



Frame Field-Driven Quad- and Hex-Remeshing

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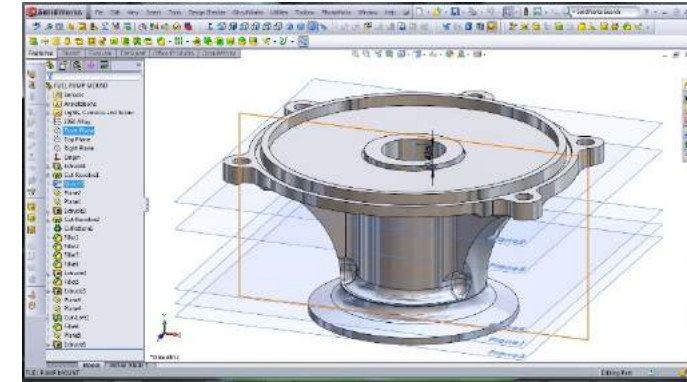
State Key Lab of CAD&CG, Zhejiang University

2020.02.27

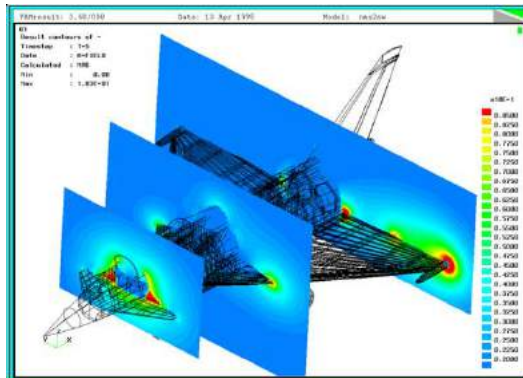
www.xzfang.top

Background

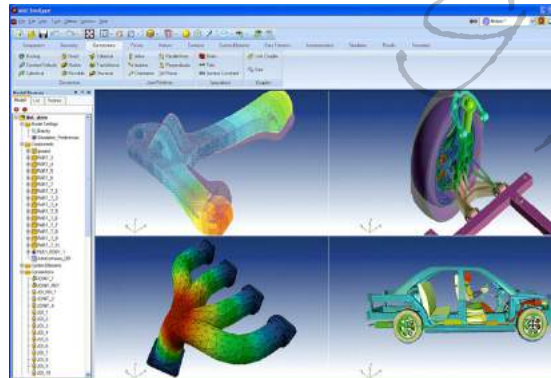
- CAD & CAE & CAM
- 3D models are widely used
- Use Mesh to represent models
- Remeshing



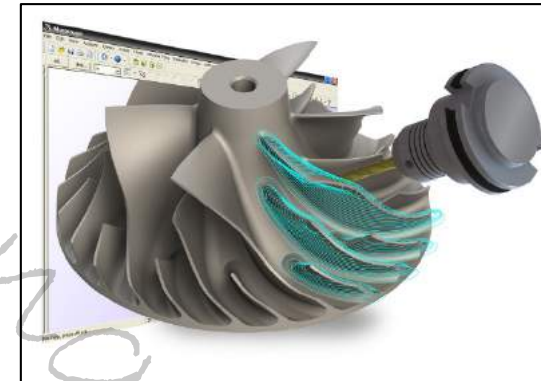
CAD



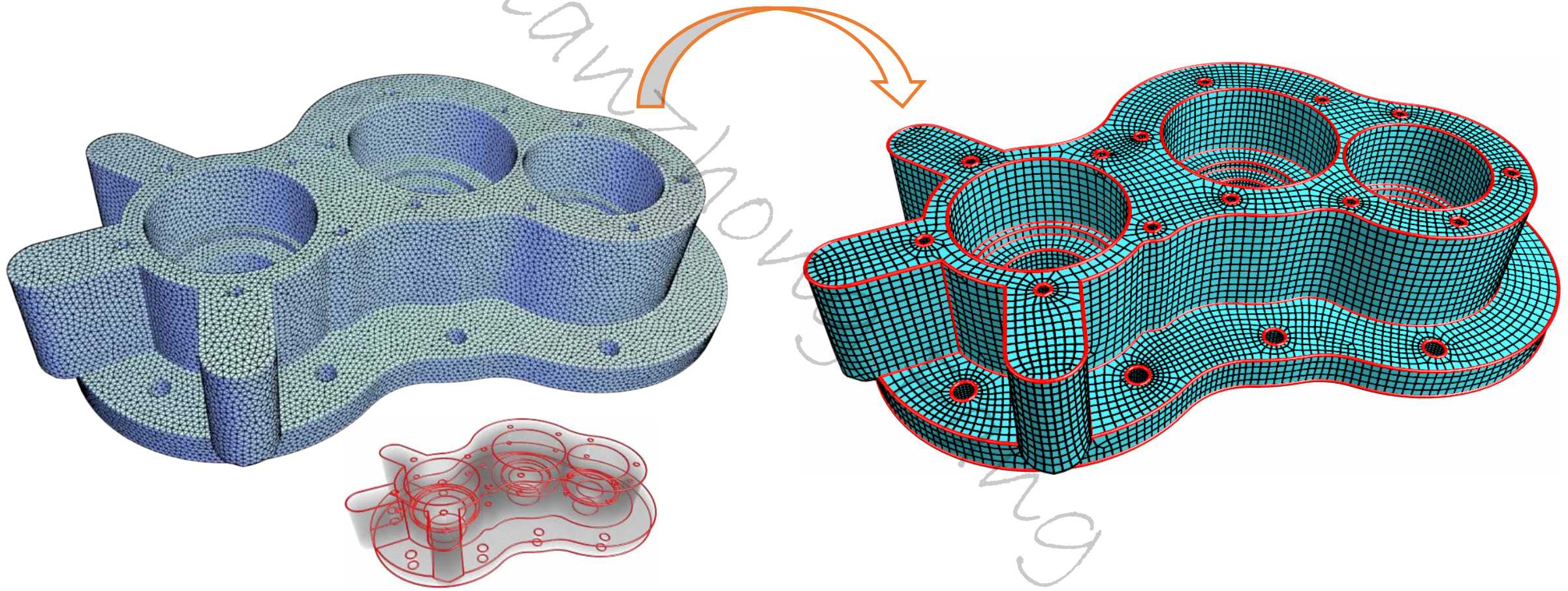
CAE



CAM



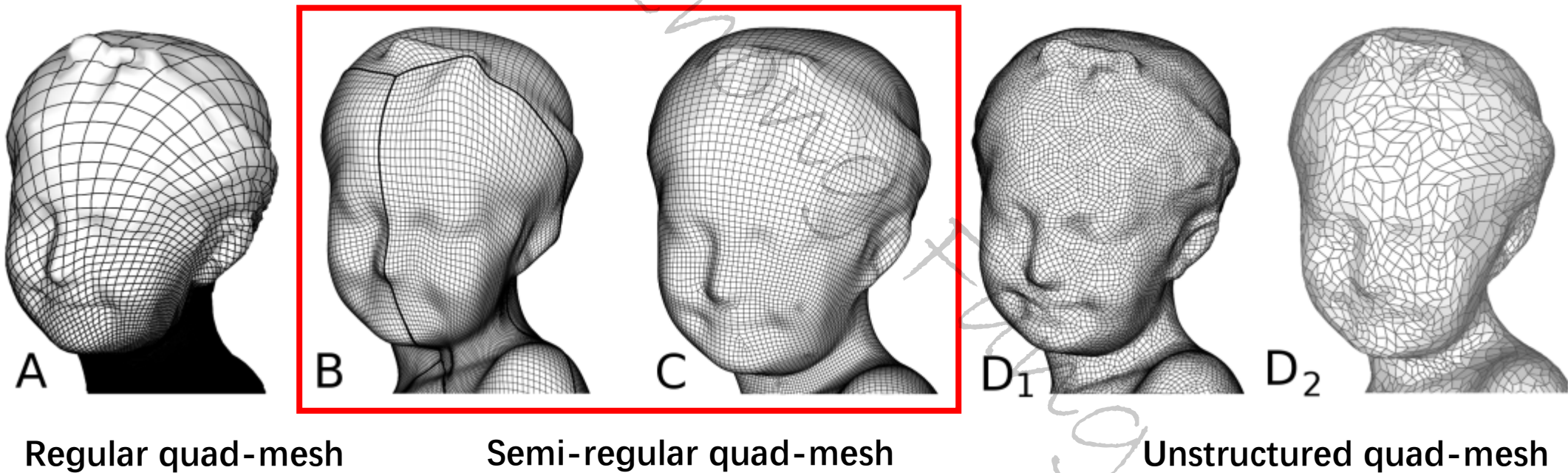
Remeshing



Frame field-driven quad- and hex-remeshing

Semi-Regular Mesh

- High computational accuracy
- Less elements

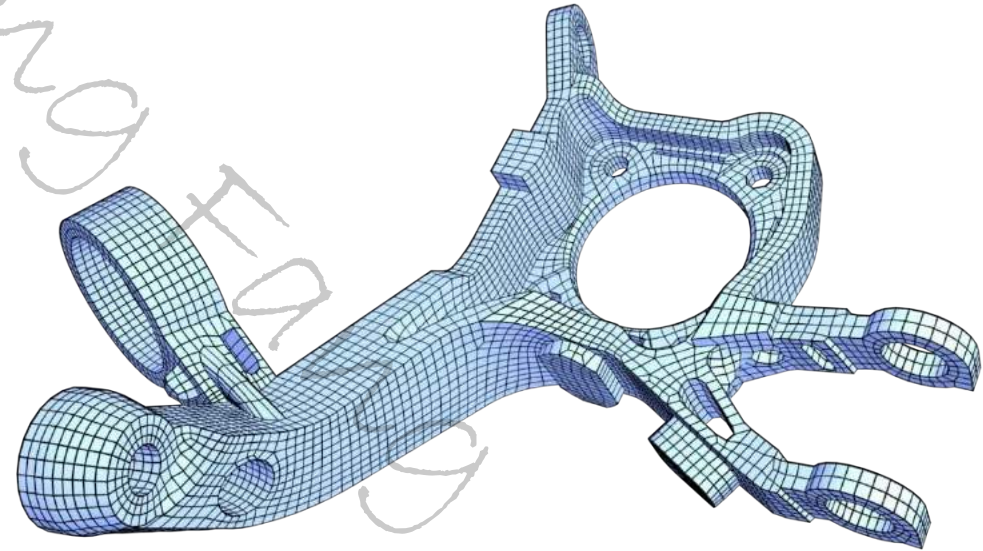
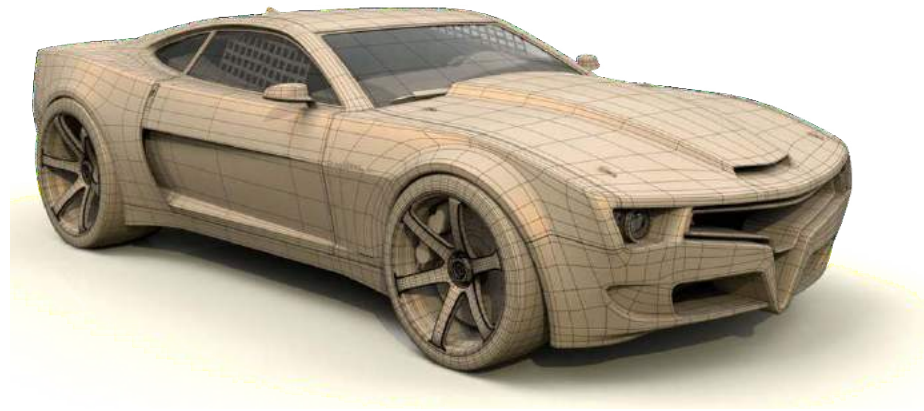


[Bommes et al. CGF 2013]

Applications

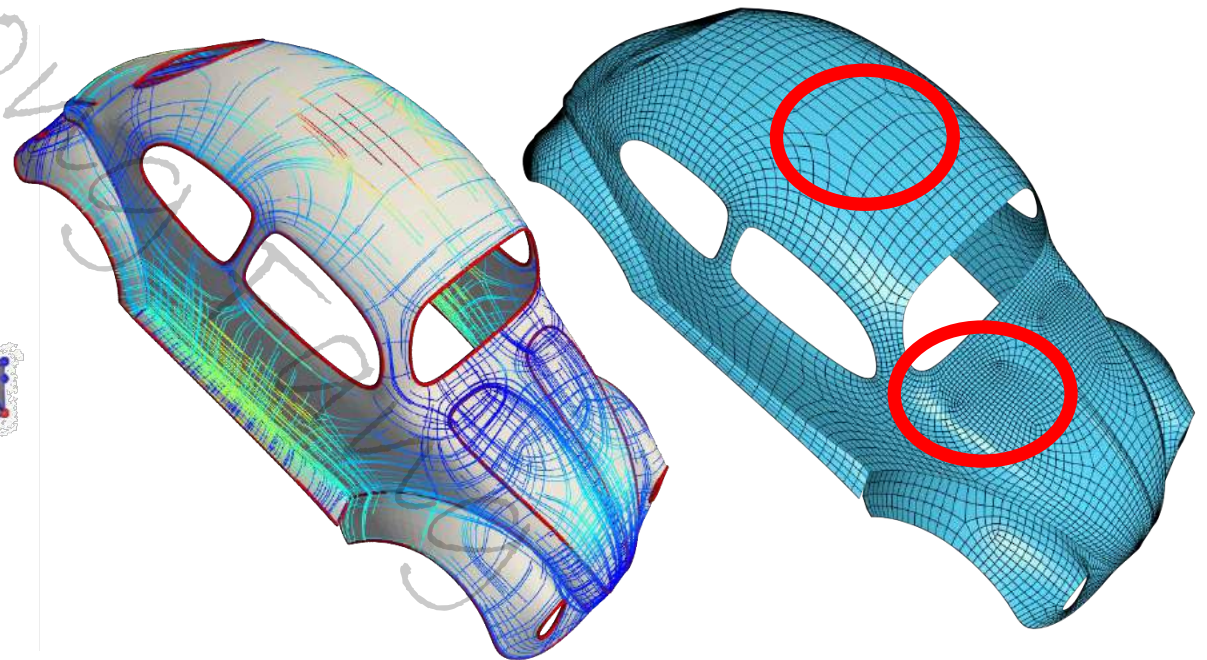
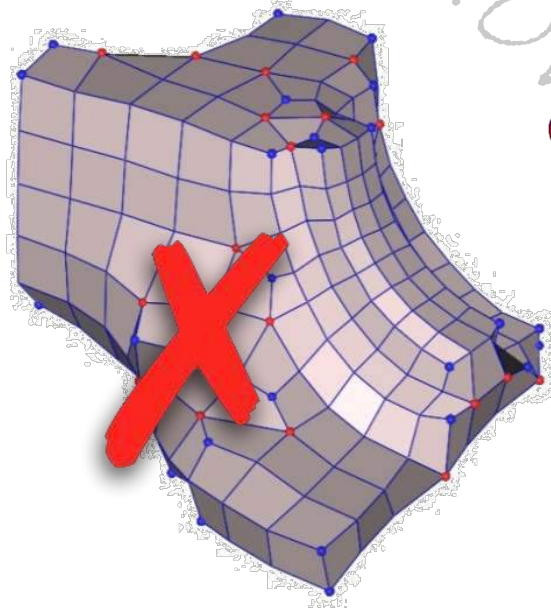
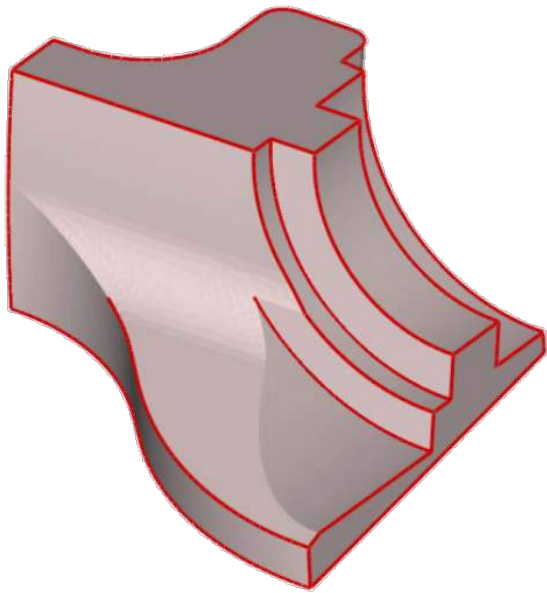
- B-spline fitting
- Simulation
- Reverse Engineering

- Finite Element Method
- Engineering Analysis
- ...



Requirements of Remeshing

- Low Hausdorff distance
- Feature preservation
- Good element shape
- Controllable: direction & size
- Robustness & efficiency



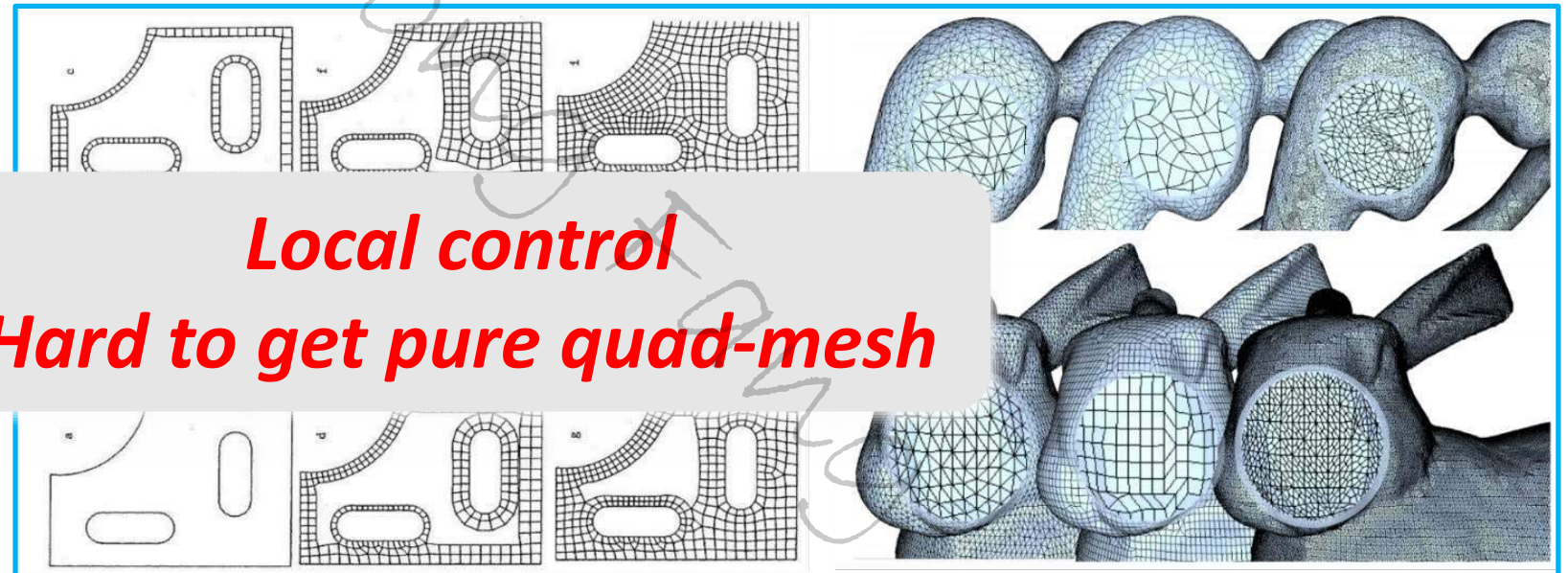
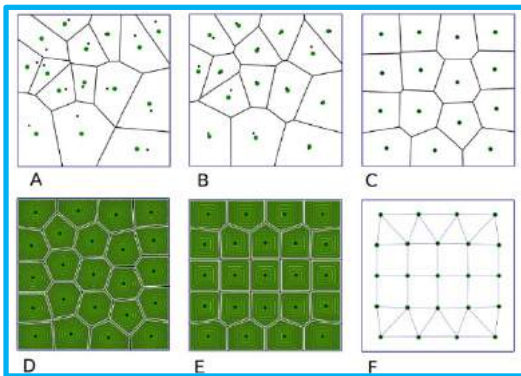
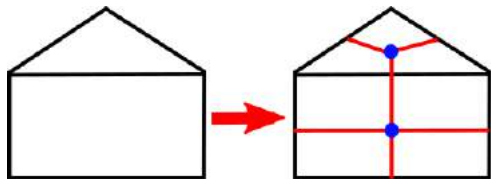


Methods of Remeshing

- Computational geometry
- Differential geometry

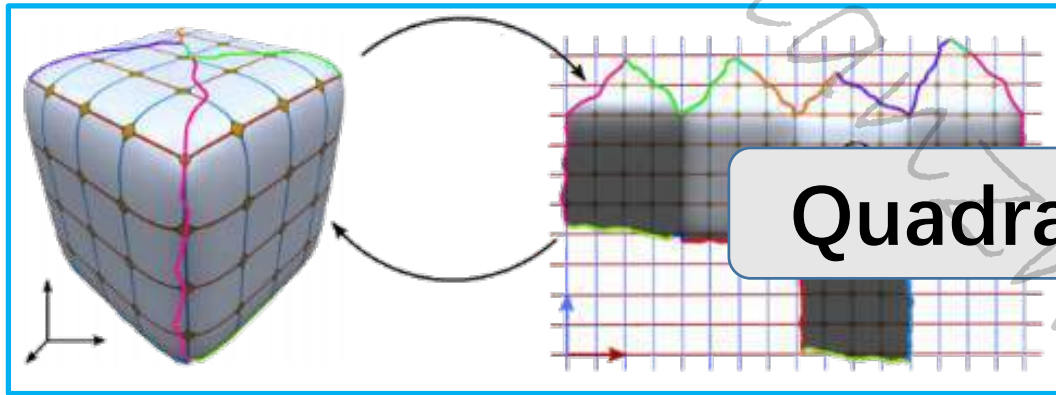
Computational geometry methods

- Catmull-Clark subdivision [Catmull and Clark '78]
- Advance front [Owen et al. '99]
-
- Tri-to-quad conversion [Gurung et al. '11, Remacle et al. '11]
- Voronoi diagram [Lévy and Liu '10]
-



