS: 88



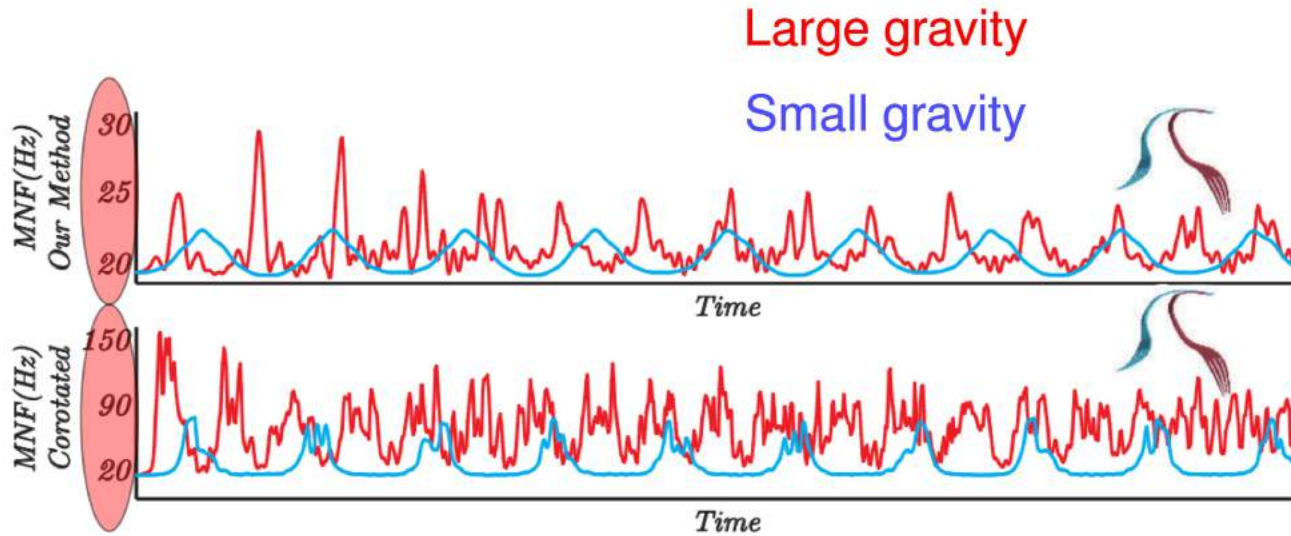


# Results



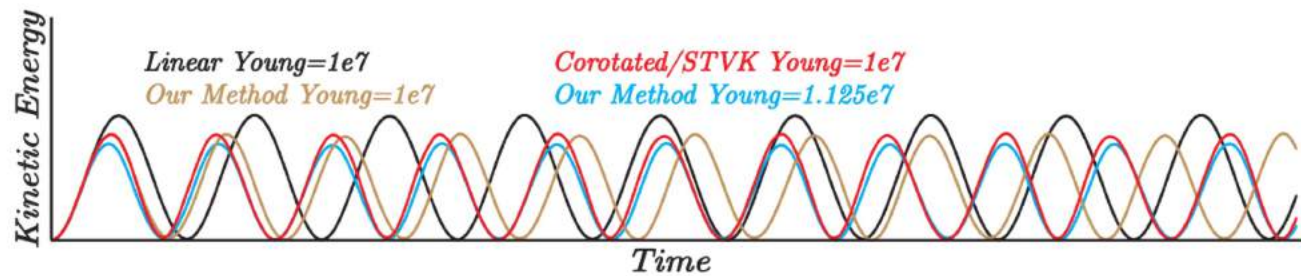
- 2s simulation run on the fork model
- Numerical indicator for nonlinearity → MNF: **M**inimal **N**atural **F**requency
- $\sqrt{\lambda^*}$ ,  $\lambda^* = \operatorname{argmin}_{\lambda} \lambda \mathbf{M} \mathbf{v} = \mathbf{K} \mathbf{v}$