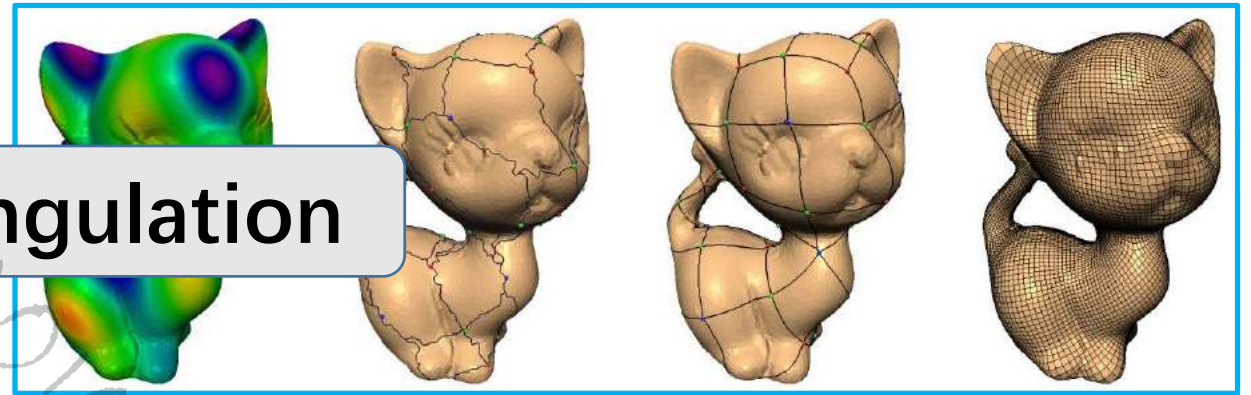
Local control
Hard to get pure quad-mesh

Differential geometry methods



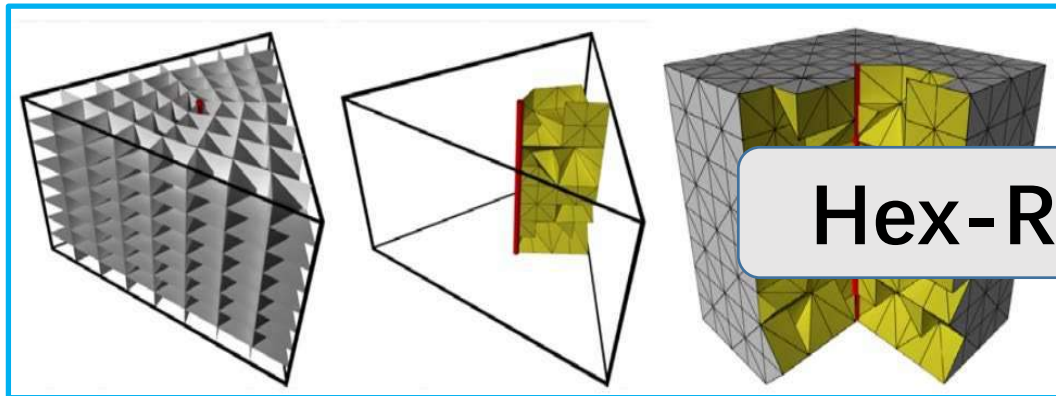
[Bommes et al. TOG 2012]

Surface parametrization



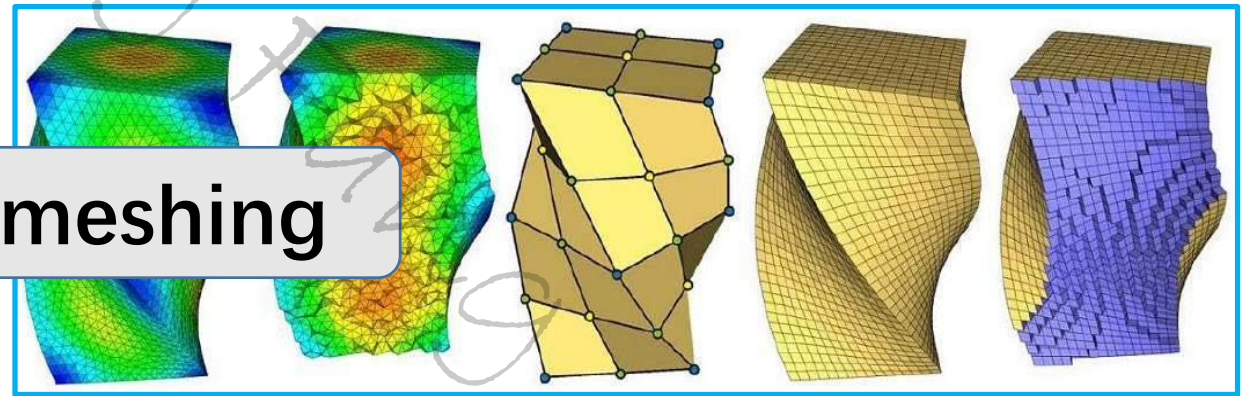
[Dong et al. TOG 2006]

2D Morse-Smale complex



[Nieser et al. CGF 2011]

Volume parametrization



[Ling et al. TOG 2014]

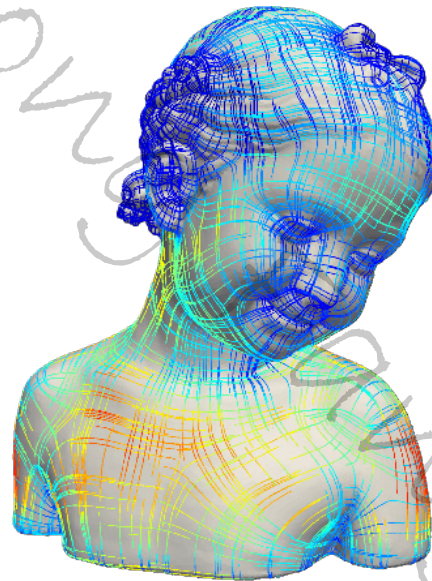
3D Morse-Smale complex

Hex-Remeshing

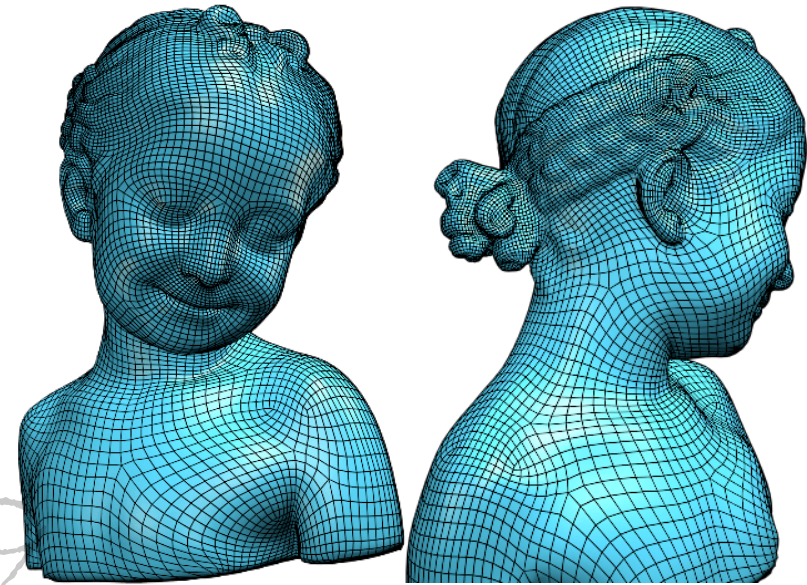
Frame field-driven quad- and hex-remeshing

Frame Field-Driven Remeshing

- Advantages
 - Feature & boundary alignment
 - Global topology control
 - Size & direction control

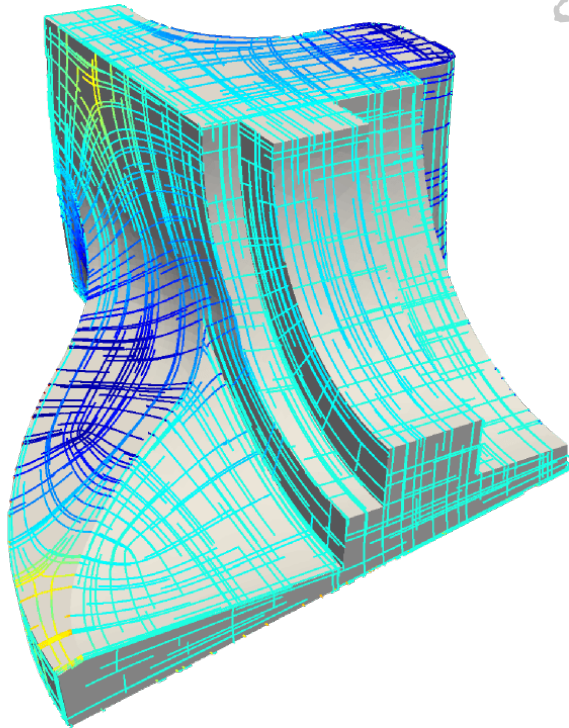


2D frame field

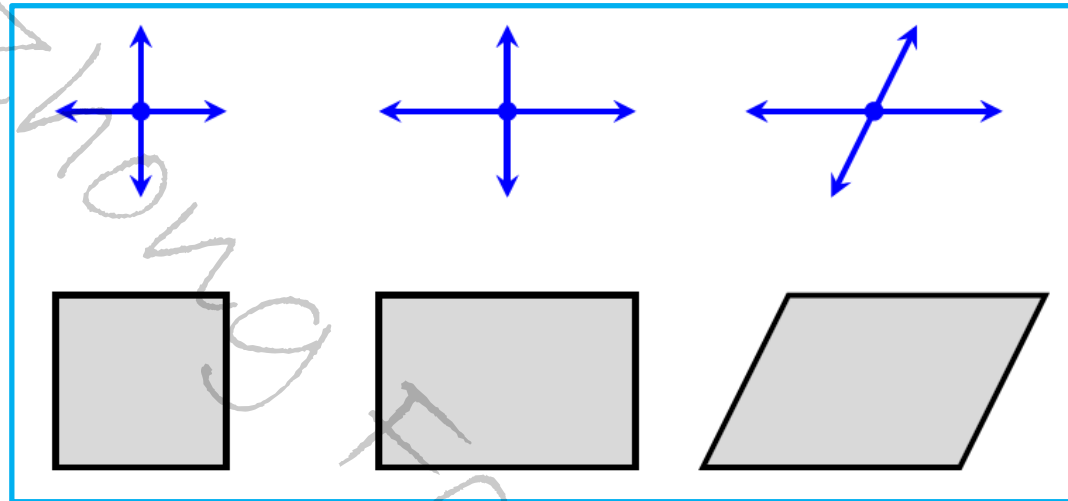


Quad-mesh

2D Frame Field

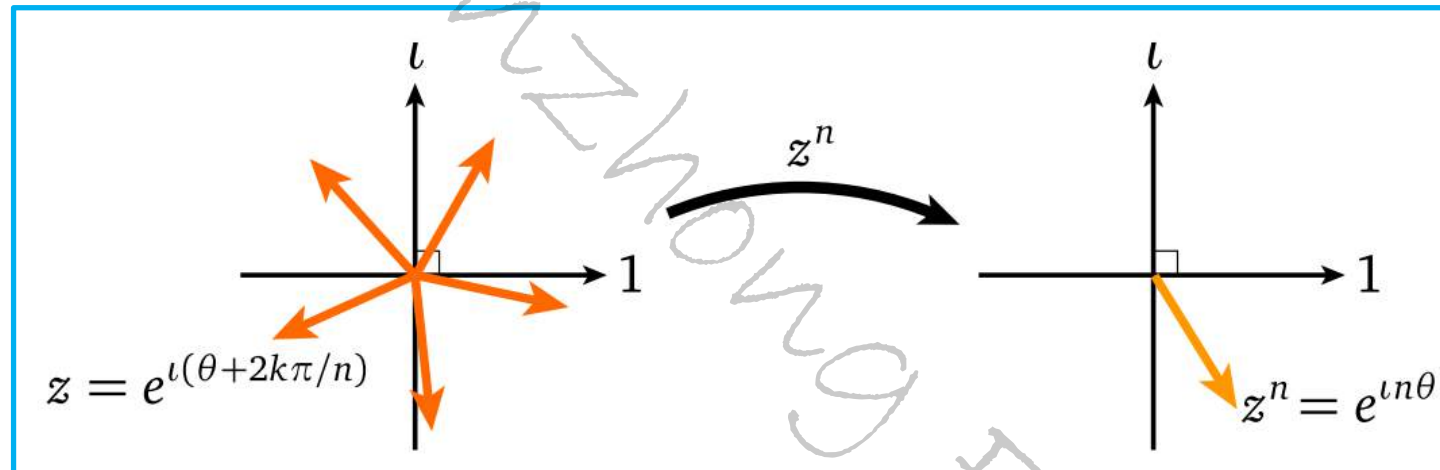


Frame field on surface



Symmetric Representation

- N-Rotational Symmetric field



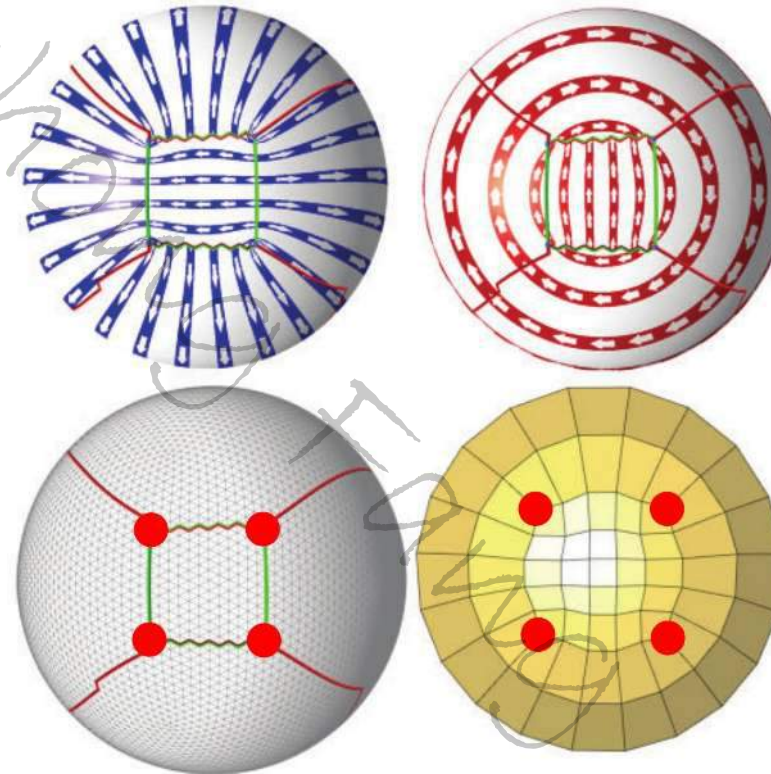
[Knöppel et al. '13]

- 4-Rotational Symmetric field (2D cross frame field)

$$(\cos(\theta + \frac{\pi}{2}k), \sin(\theta + \frac{\pi}{2}k)) \Leftrightarrow (\cos 4\theta, \sin 4\theta)$$

Frame Field and Quad Mesh

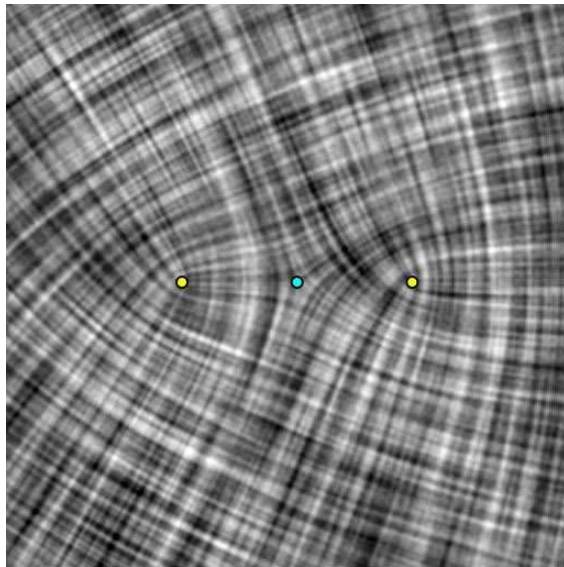
- Two directions for quadrangulation
- Smooth change
- Align to features
- With size control



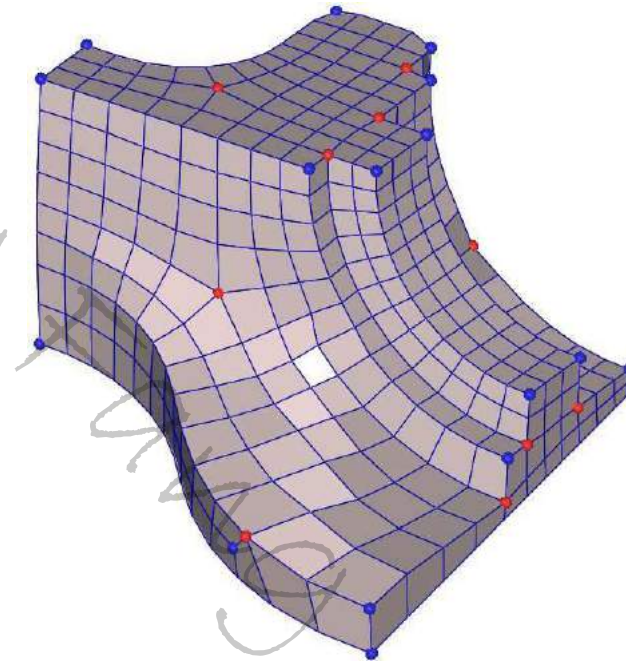
[Tong SGP 2006]

Singularity

- Non-smooth places of frame field
- Non-regular valence in quad mesh

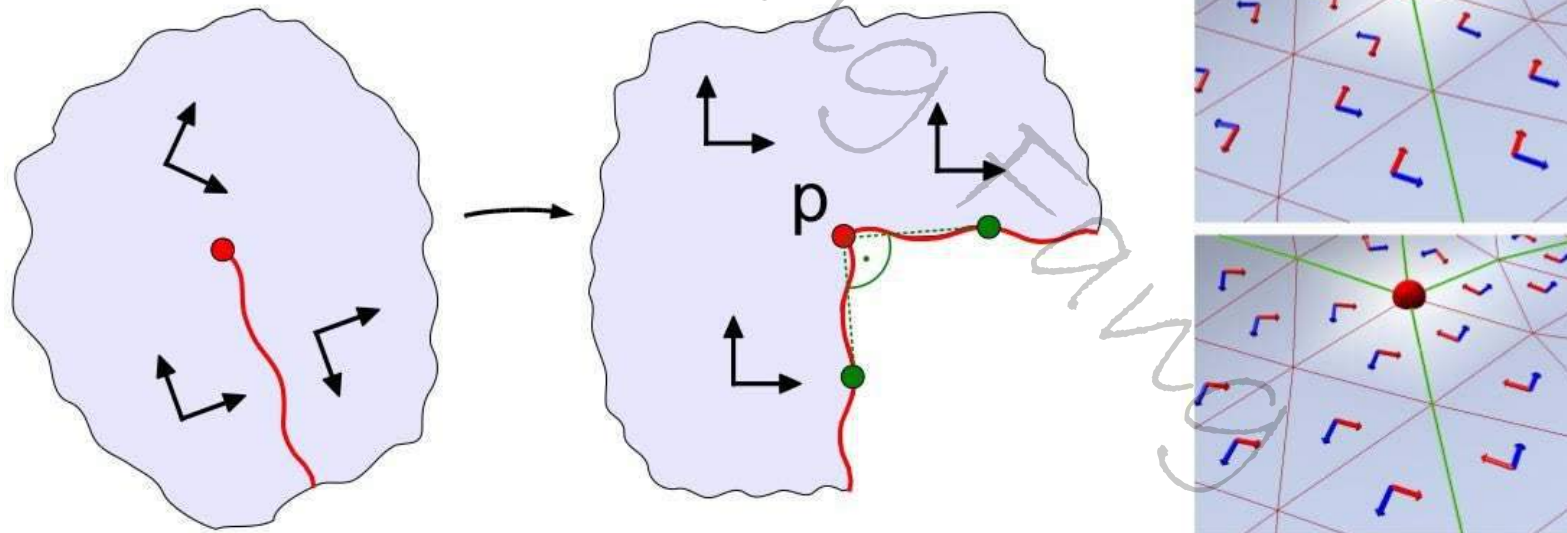


[Palacios et al. TOG '07]



Frame Field-Driven Parametrization

- Given frame field on surface
- Locate the singularities, and make cuts
- A single chart with aligned frames
 - But with transitions along the cuts

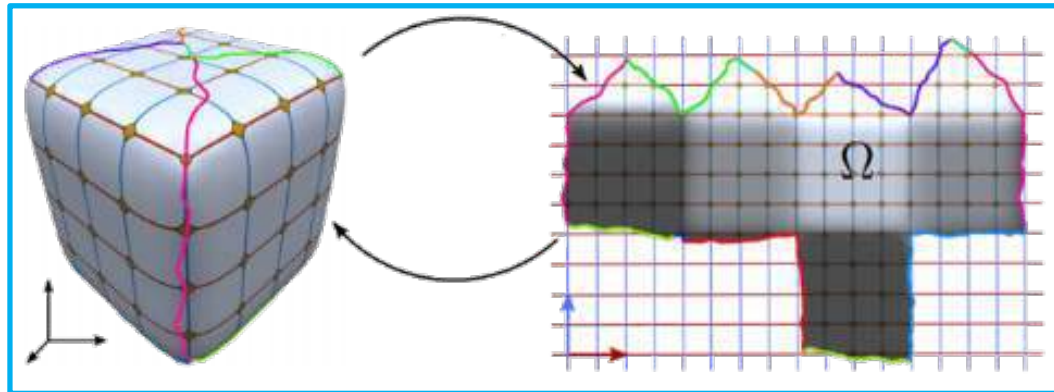


Frame Field-Driven Parametrization

- Frame field V drives parameterization φ

$$\varphi: S \rightarrow \begin{pmatrix} u \\ v \end{pmatrix} \in \mathbb{R}^2$$

Poisson reconstruction $\min_{\varphi} \int_S \|\nabla \varphi - V\|^2$



[Bommes et al. TOG 2013]

Decomposition $V = \nabla \varphi + \nabla \times \psi$

Integrable (Curl-free)

Parametrization-based Quadrangulation

$$\min_{\varphi} \int_S \|\nabla \varphi - V\|^2$$

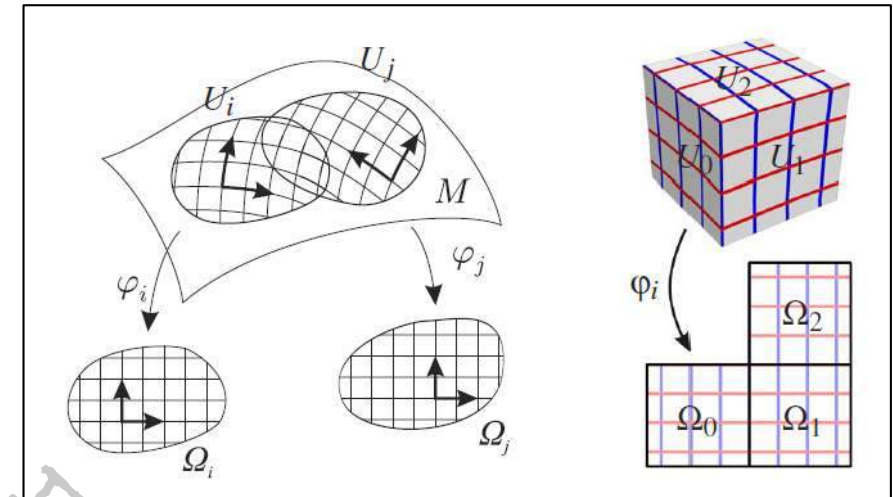
Seamless & non-degenerated

$$s.t. \quad \varphi_j(p) = R^{k_{ij}\frac{\pi}{2}} \varphi_i(p) + T_{ij}$$

$$\det(\nabla \varphi) > 0$$

Integer constraints

$$k_{ij} \in \mathbb{Z}, T_{ij} \in \mathbb{Z}^2$$



[Kälbere et al. '07]

Multi-chart parametrization

Parametrization-based Quadrangulation

$$\min_{\varphi} \int_S \|\nabla \varphi - V\|^2$$

Boundary condition

Seamless & non-degenerated

$$s.t. \quad \varphi_j(p) = R^{k_{ij}\frac{\pi}{2}} \varphi_i(p) + T_{ij}$$

$$\det(\nabla \varphi) > 0$$

Integer constraints

$$k_{ij} \in \mathbb{Z}, T_{ij} \in \mathbb{Z}^2$$



unconstrained



seamless $r = R_{k\pi/2}$
 t unconstrained



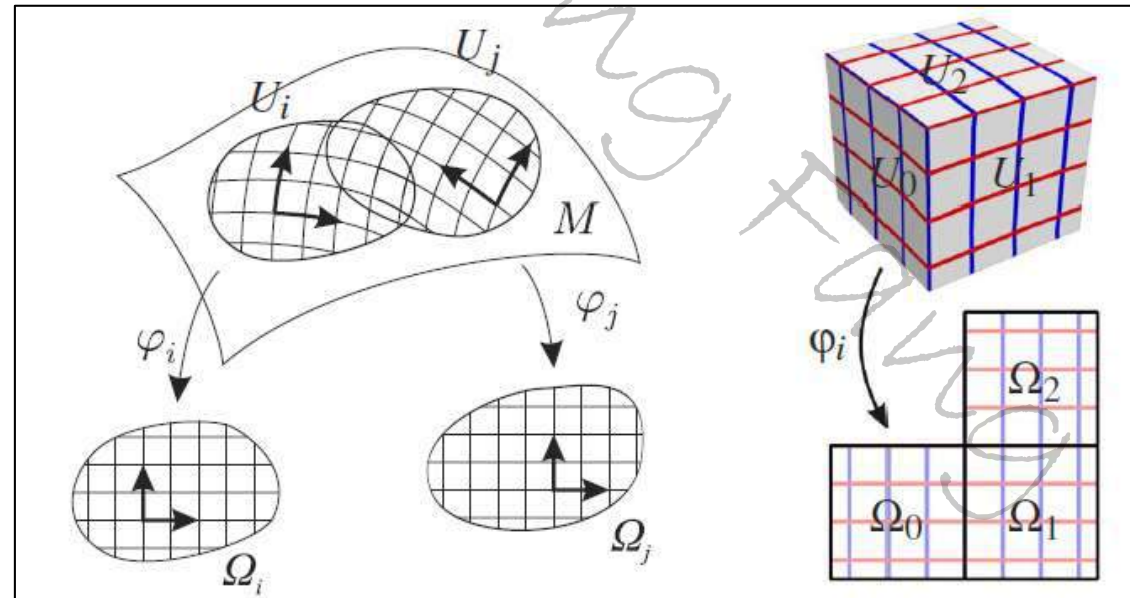
quadrangulation

$r = R_{k\pi/2}$
 t integer

[Myles and Zorin '13]

Parametrization-based Quadrangulation

- Given the parametrization of the input
- ***Extract Integer points***
- ***Re-map integer points onto the input surface***
- ***These integer points construct the quad mesh***



[Kälberer et al. '07]



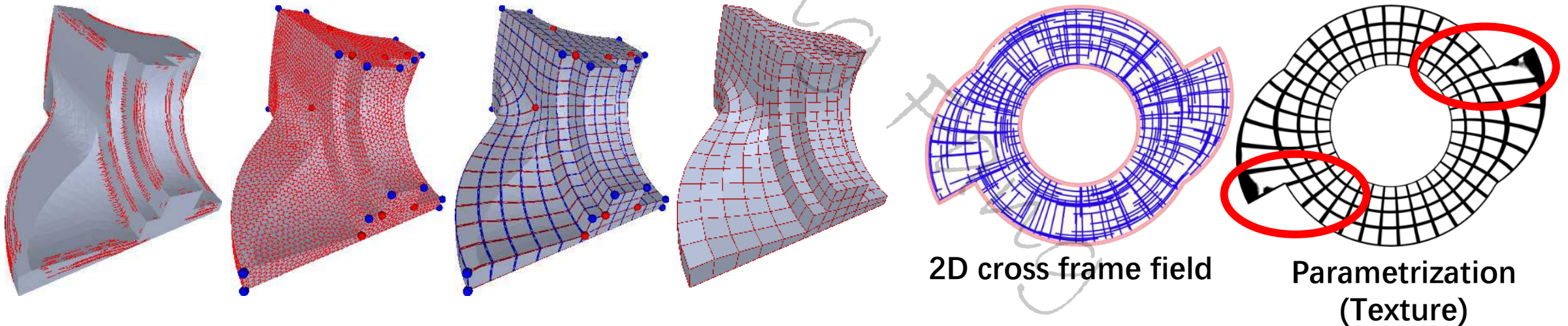
Invalid Parameterization

- The solution may even not exist!
 - Feasible region is a null set.
- **Conflict** among
 - Boundary & feature alignment
 - Non-degenerated
 - Transition at cut

Related works:

Parametrization-based Quadrangulation

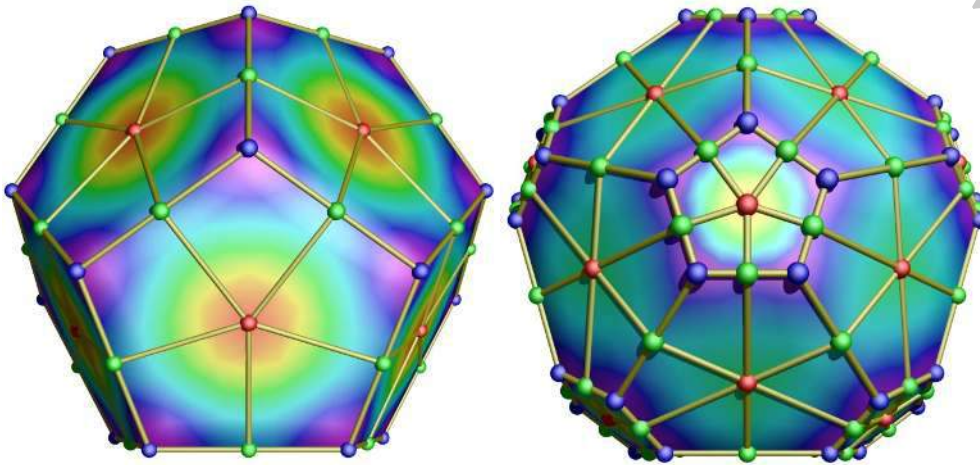
- QuadCover: using branched coverings [Kälberer et al. '07] *No guarantee*
- Mixed-Integer Quadrangulation [Bommes et al. '09]
- Integer-Grid Maps for Reliable Quad Meshing [Bommes et al. '13]
-



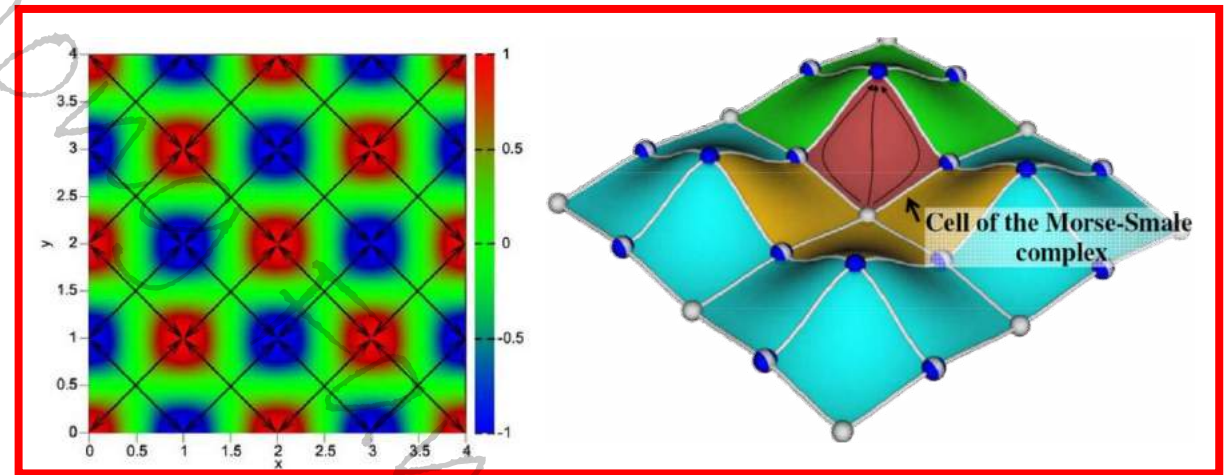
Related works:

MSC-based quadrangulation

- Morse function and Morse-Smale complex (MSC)



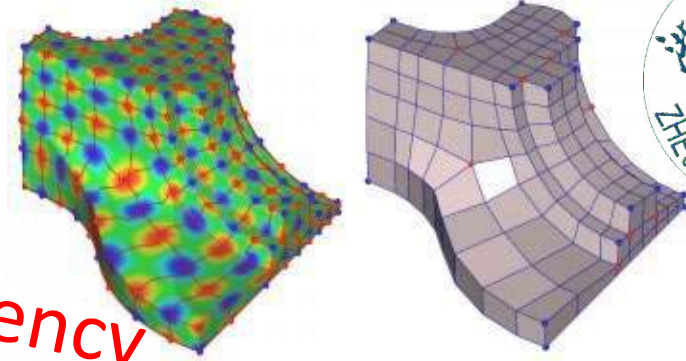
[Dong et al. TOG 2006]



Related works: (MSC-based methods)

- Spectral surface quadrangulation [Dong et al. '06]
 - (Dual) Morse-Smale complex to guarantee quads [Edelsbrunner et al. '03]
 - Orientation, alignment & size control [Huang et al. '08, Ling et al. '14]
- Wave-based anisotropic quadrangulation [Zhang et al. '10]
-

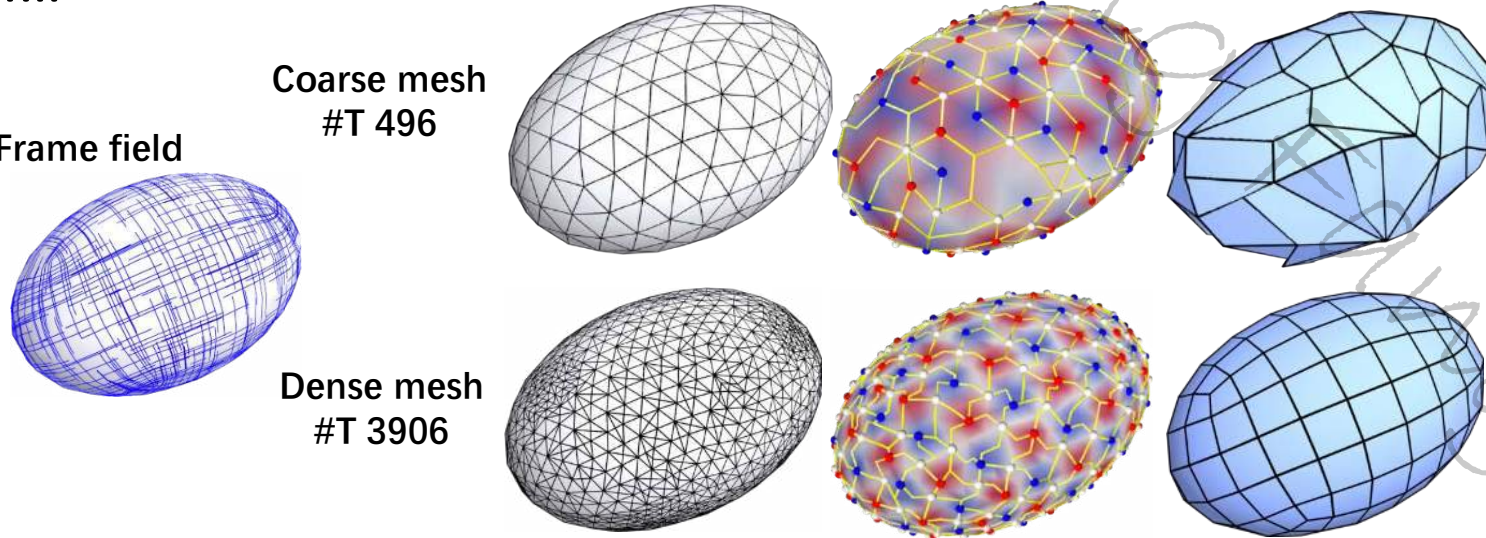
Low efficiency



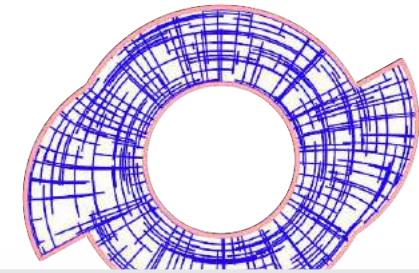
Frame field

Coarse mesh
#T 496

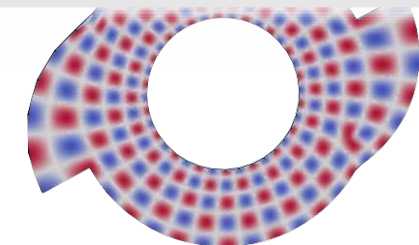
Dense mesh
#T 3906



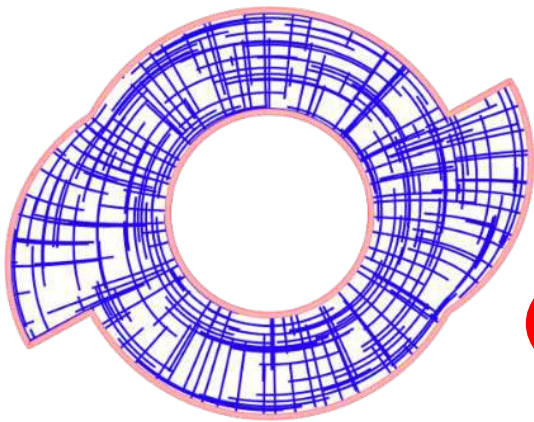
Frame field-driven quad- and hex-remeshing



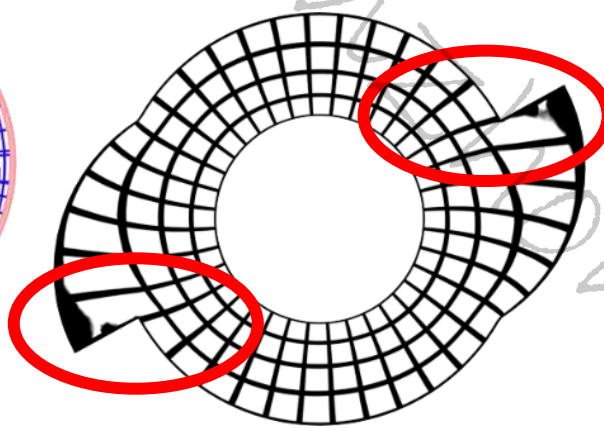
Guarantee



Topological conflicts

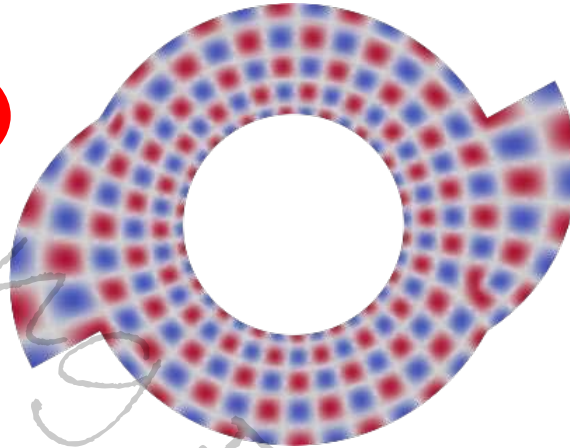


Cross frame field

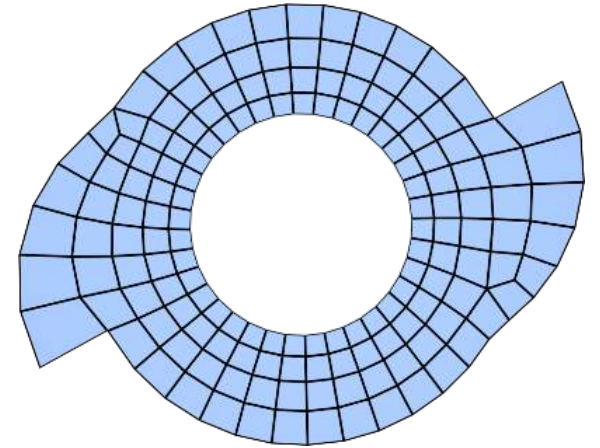


Degenerated
Parametrization

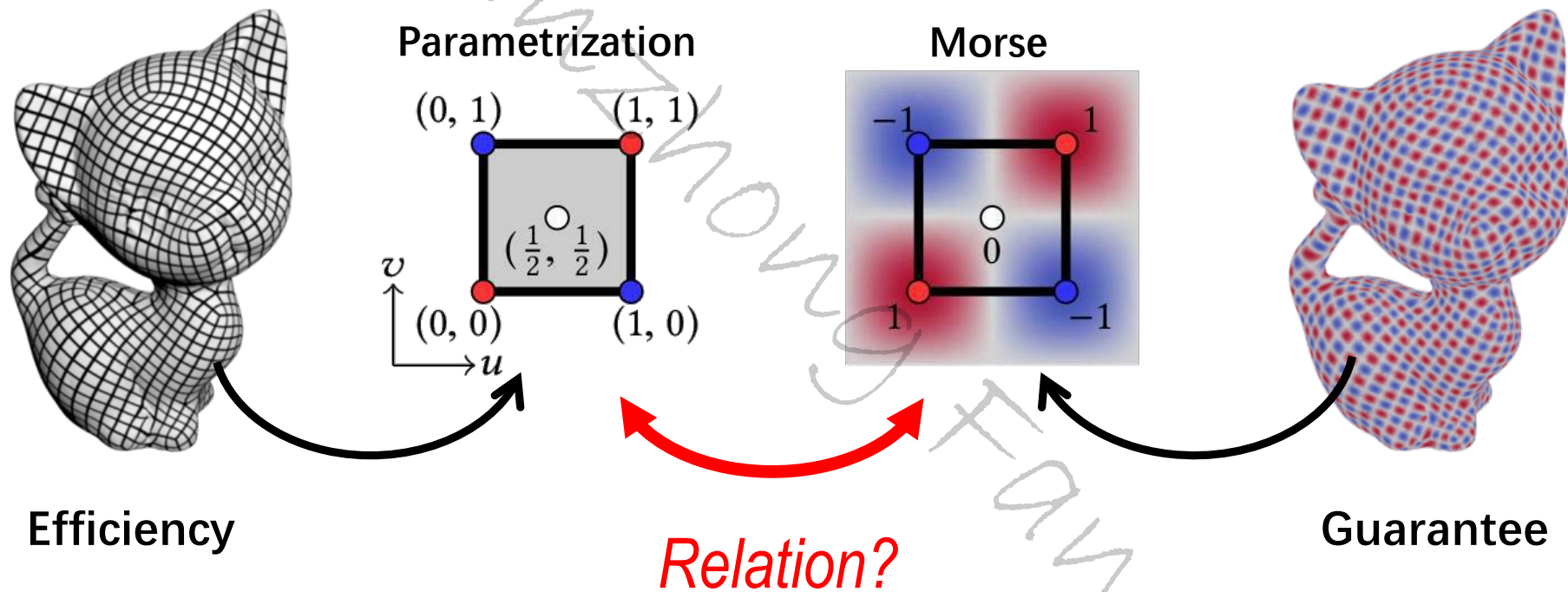
Holonomy condition



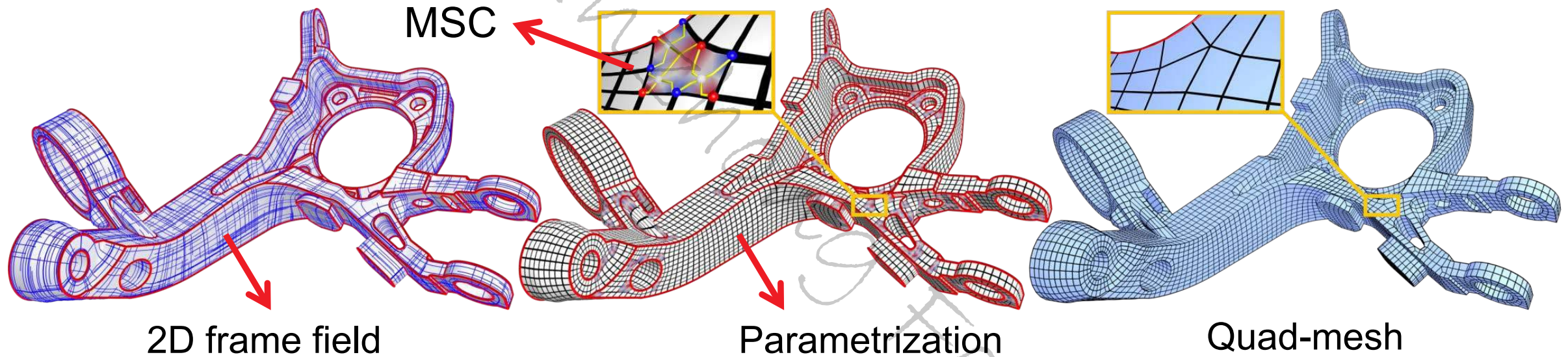
MSC: guarantee, but low efficiency.
Need dense enough mesh as input



Parametrization & Morse function



Parametrization & MSC -- Quadrangulation



[Fang et al. TOG '18]

MSC automatically inserts singularities.
Resolve topological conflicts.