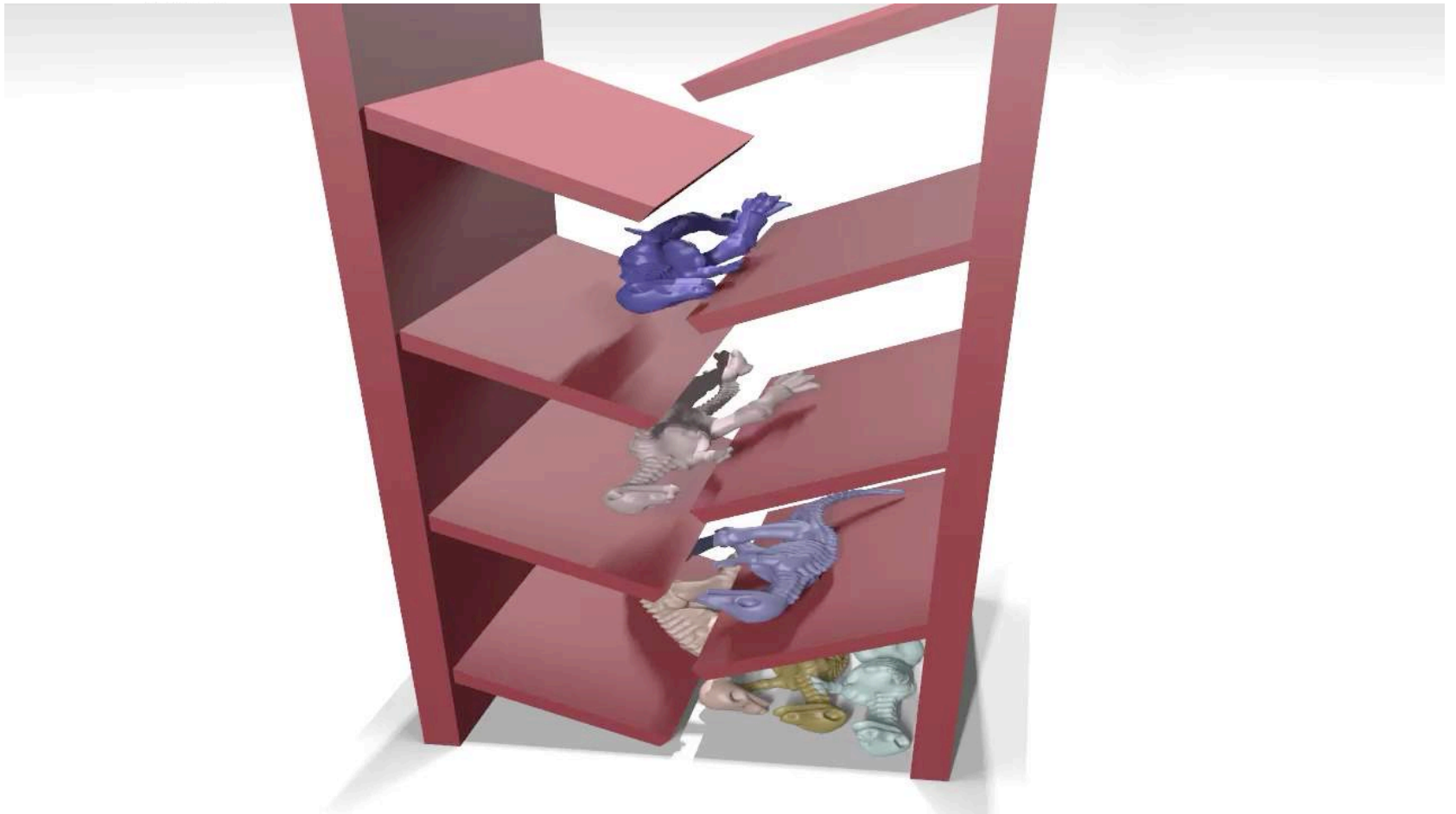
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# Results





# Future work

- Intrinsic representation of elasticity
  - Redundant DOFs:  $9|T|$  v.s  $3|N|$
  - Pure strain representation
  - Embeddable condition (integratable condition)
- Physically accurate warping
  - Change rotation extrapolation function, e.g. Cayley mapping
  - Introduce material-aware metric for Poisson construction

**Thank you!**