Periodic vector field Ψ :

From Morse function to parametrization

$$\Psi = \psi \circ \varphi \quad \text{with}$$

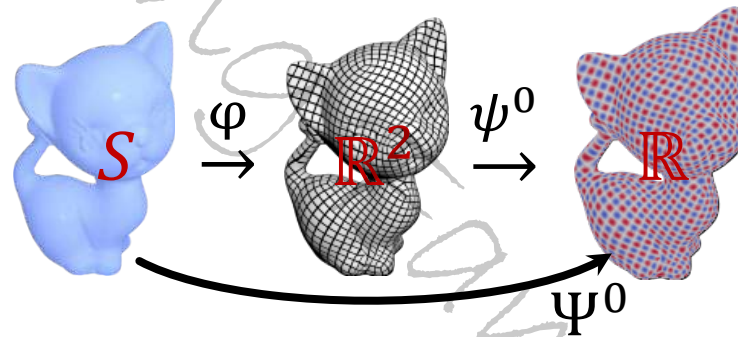
Morse function

$$\psi(u, v) = (cc(u, v), sc(u, v), cs(u, v), ss(u, v))^T$$



$$\varphi = \psi^{-1} + (T_1, T_2)^T \quad T_1 \pm T_2 \in 2\mathbb{Z}$$

$$\begin{cases} cc(u, v) = \cos(\pi u) \cos(\pi v) \\ sc(u, v) = \sin(\pi u) \cos(\pi v) \\ cs(u, v) = \cos(\pi u) \sin(\pi v) \\ ss(u, v) = \sin(\pi u) \sin(\pi v) \end{cases}$$



Conditions

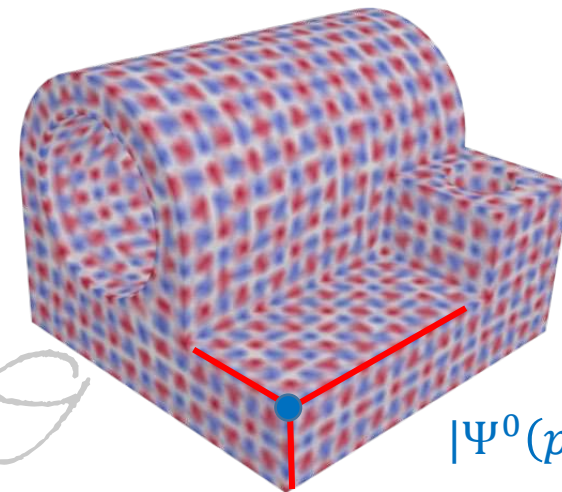
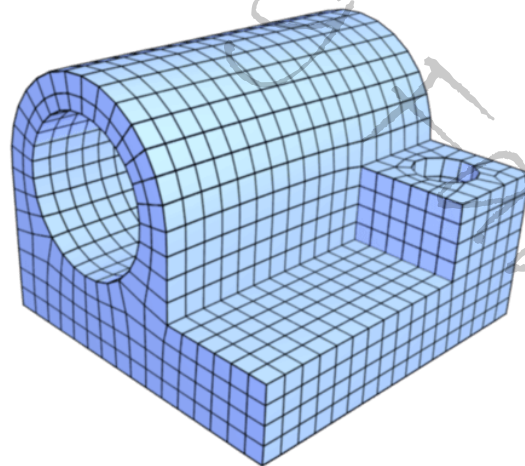
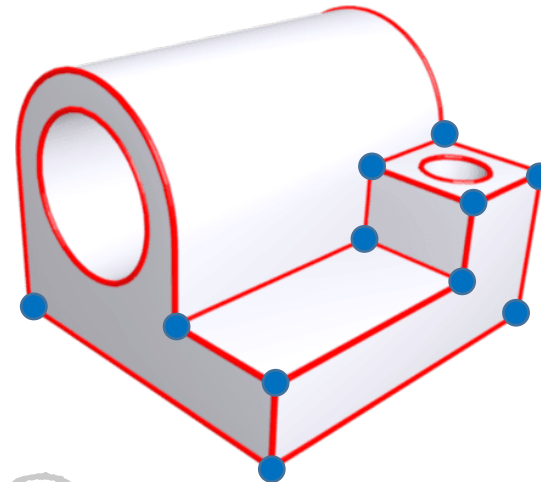
$$\begin{aligned} \|\Psi\|_2 &= 1 \\ \Psi^0 \Psi^3 &= \Psi^1 \Psi^2 \\ \hat{\nabla}_v \Psi &= \frac{\partial \Psi}{\partial p} - \pi W(F^{-1}v)\Psi \end{aligned}$$

Idea: 1) Compute a good Ψ
 2) Reconstruct φ where it's easy
 3) Revert to Morse if needed

Compatible

Boundary & feature alignment

- Vertices on boundary & feature
 - u or $v \in \mathbb{Z} \dots$
 - $\Psi^3(p) = ss(u(p), v(p)) = 0$
- Corners
 - u and $v \in \mathbb{Z} \dots$
 - $\Psi^1(p) = \Psi^2(p) = \Psi^3(p) = 0$



$$\Psi^3(p) = 0$$

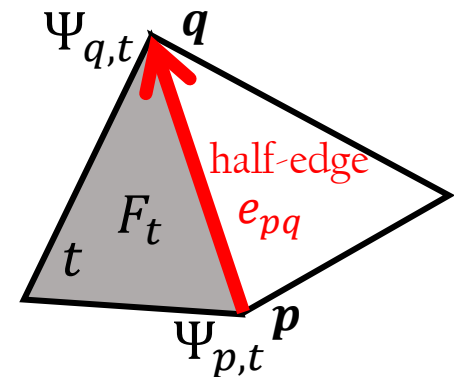
$$|\Psi^0(p)| = 1$$

Periodic 4D Vector Field Optimization

- Frame field driven periodic vector field generation

$$\min_{\Psi} \int_S \|\hat{\nabla} \Psi\|^2 \quad s.t. \begin{cases} \|\Psi\|_2 = 1 \\ \Psi^0 \Psi^3 = \Psi^1 \Psi^2 \\ \text{corners \& features} \end{cases}$$

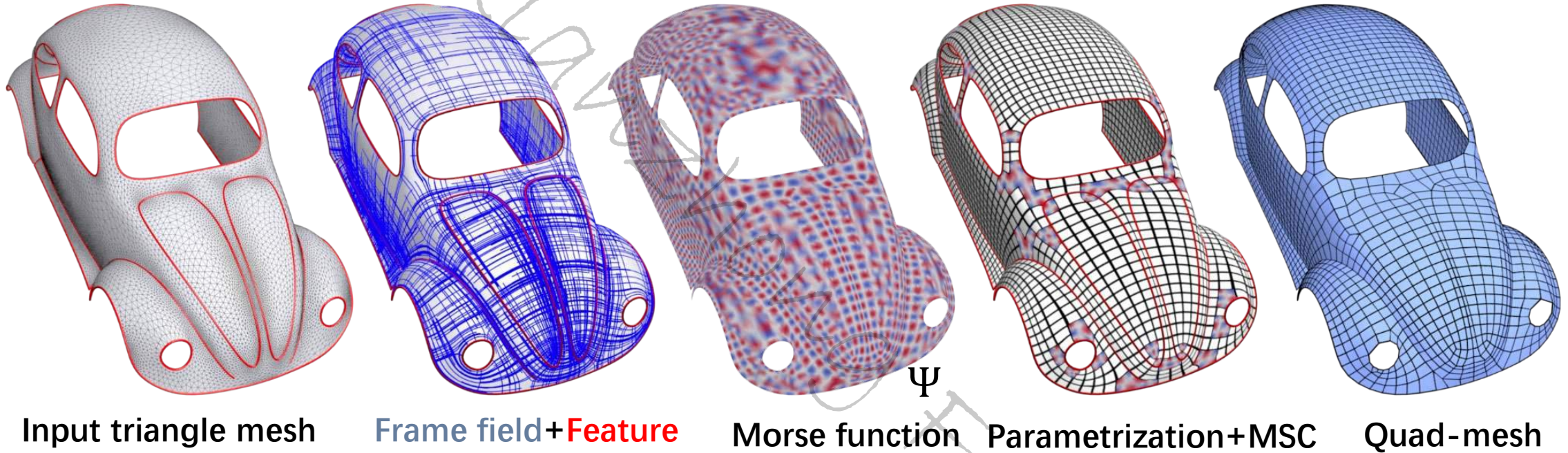
$$\mathcal{E}(\Psi) = \sum_{(p,q)} \mathcal{E}_{pq} \quad \text{with} \quad \mathcal{E}_{pq} = \frac{|t|}{2|e_{pq}|^2} \|\Psi_{q,t} - \exp(\pi W(F_t^{-1} e_{pq})) \Psi_{p,t}\|^2$$



- Constrained nonlinear optimization

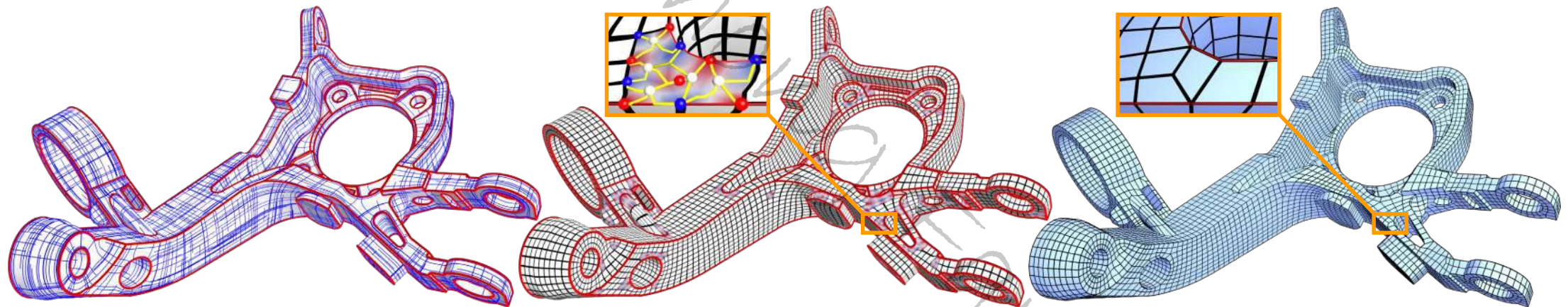
$$\min_{\Psi} \mathcal{E}(\Psi) \quad s.t. \begin{cases} \|\Psi_p\|^2 = 1, & p \in V \\ \Psi_p^0 \Psi_p^3 = \Psi_p^1 \Psi_p^2, & p \in V \\ \Psi_p^3 = 0, & p \in V_b \\ \Psi_p^1 = \Psi_p^2 = 0, & p \in V_c \end{cases}$$

Pipeline



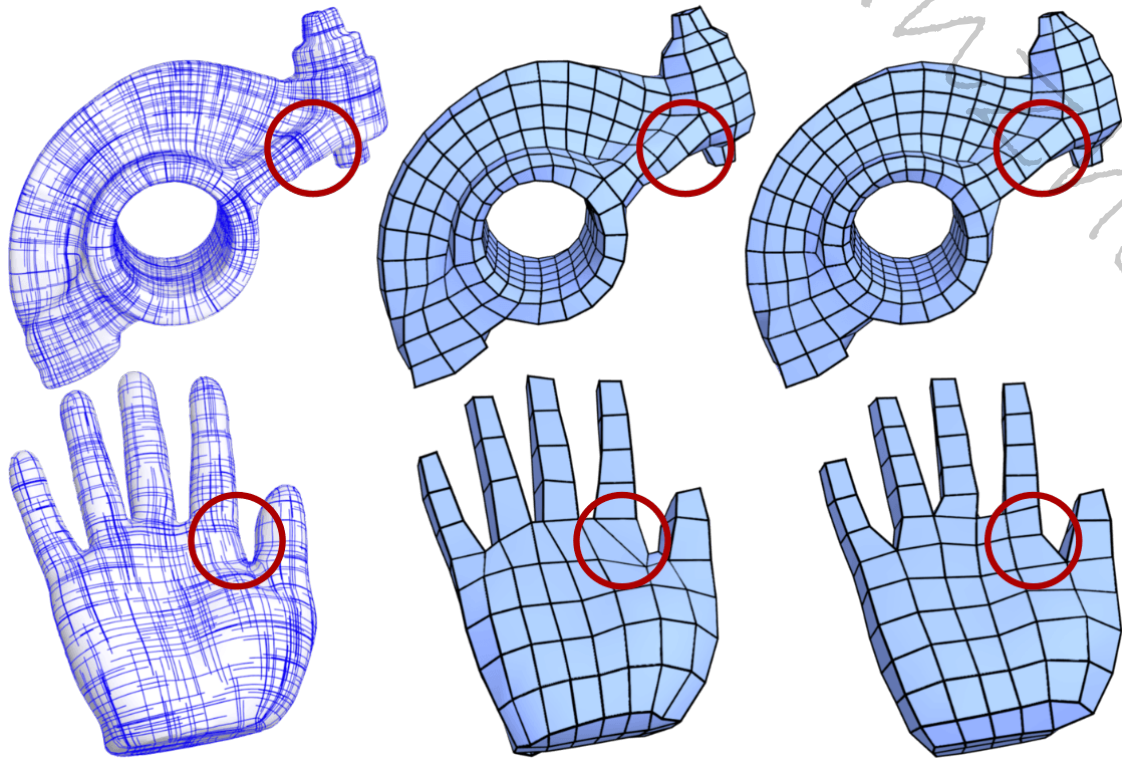
- **Extract quad-mesh from periodic vector function**
 - Construct global parametrization
 - Extract quads by two steps: **Regular region & Singular region**

Results



V.S. IGM

- Better frame alignment



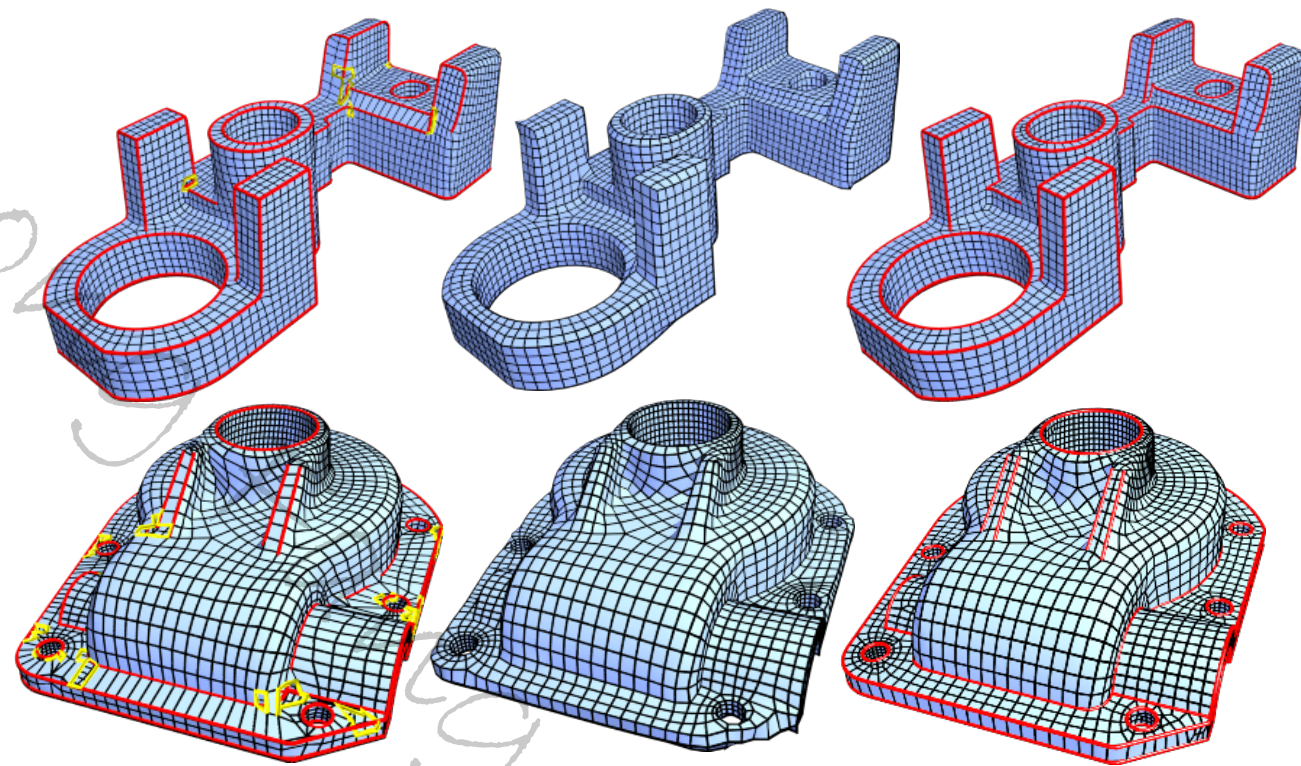
Frame field

IGM

Ours

V.S. MIQ

- Guarantee



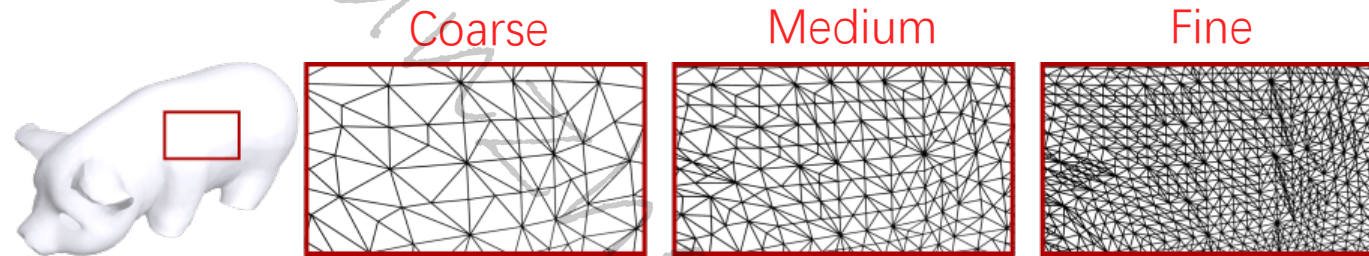
MIQ (Feature)

MIQ (No feature)

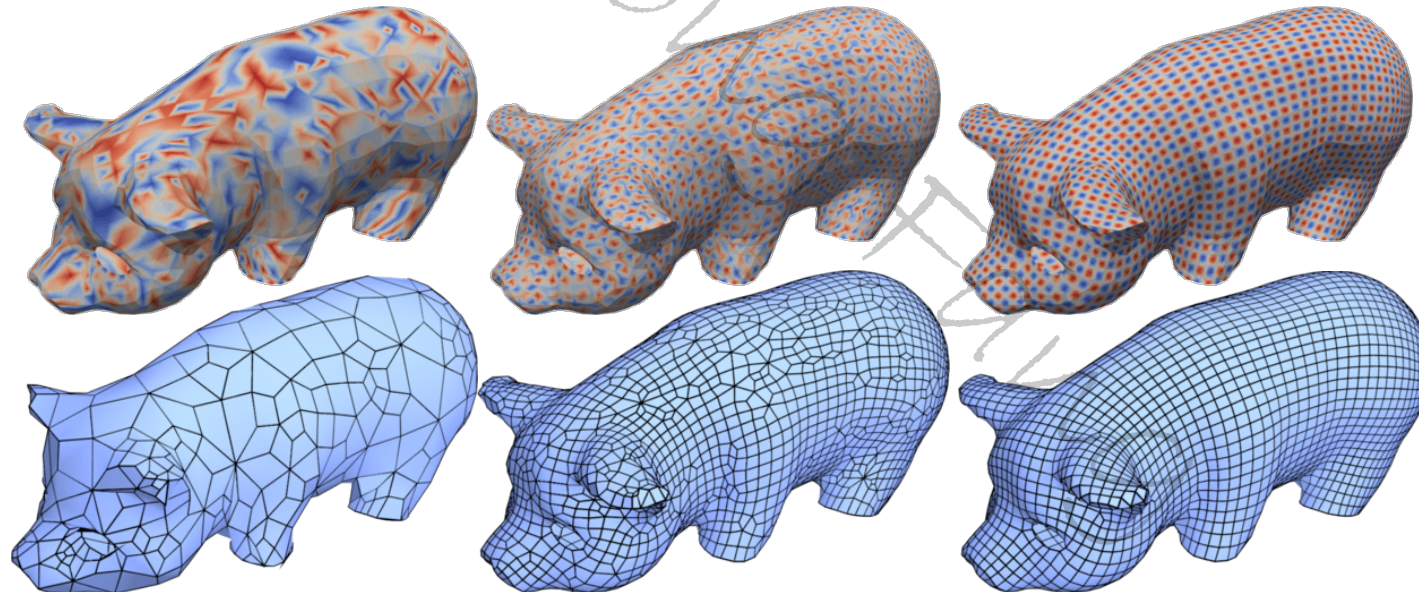
Ours (Feature)

V.S. Wave-based method

- More efficient

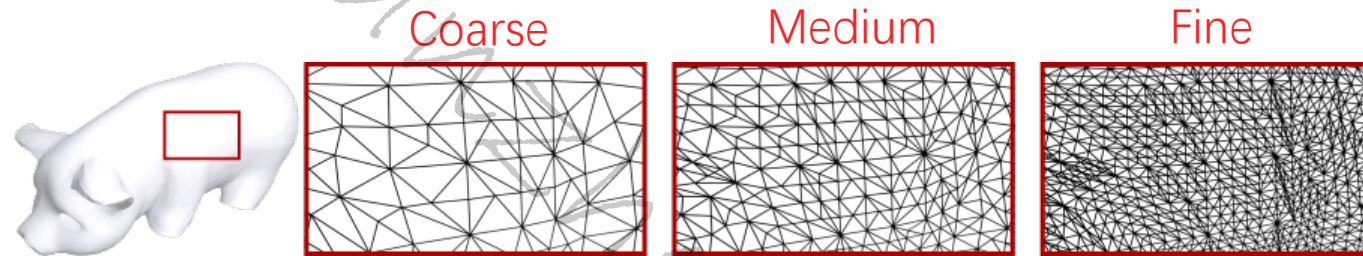


Wave-
based
method

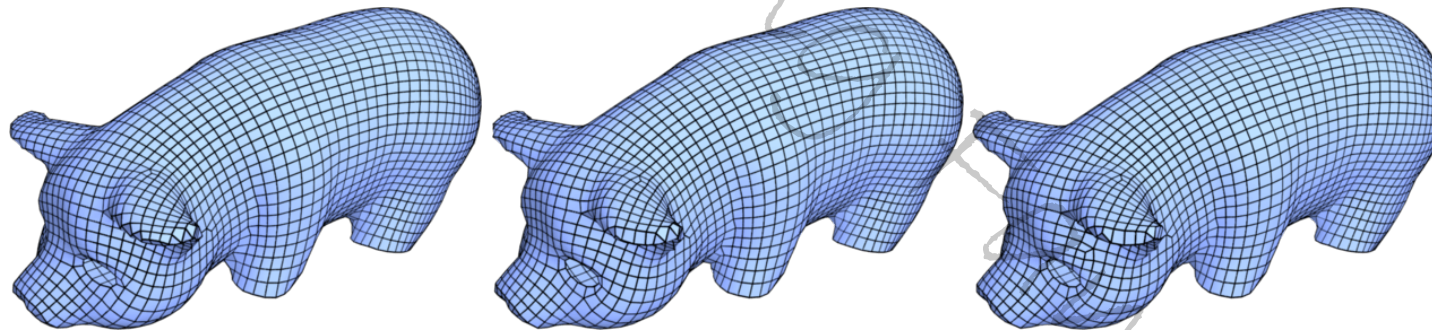


V.S. Wave-based method

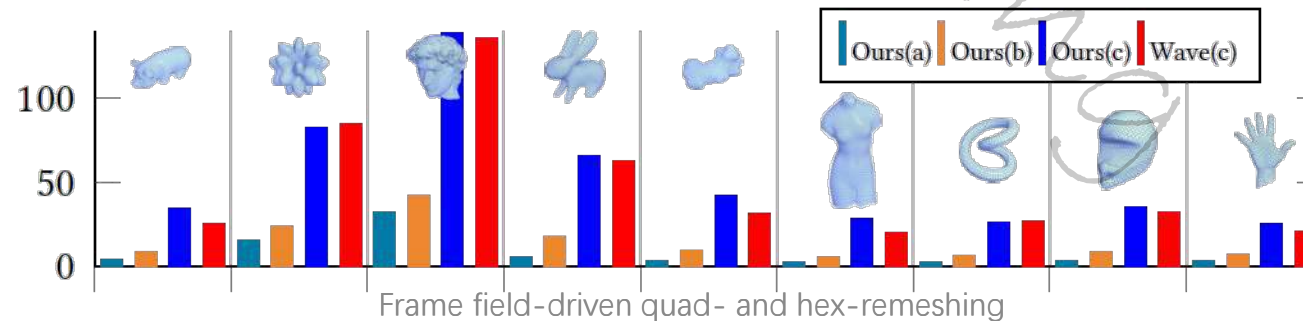
- More efficient



Ours

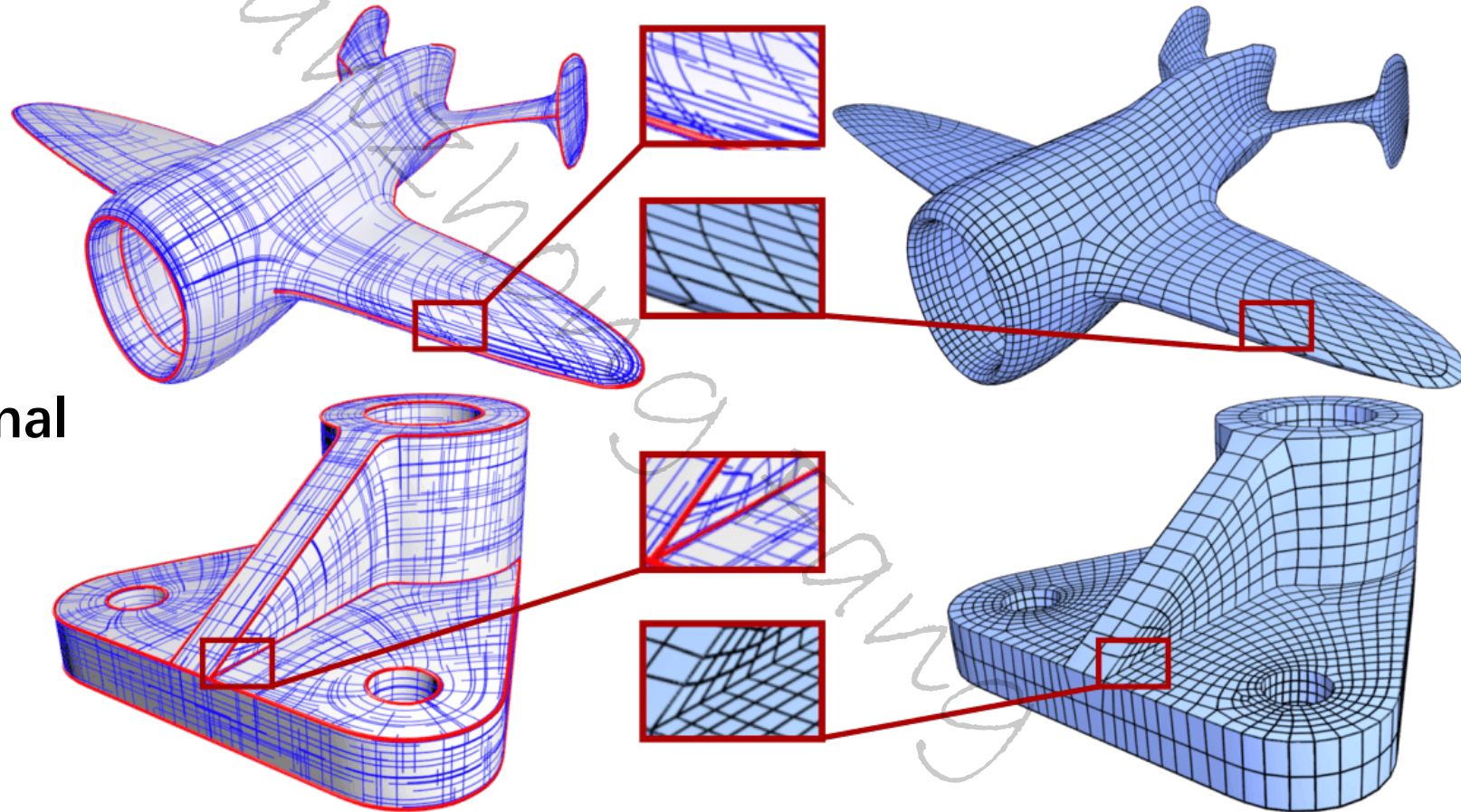


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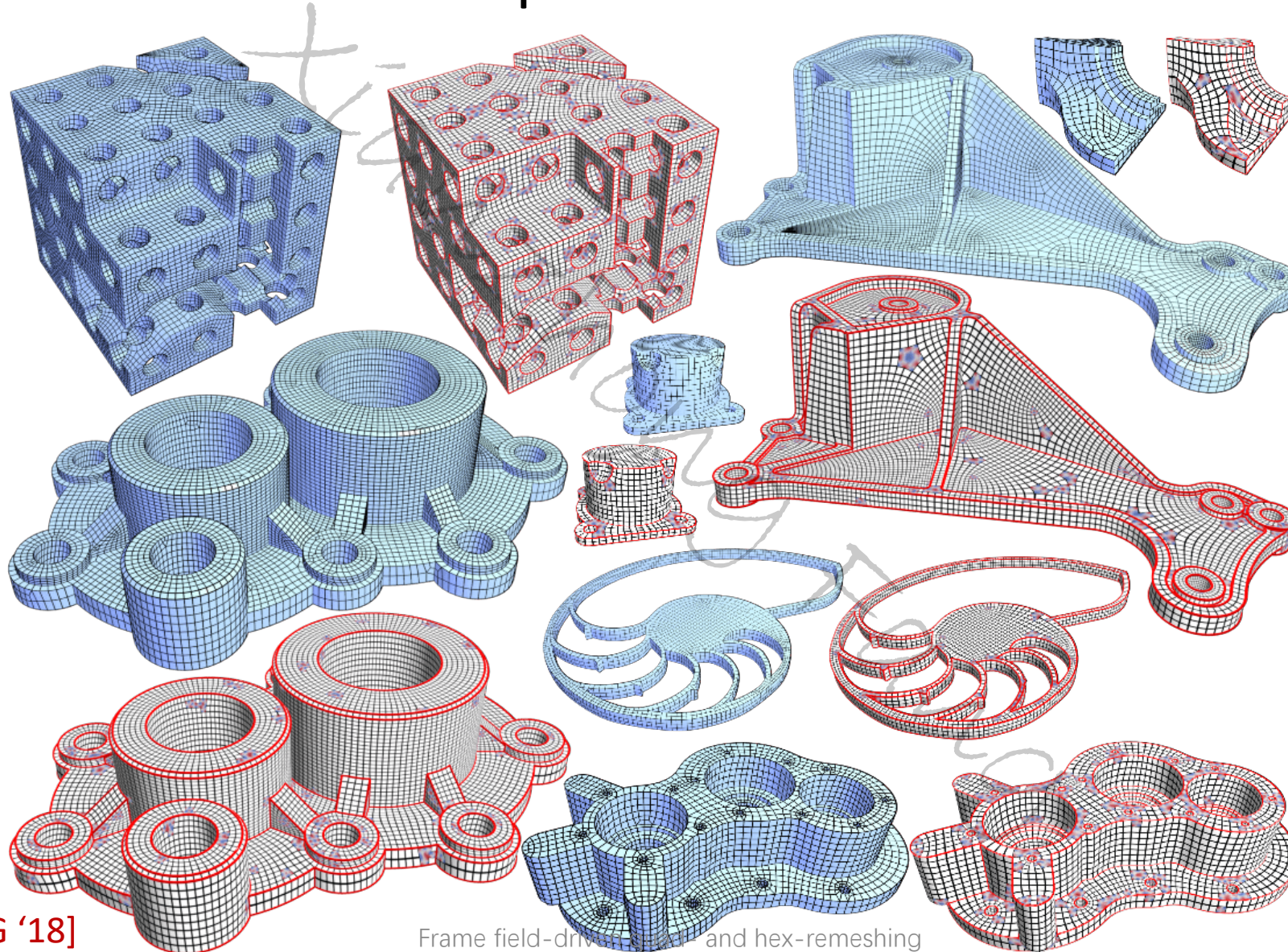


Frame Field Control

- Anisotropic
- Non-orthogonal



Results on models with complicated features



[Fang et al. TOG '18]

Frame field-driven meshing and hex-remeshing



Can these QUAD techs
extend to HEX ?



There are several big challenges!

- Algebra representation of 3D frame field: **Non-commutative**
- Global topology: **No Gauss-Bonnet theorem** in 3D
- **No conformal structure** in 3D

Can these quad techs extend to Hex?

Frame field driven
parametrization

*Hard to get
hex-meshable
frame field*

*Hard to control the inner
singularity structure*

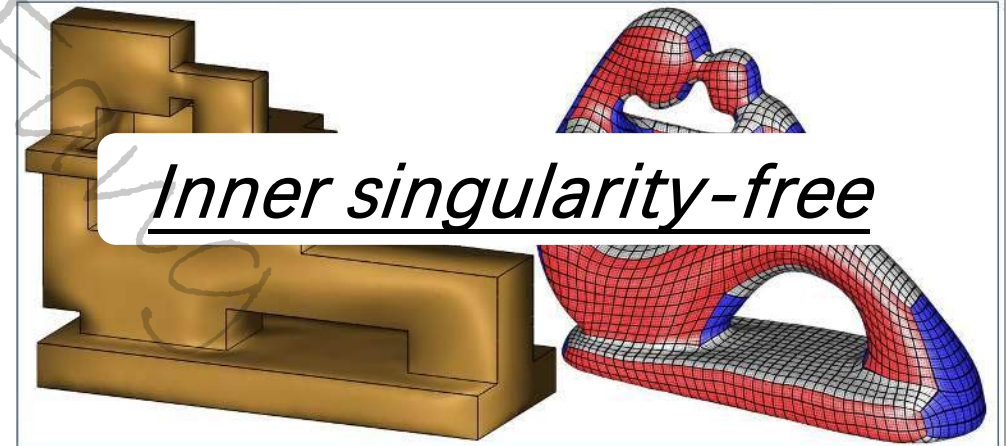
Hex-Remeshing

Polycube

3D Morse-Smale
complex

No guarantee

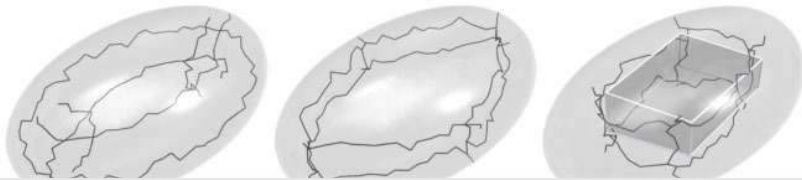
Inner singularity-free



Parametrization-based Hex-Remeshing

Frame field driven parametrization

Polycube



**Global topology constraint is
not clear.
Not robust.**



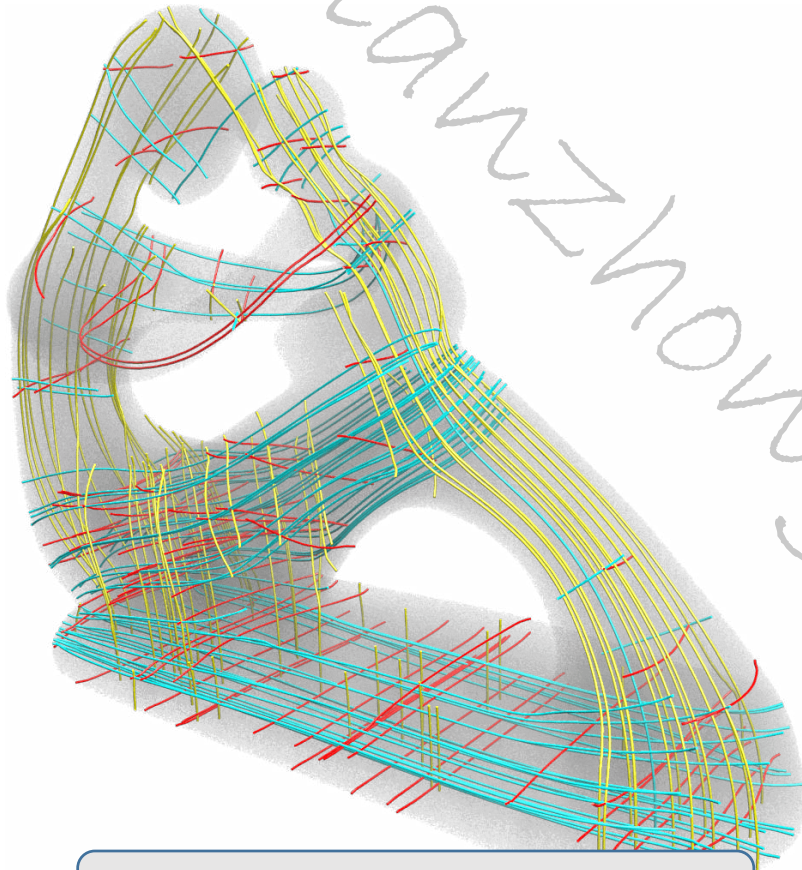
[Li et al. TOG '12]



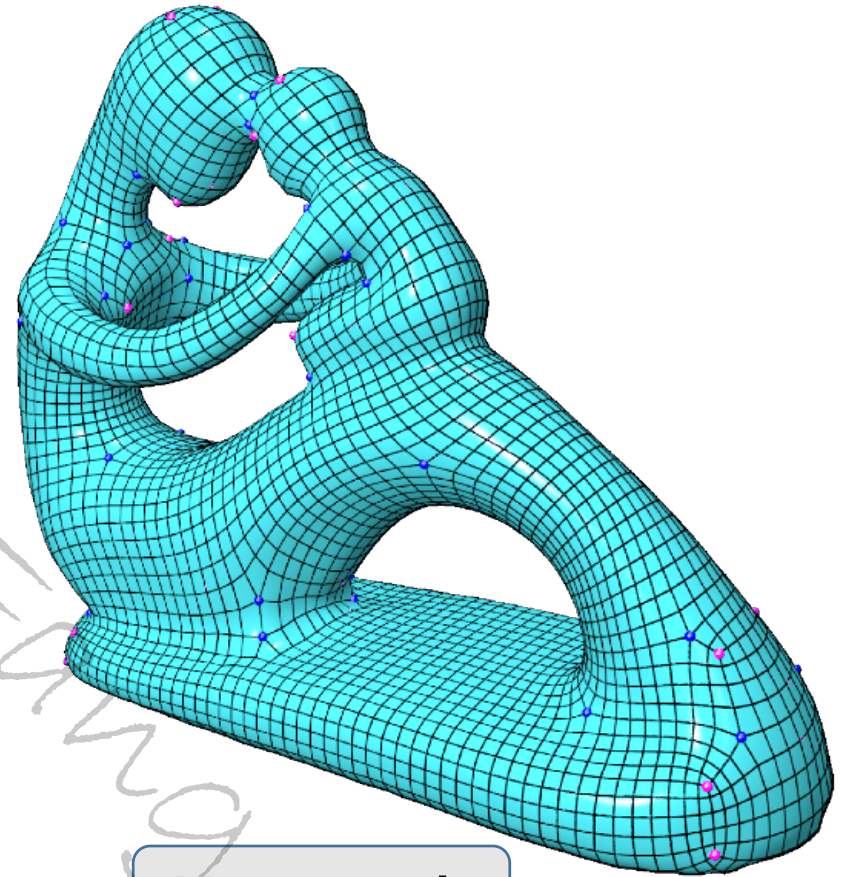
**Simple global topology structure.
Robust.
Bad element quality.**

[Livesu et al. TOG '13]

3D Frame Field



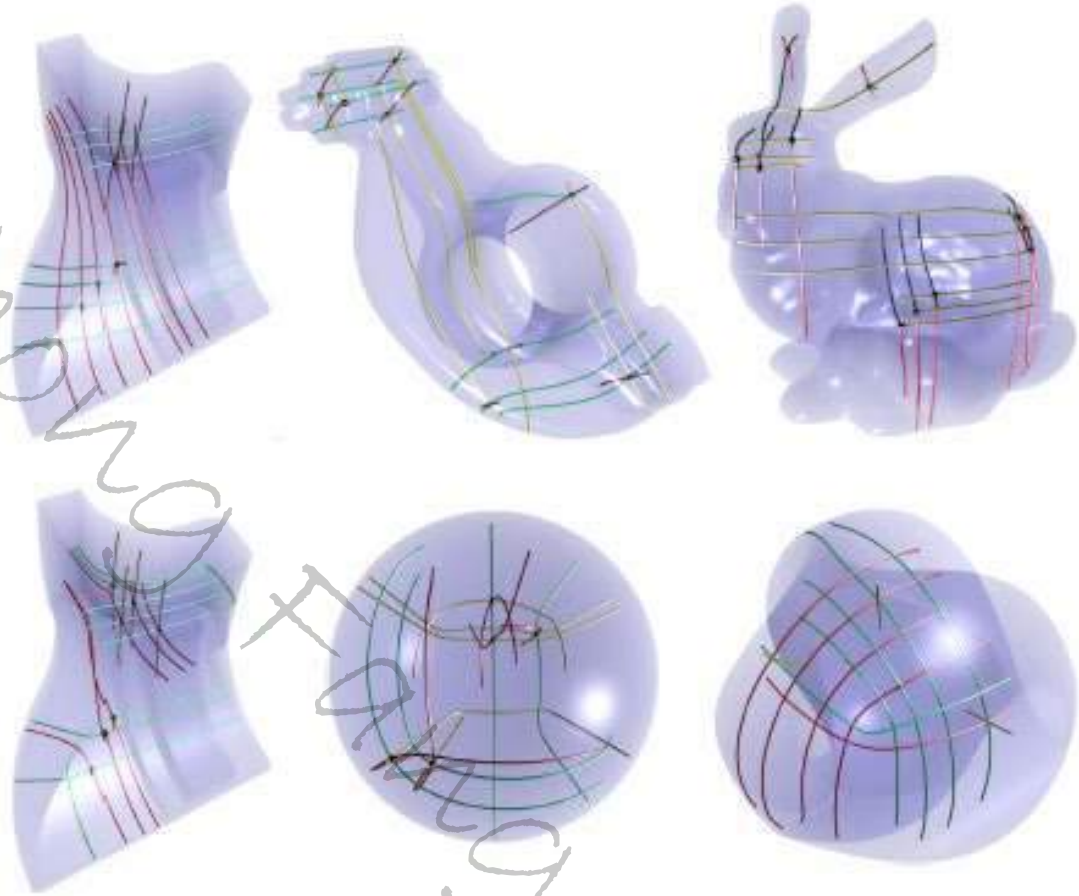
3D cross frame field



Hex-mesh

3D Frame Field Generation

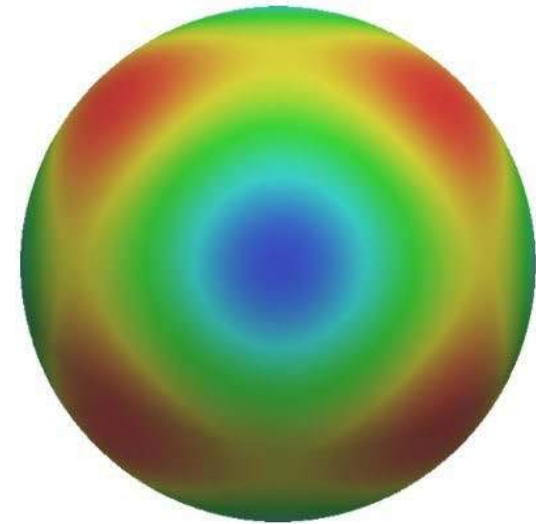
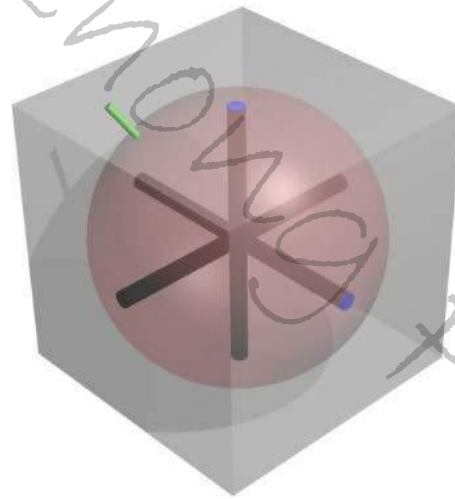
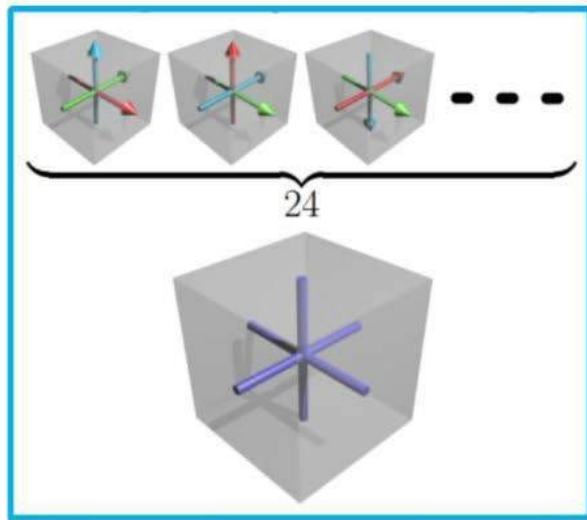
- Cubic symmetry
- Smoothness
- Boundary alignment



[Huang TOG 2011]

SH for Symmetric Field

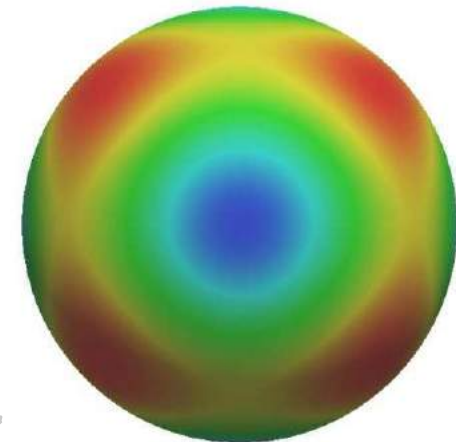
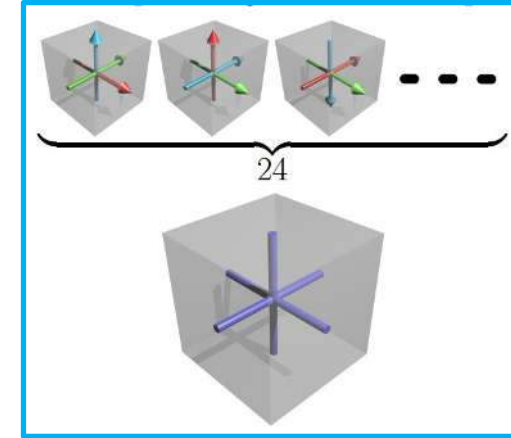
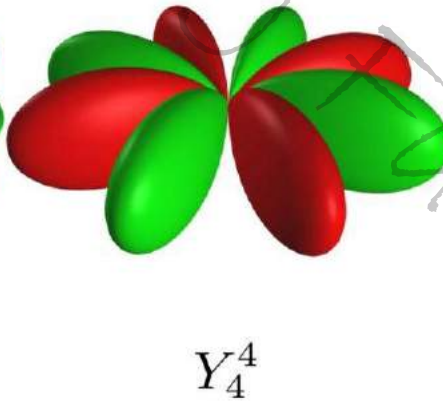
- Symmetric spherical function



SH for Symmetric Field

- Symmetric spherical function
- Vector space of spherical harmonics

$$f = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ \sqrt{7} \\ 0 \\ 0 \\ 0 \\ \sqrt{5} \end{pmatrix}$$

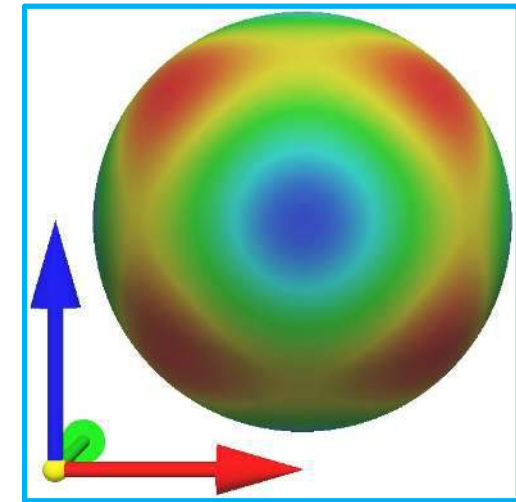


Advantages

- Simple math in a vector space
 - A single vector represents all 24 symmetries.
 - Smoothness is measured by Dirichlet energy of vectors

$$\int_{\Omega} \|\nabla f\|^2$$

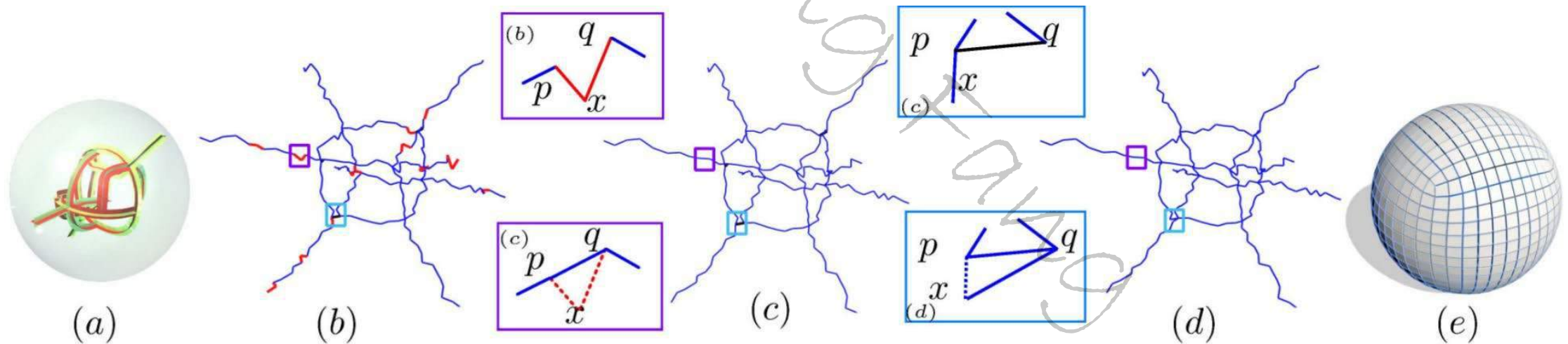
- Normal alignment is a linear constraint
 - If and only if $(R_{n \rightarrow z} f)[4] = \sqrt{7}$
- Linear initialization for non-linear optimization



Spherical harmonical function

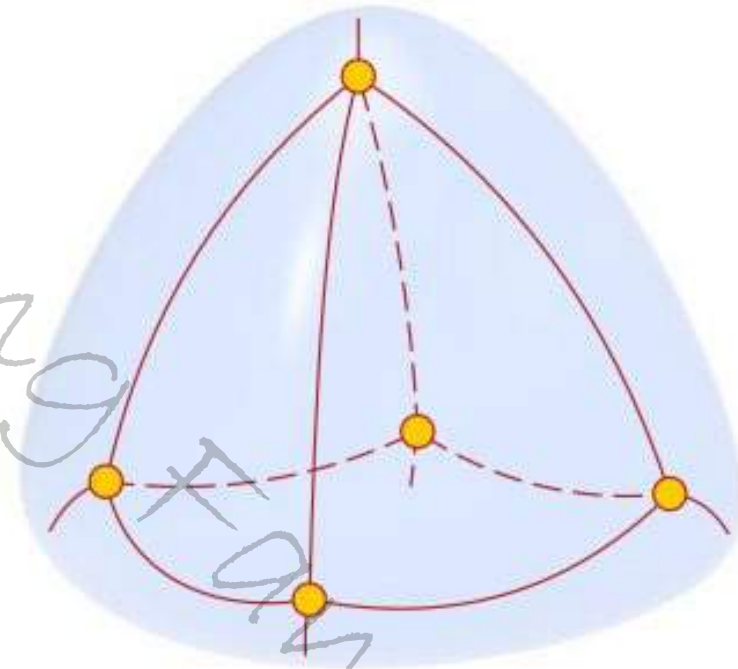
Topology Conflict

- Local conflict [Jiang TVCG 2014]
 - Defines all (inner & boundary) local conflicts
 - Detects all and fix all
 - All can be removed with proof



Topology Conflict

- BUT: there is global conflict!
 - No clear definition of it
 - Cannot be detected and fixed



[Li et al. TOG 2012]

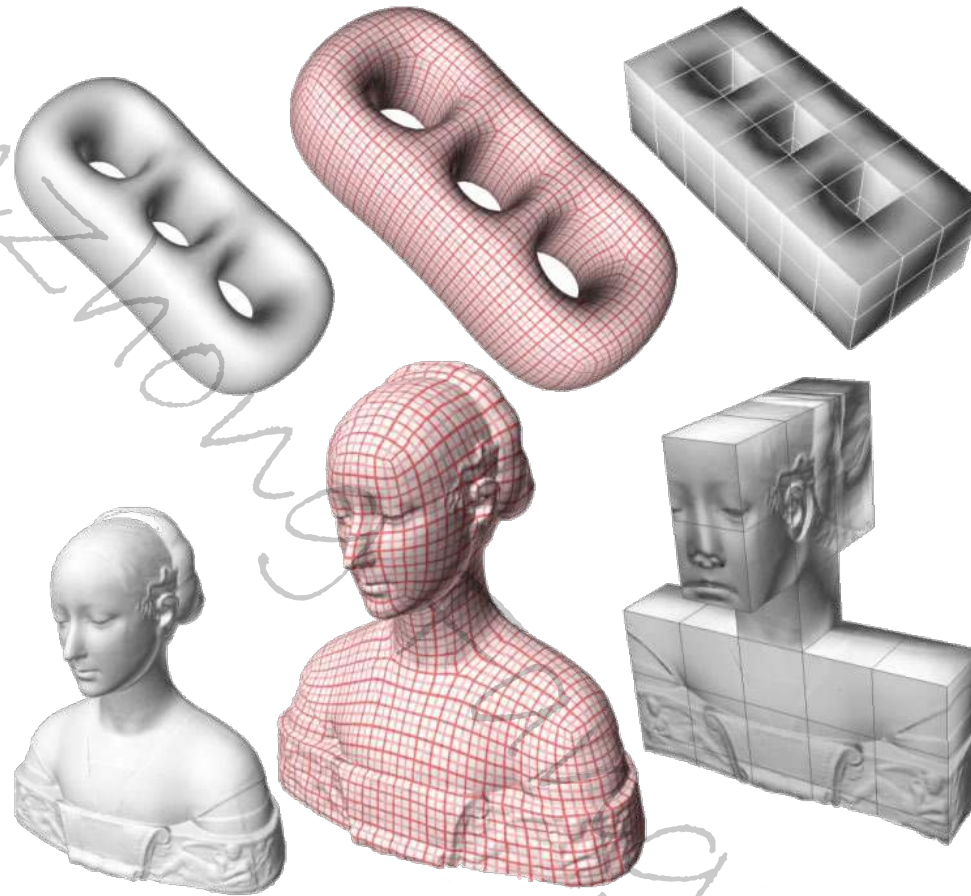


Frame Field-Driven Method

- High DOFs and quality if the feasible region is not empty
- But global conflict is hard to be resolved
 - Begin with ***simple and robust structure***
 - Gradually introducing more DOFs for better quality

Polycube-Based Method

No Inner Singularity

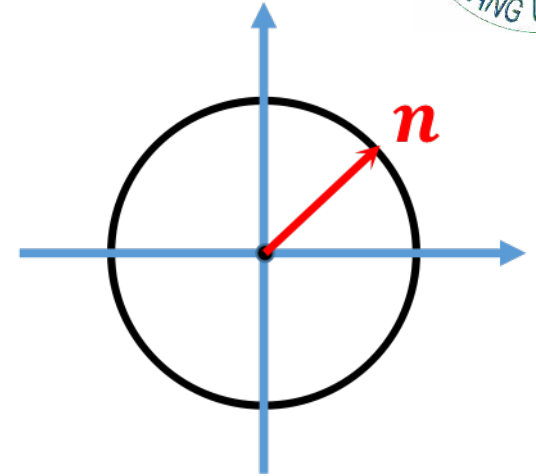


[Tarini et al. TOG '04]

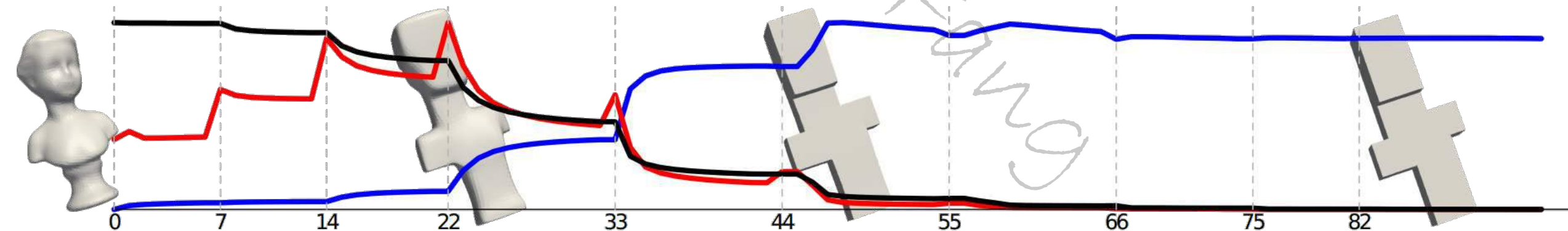
Polycube-Based Method

- Polycube: Global structure is simple
- L1 Polycube [Huang TOG 2014]

$$\|\mathbf{n}\|_1$$



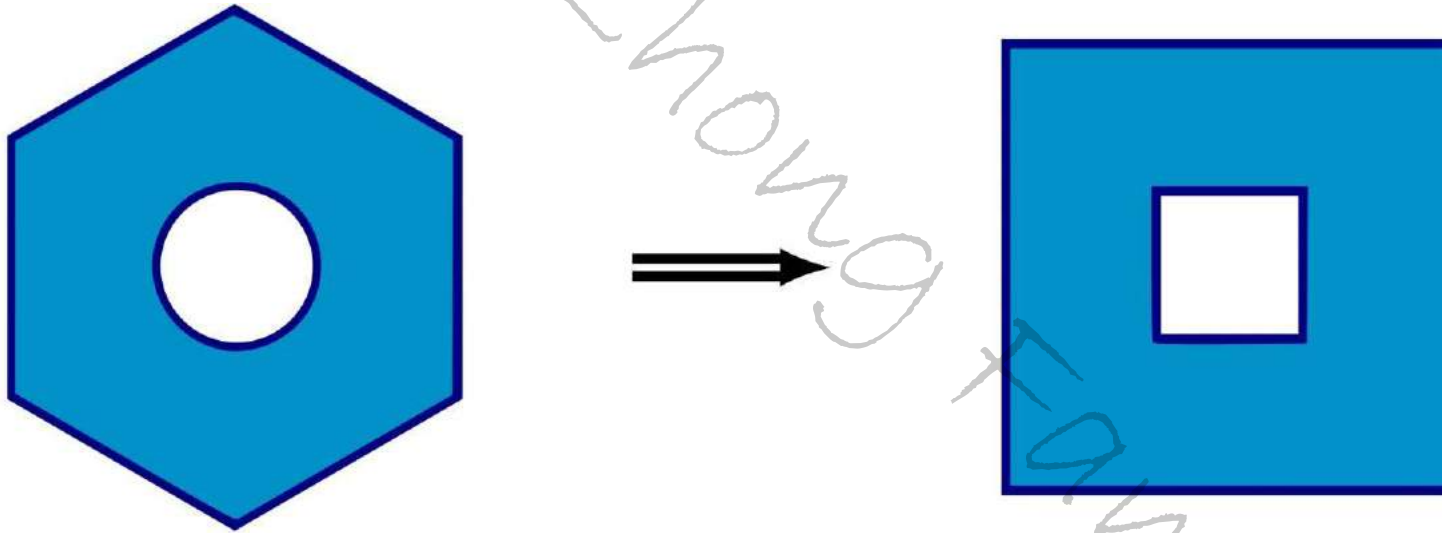
$$\min \int_{\partial\Omega} \|\mathbf{n}\|_1 + E_{ARAP}$$



Frame field-driven quad- and hex-remeshing

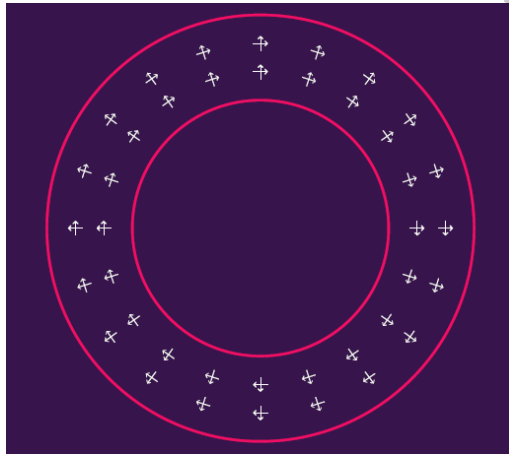
Polycube-Based Method

- Robust, but low quality

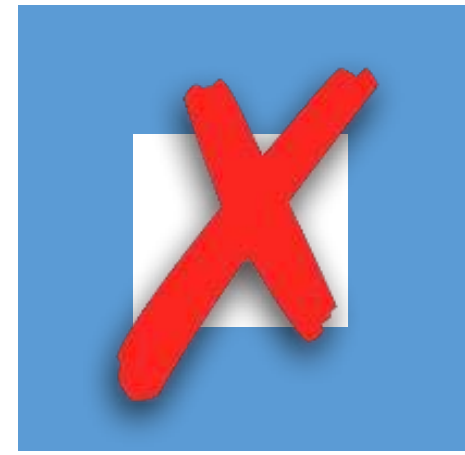
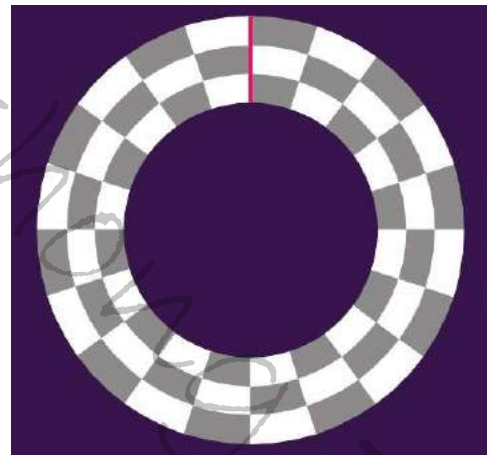


Another Simple Case

No singularity



Parametrization domain is not polycube



$$\omega = d\alpha + h$$

Closed-form

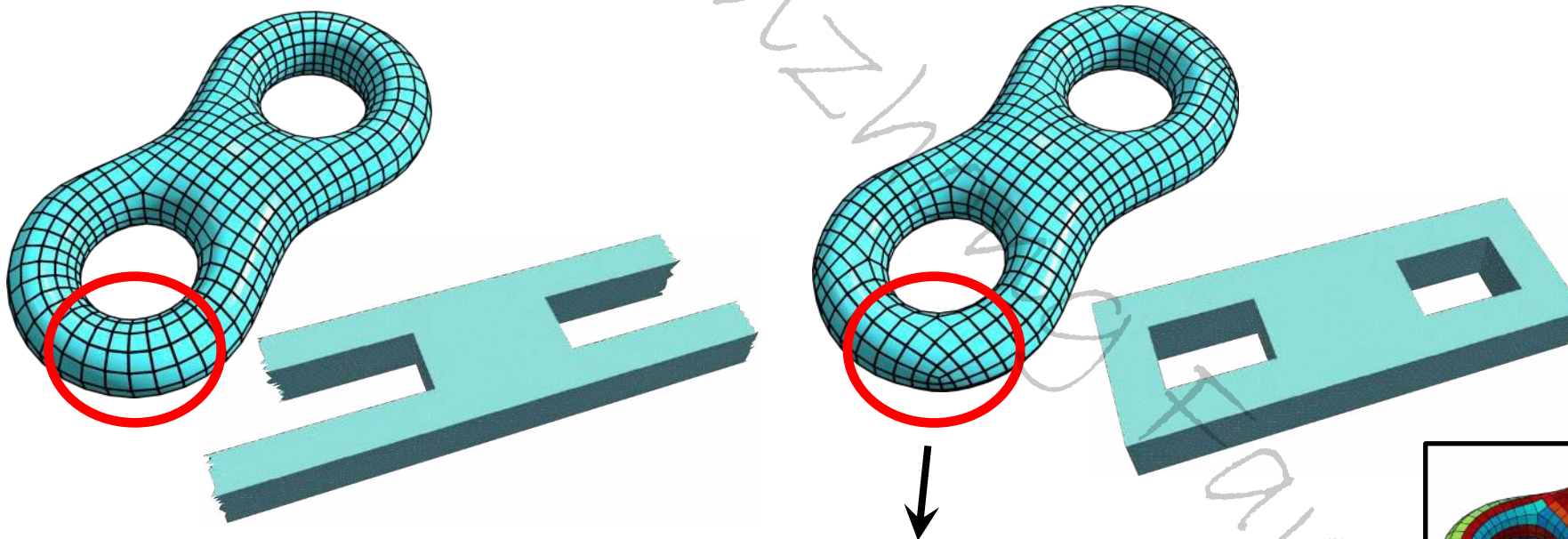
Exact-form

Harmonic form

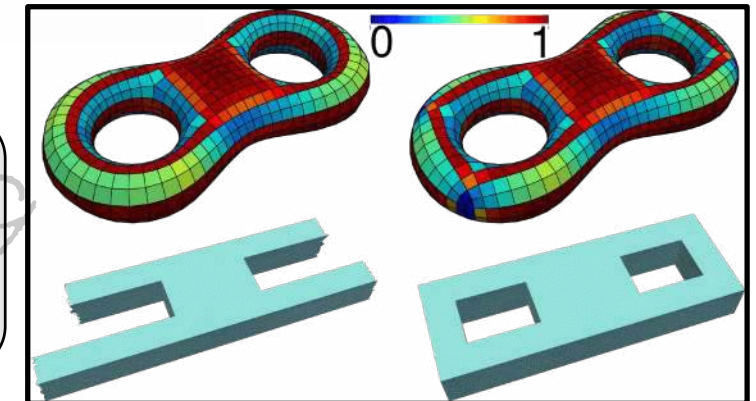
Related to
global topology

Global Topology Introduces DoF

- Genus, non-contractible loops, first homology group



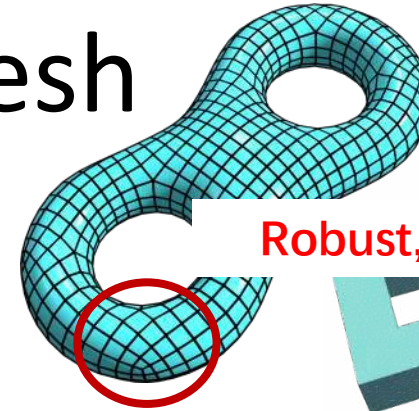
Do not consider global topology.
The quality of hex elements is low.





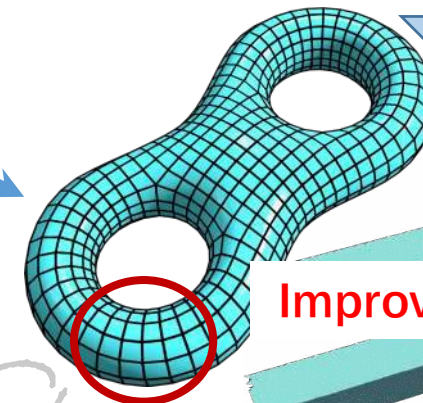
Inner Singularity-Free Hex-mesh

Exact-form Polycube



Robust, but low quality

Consider global topology



Improve quality

Closed-form
Polycube

Form

Closed form

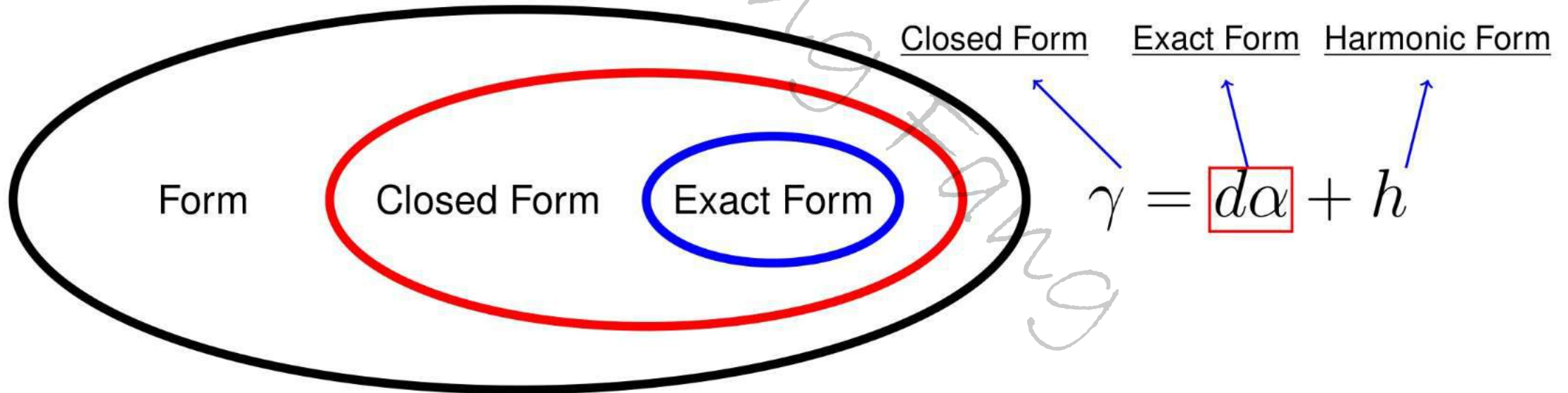
Exact
form

Inner singularity-free hex-mesh
Easy to generate

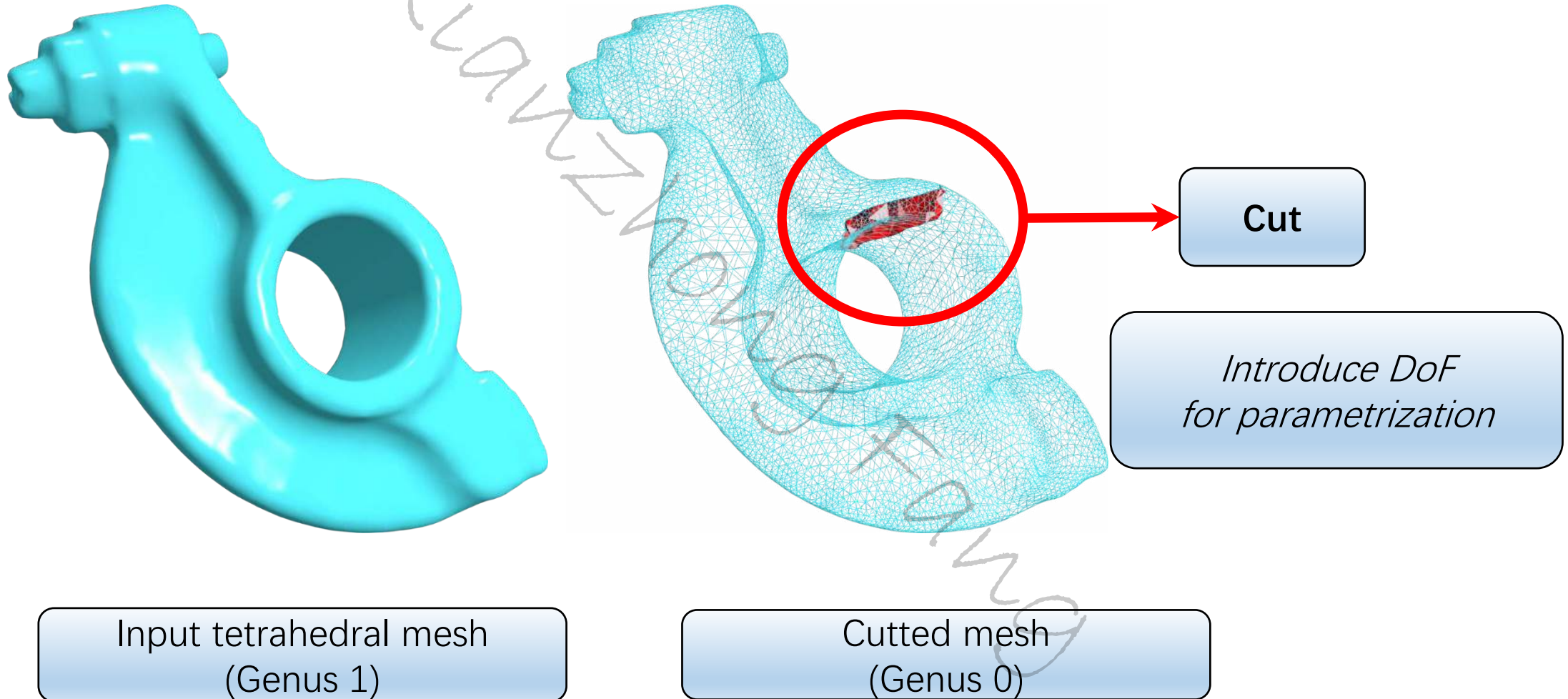
Frame field-driven quad- and hex-remeshing

Inner Singularity-Free Structure

- Hex-meshes \Rightarrow Differential form (**Non-robust, High DOFs & High quality**)
- Polycube-based \Rightarrow Exact-form (**Robust, but Low DOFs & Low quality**)
- Keep robustness with more DOFs:
 - Inner singularity-free \Rightarrow Closed-form

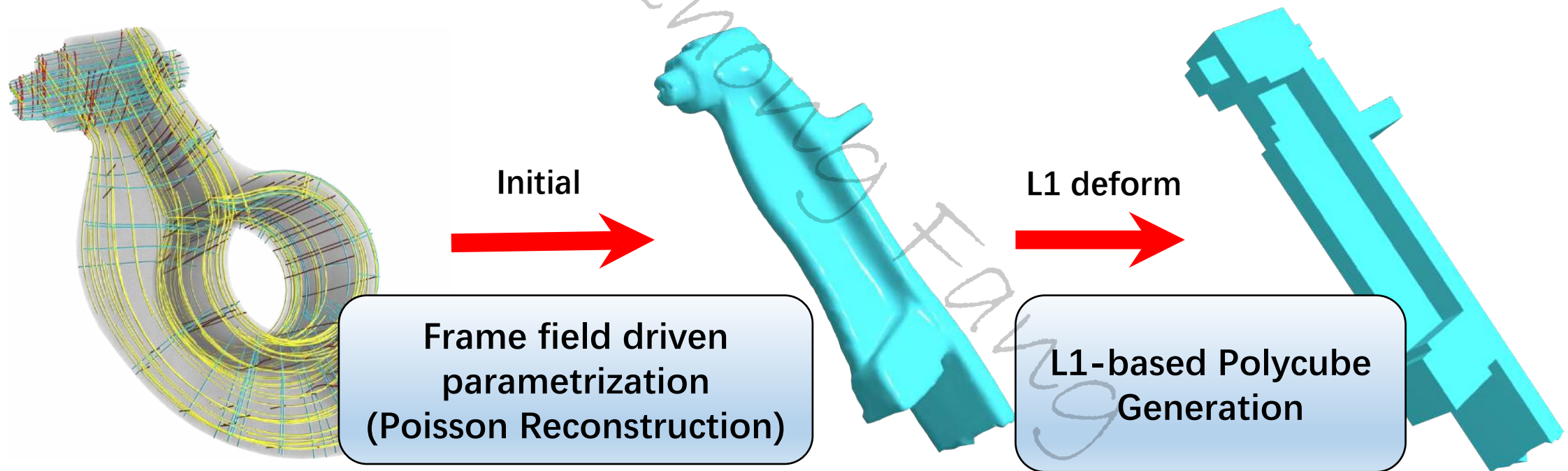


Topology Cutting: Introduce DoF



Closed-Form induced Polycube

- Inner singularity-free frame field
- L1 Polycube



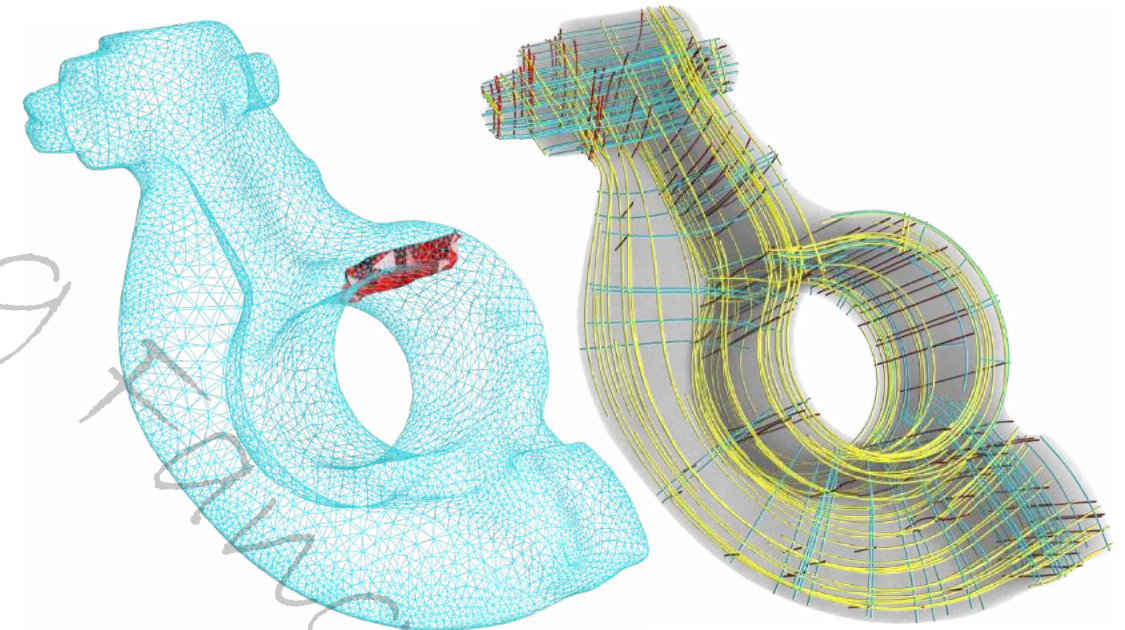
Inner Singularity-Free Frame Field

- Smoothness: As smooth as possible about \mathbf{R}
- Boundary alignment: Align the boundary normals

$$\begin{aligned}
 \min_{\mathbf{R}} \quad & w_f \int_{\mathcal{F} \setminus \mathcal{C}} \|\nabla \mathbf{R}\|^2 + w_c \int_{\mathcal{C}} \tilde{\nabla} \mathbf{R} \\
 & + w_a \int_{\partial \mathcal{M}} \|\mathbf{R} \mathbf{n}\|_1 + w_d \int_{\partial \mathcal{M} \setminus \partial \mathcal{C}} \|\nabla (\mathbf{R} \mathbf{n})\|^2 \\
 & + w_R \int_{\mathcal{M}} \|\mathbf{R}^T \mathbf{R} - \mathbf{I}\|^2.
 \end{aligned}$$

Smoothness
Smoothness on cuts

Alignment



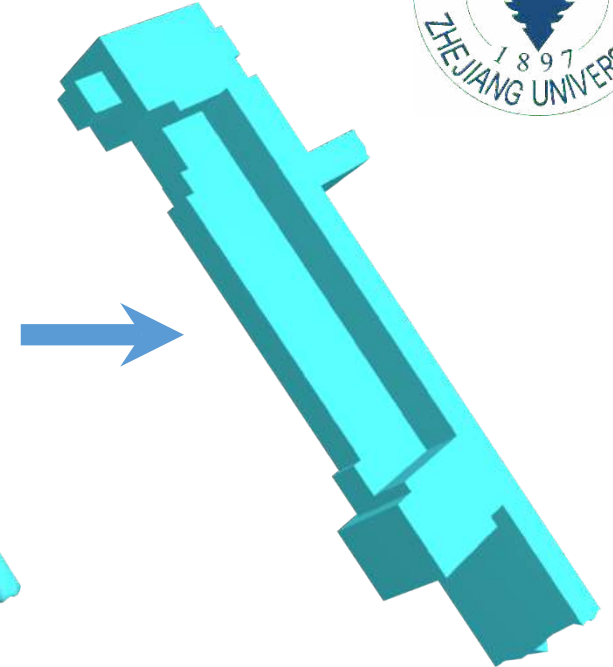
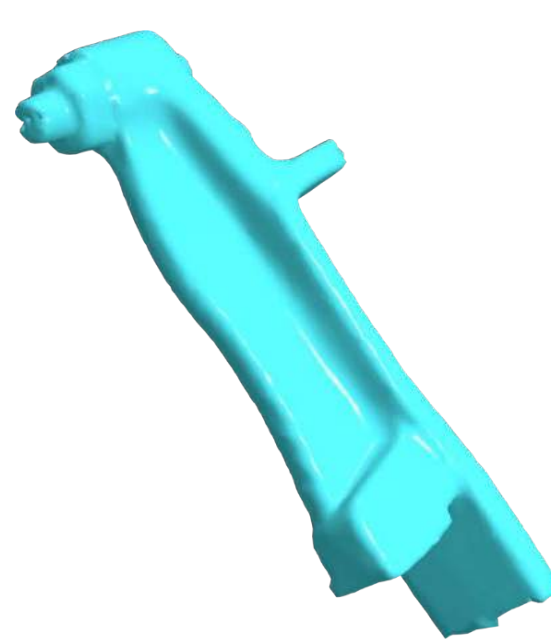
Boundary-aligned Smooth
Frame field as Initial

After above optimization

Inner singularity-free

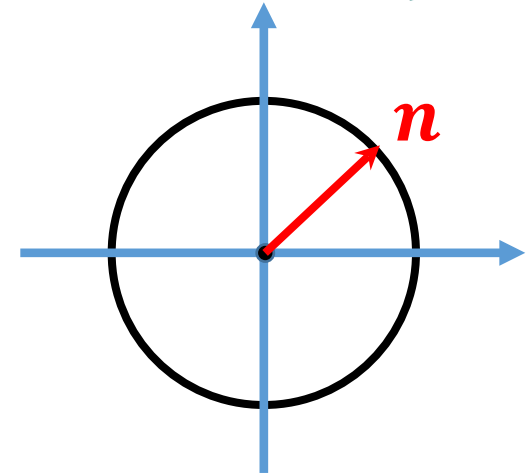
Polycube Generation

- Based on L1 deformation
- Use Poisson Reconstruction as Initial value
- ARAP + Alignment
- Transition functions on cuts
- Nonlinear optimization

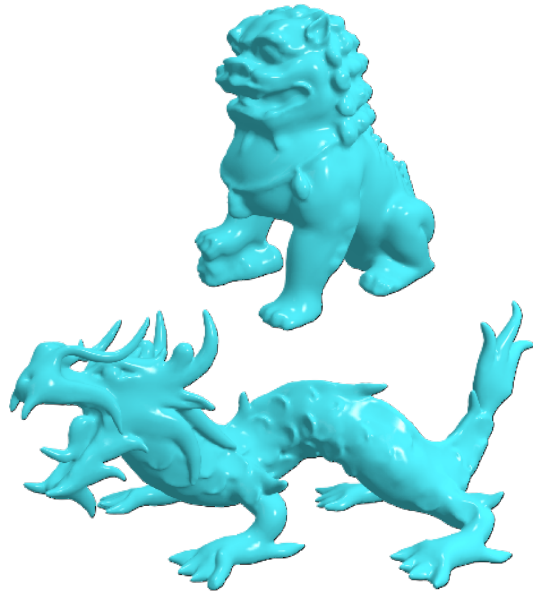


$$\begin{aligned}
 \min_{\bar{\mathcal{X}}} \quad & E_{arap} + w_{align} E_{align} + w_{diff} E_{diff} \\
 \text{s.t.} \quad & \bar{A}(\bar{\mathcal{X}}(\mathcal{M})) = A_{\partial\mathcal{M}} \\
 & \Pi_{a,b} \bar{\mathcal{X}}_a(e) = \bar{\mathcal{X}}_b(e), \quad \forall e \in t_a \cap t_b \in \mathcal{C}.
 \end{aligned}$$

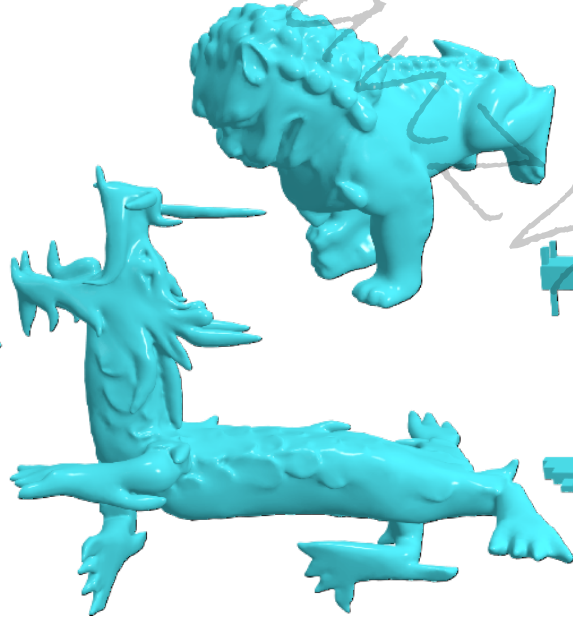
$$\|n\|_1$$



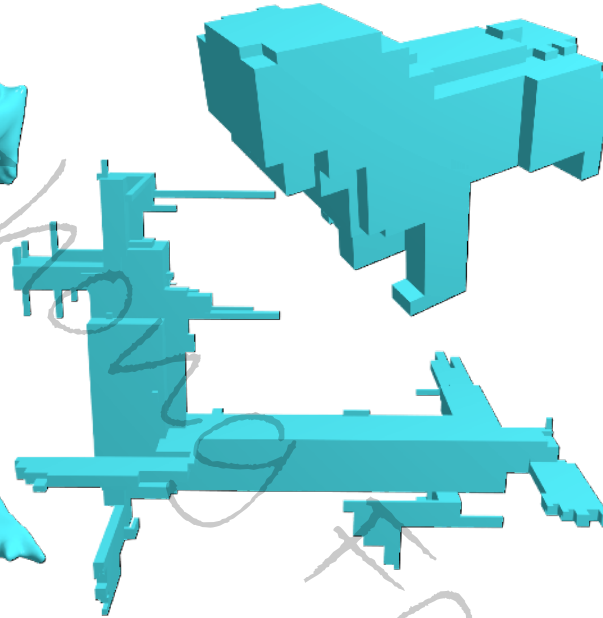
Better Alignment



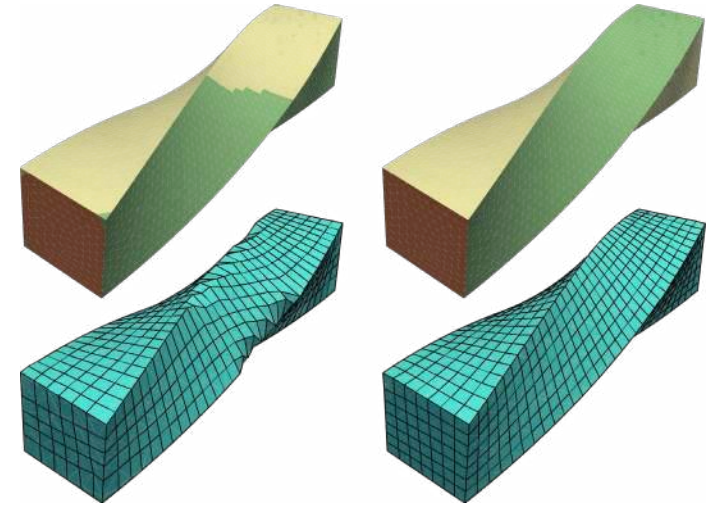
Input mesh



Poisson
Reconstruction

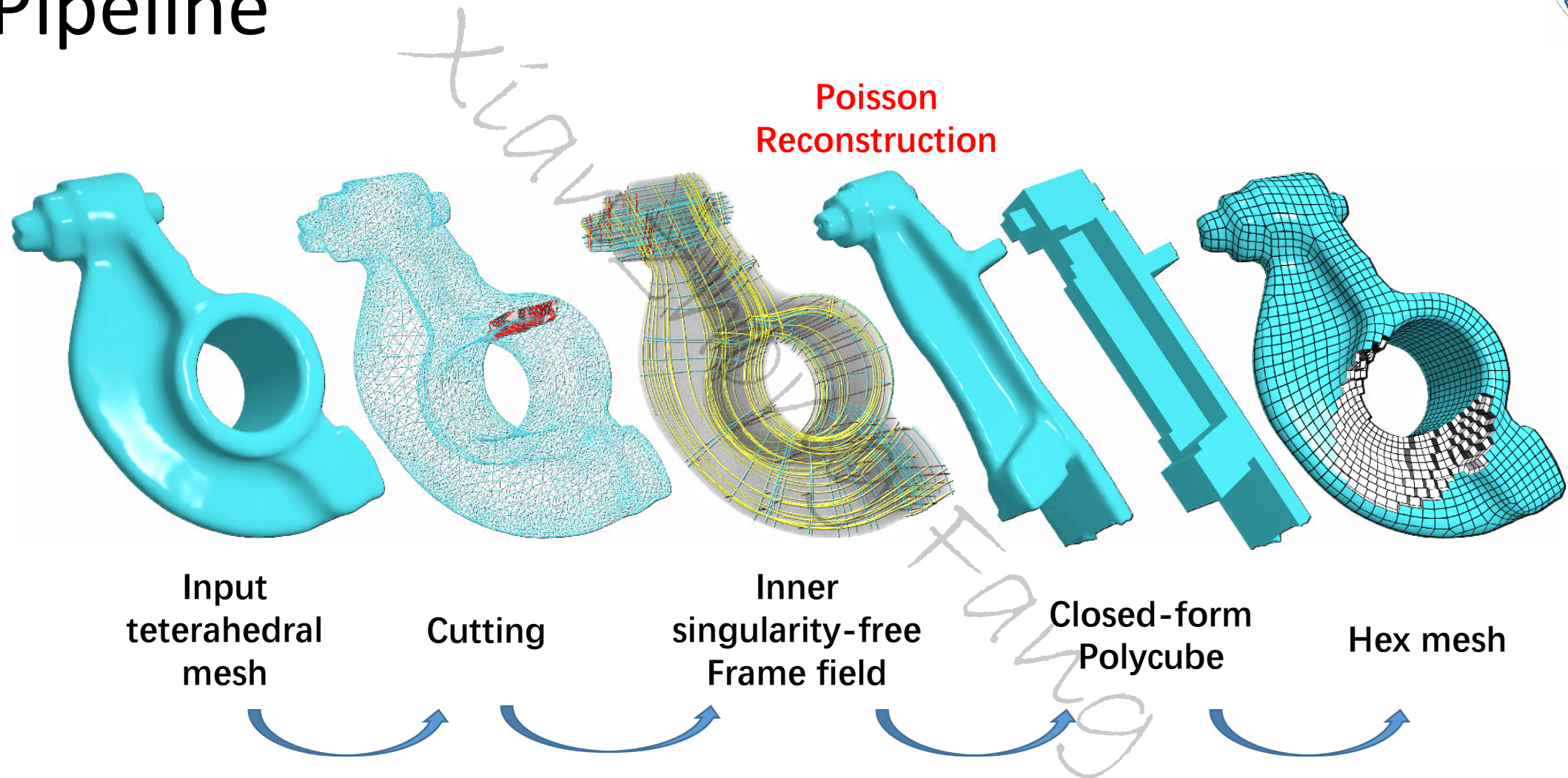


Closed-form
polycube



Better Feature alignment

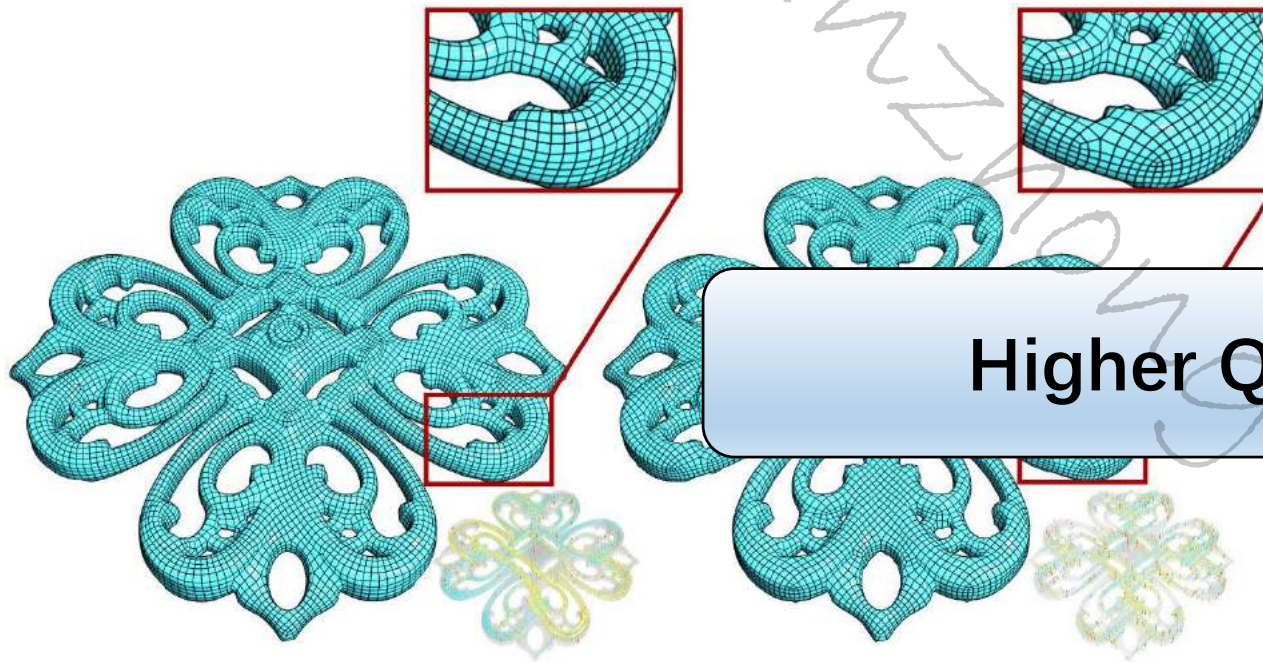
Pipeline



[Fang et al. TOG '16]

Results

- Closed-form Polycube VS Exact-form Polycube

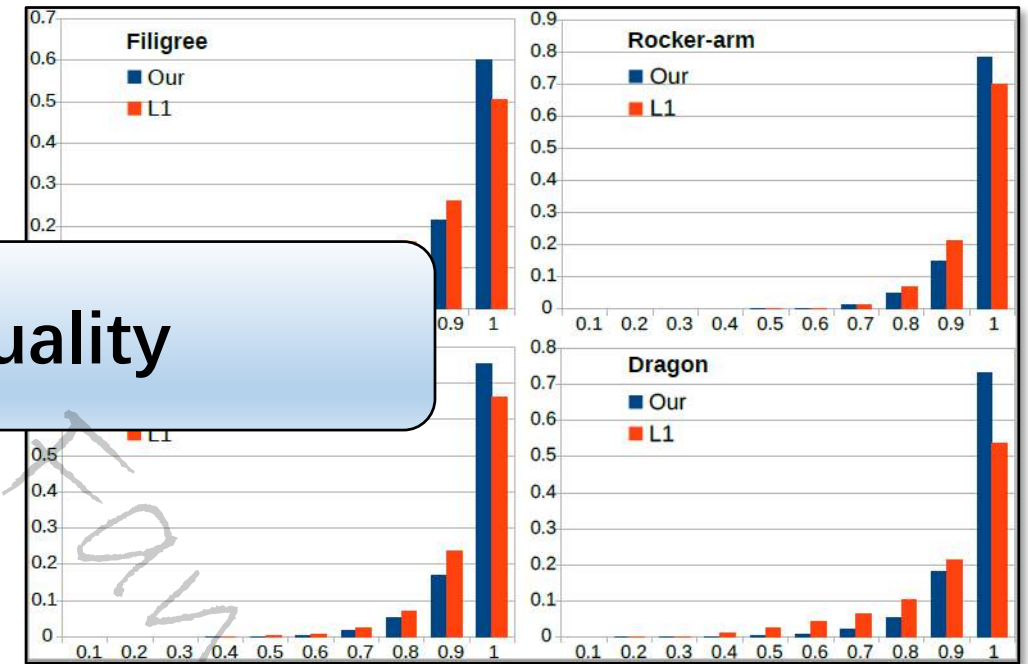


Consider
topology

Constrained by
global topology

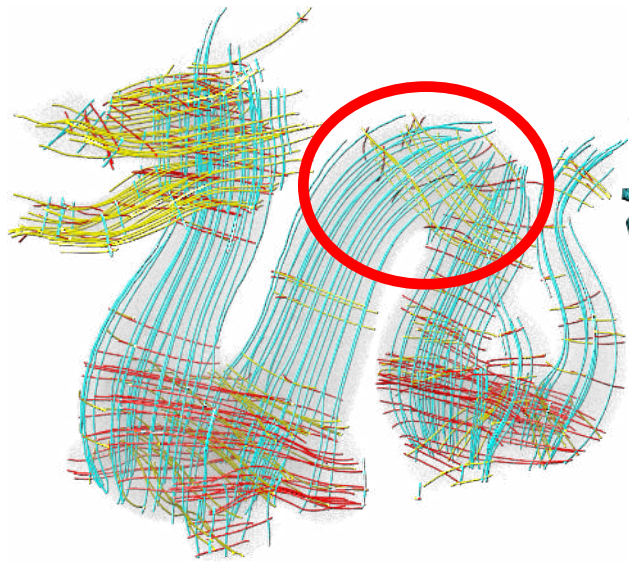
Frame field-driven quad- and hex-remeshing

Higher Quality

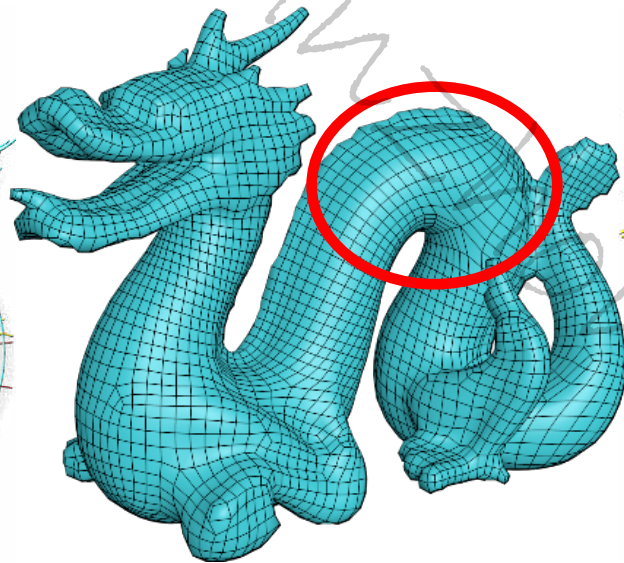


Scaled Jacobian Distribution of Results

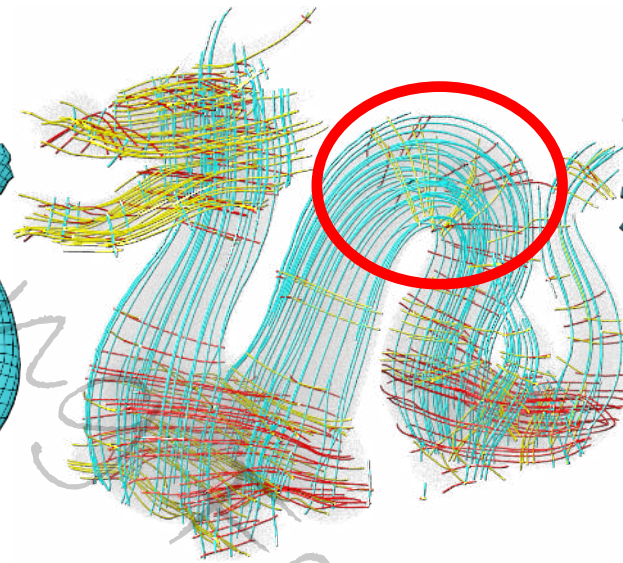
Frame Field Control



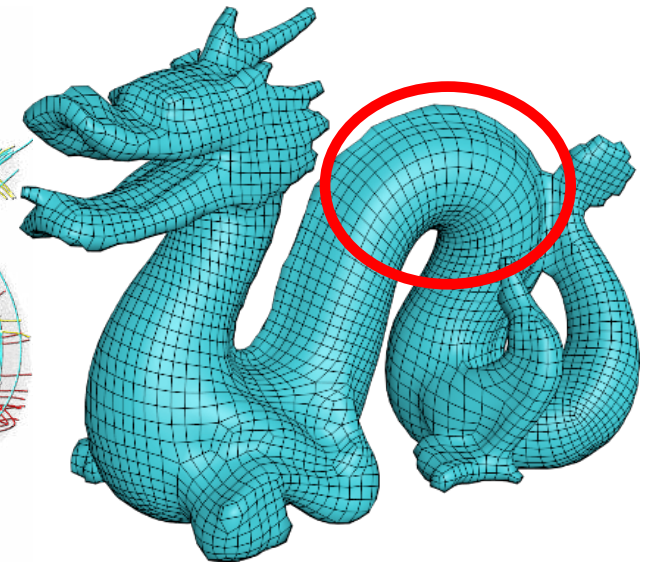
Frame field



Hex mesh

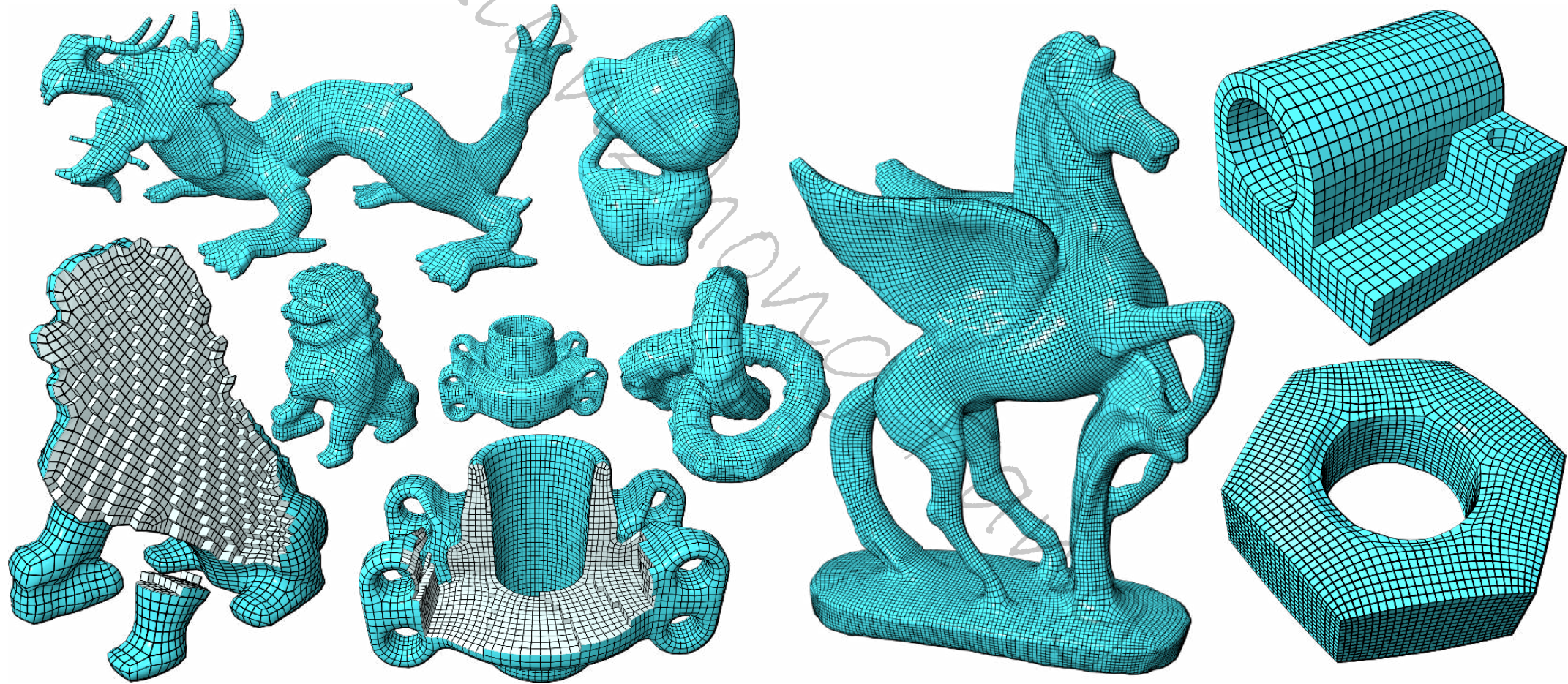


Frame field



Hex mesh

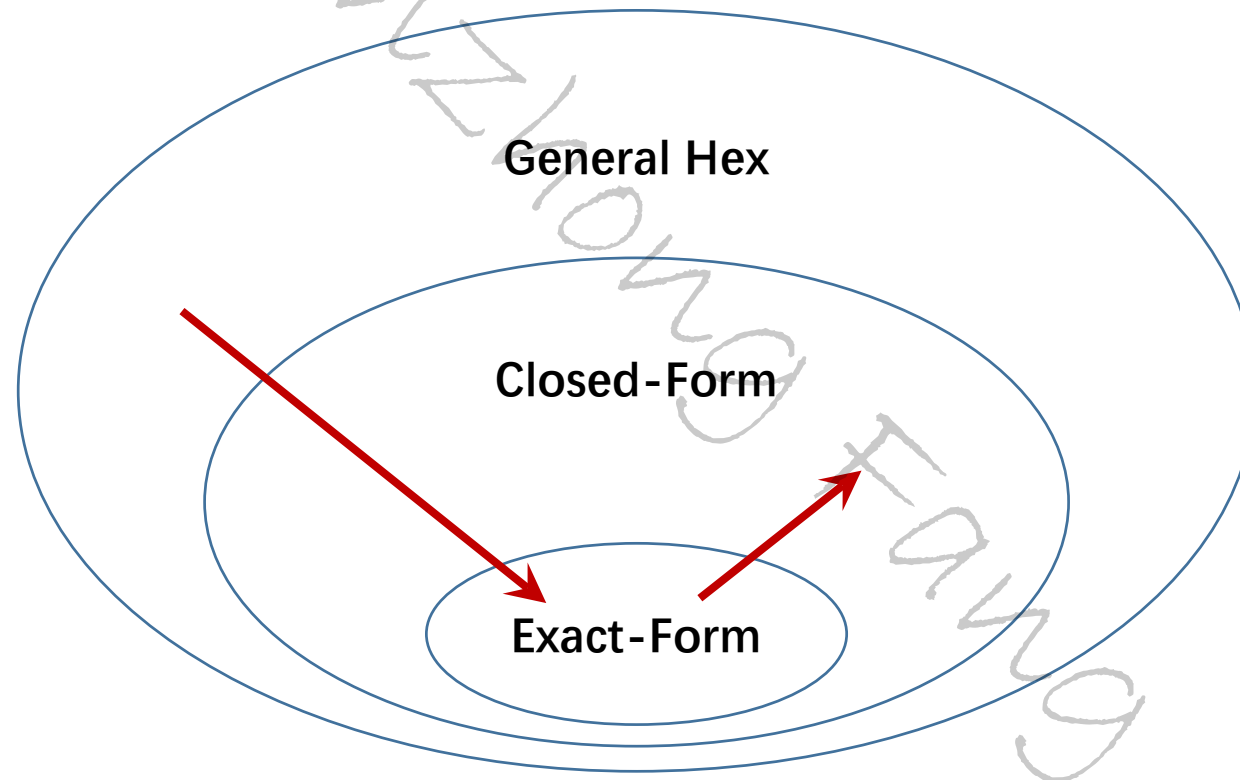
Results



[Fang et al. TOG '16]

Frame field-driven quad- and hex-remeshing

The Big Picture of Hex-Remeshing





Conclusion

- Internal singularity-free hexahedral mesh can be reliably generated
- Future works:
 - Consider internal singularities
 - Flexible control: arbitrary size/direction



Reference

- [Fang et al. TOG '16] All-hex meshing using closed-form induced polycube
- [Huang et al. TOG '14] ℓ_1 -based construction of polycube maps from complex shapes
- [Huang et al. TOG '11] Boundary aligned smooth 3d cross-frame field
- [Jiang et al. TVCG '14] Frame field singularity correction for automatic hexahedralization
- [Li et al. TOG '12] All-hex meshing using singularity restricted field
- [Fang et al. TOG '18] Quadrangulation through Morse-parameterization hybridization
- [Zhang et al. TOG '10] A wave-based anisotropic quadrangulation method
- [Bommes et al. TOG '12] Mixed-integer quadrangulation
- [Bommes et al. TOG '13] Integer-grid maps for reliable quad meshing
- [Myles and Zorin TOG '13] Controlled-distortion constrained global parameterization
- [Bommes et al. CGF '13] Quad-mesh generation and processing: A survey
- [Livesu et al. TOG '13] Polycut: Monotone graph-cuts for polycube base-complex construction
- [Nieser et al. CGF '11] Cubecover-parameterization of 3d volumes
- [Palacios et al. TOG '07] Rotational symmetry field design on surfaces
- [Kälbere et al. CGF '07] Quadcover: Surface parameterization using branched coverings
- [Dong et al. TOG '06] Spectral surface quadrangulation
- [Tarini et al. TOG '04] Polycube-maps

Thanks!
Q & A